

GVTDOC
D 211.
9:
4252

NAVAL SHIP RESEARCH AND DEVELOPMENT CENTER

Bethesda, Md. 20034



A COMPUTER PROGRAM THAT USES INTERACTIVE GRAPHICS TO SOLVE
INVISCID TRANSONIC FLOWS OVER LIFTING AIRFOILS

by

Douglas A. Lien

and

Tsze C. Tai

DISTRIBUTION STATEMENT A

Approved for Public Release
Distribution Unlimited

LIBRARY

MAY 6 1974

U.S. NAVAL ACADEMY

FOR OFFICIAL USE ONLY

AVIATION AND SURFACE EFFECTS DEPARTMENT
RESEARCH AND DEVELOPMENT REPORT

20070119127

September 1973

Report 4252

Best Available Copy

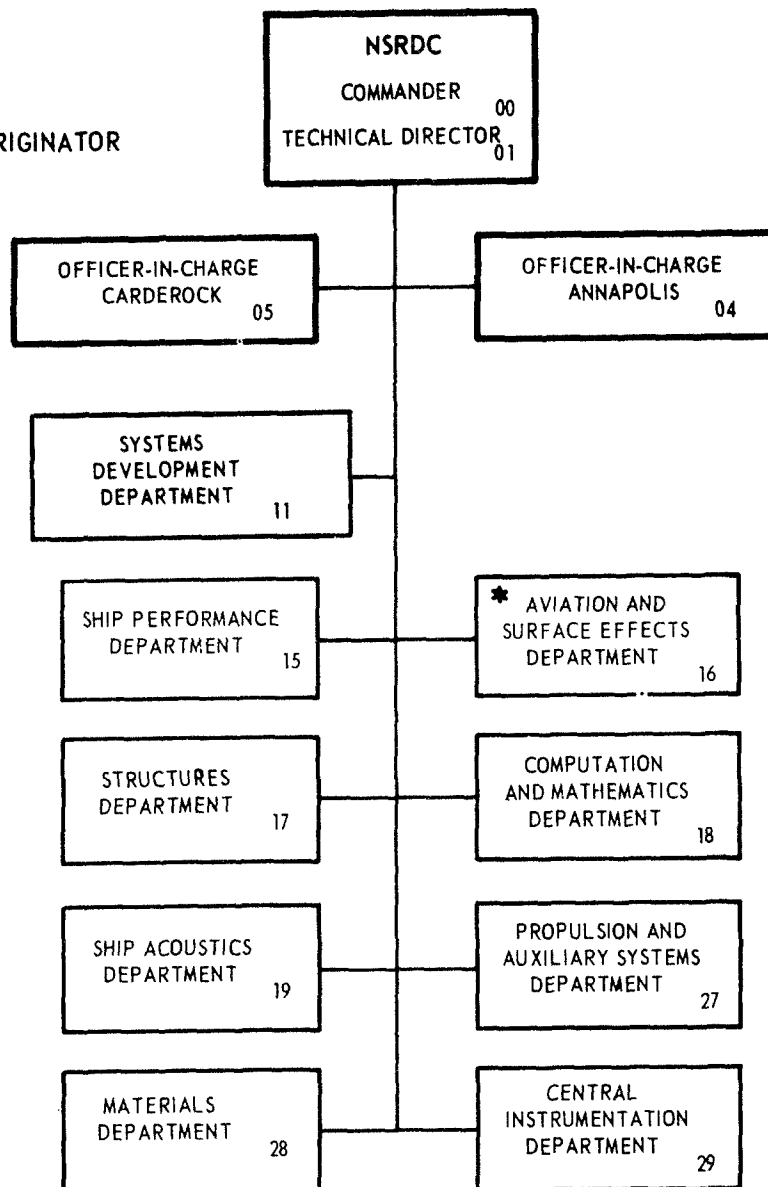
A COMPUTER PROGRAM THAT USES INTERACTIVE GRAPHICS TO SOLVE
INVISCID TRANSONIC FLOWS OVER LIFTING AIRFOILS

The Naval Ship Research and Development Center is a U. S. Navy center for laboratory effort directed at achieving improved sea and air vehicles. It was formed in March 1967 by merging the David Taylor Model Basin at Carderock, Maryland with the Marine Engineering Laboratory at Annapolis, Maryland.

Naval Ship Research and Development Center
Bethesda, Md. 20034

MAJOR NSRDC ORGANIZATIONAL COMPONENTS

* REPORT ORIGINATOR



DEPARTMENT OF THE NAVY
NAVAL SHIP RESEARCH AND DEVELOPMENT CENTER
Bethesda, Maryland 20034

A COMPUTER PROGRAM THAT USES INTERACTIVE GRAPHICS TO SOLVE
INVISCID TRANSONIC FLOWS OVER LIFTING AIRFOILS

by

Douglas A. Lien
and
Tsze C. Tai



FOR OFFICIAL USE ONLY

September 1973

Report 4252
Aero Report 1194

TABLE OF CONTENTS

	<u>Page</u>
ABSTRACT	1
ADMINISTRATIVE INFORMATION	1
INTRODUCTION	1
DESCRIPTION OF COMPUTER PROGRAM	3
ORDER OF OPERATIONS	4
ILLUSTRATIVE EXAMPLES	7
APPLICATION OF INTERACTIVE GRAPHICS	12
BASIC FORMAT	13
ILLUSTRATIVE EXAMPLE	14
APPENDIX A - AIRFOIL REPRESENTATION BY SPLINES	47
APPENDIX B - DESCRIPTION OF SUBROUTINES	50
APPENDIX C - SUBROUTINE FLOW CHARTS	68
APPENDIX D - DESCRIPTION OF INTERACTIVE GRAPHICS PROGRAM	80
APPENDIX E - INPUT DESCRIPTION FOR INTERACTIVE GRAPHICS	89
APPENDIX F - IGS PROGRAM LISTING	104
APPENDIX G - MIR SUBROUTINES LISTING	148
REFERENCES	197

LIST OF FIGURES

Figure 1 - The Solution Procedures for Transonic Flow Problems	21
Figure 2 - Flow Chart for the More Important Subroutines	22
Figure 3 - Overview of the Solution Process	23
Figure 4 - Choice of Stagnation Point	24
Figure 5 - Choice of CYDL for Lower Surface Flow	25
Figure 6 - Control Volume Used to Determine Initial Velocity on Airfoil Surface	26
Figure 7 - Effect of CYD on $\rho_b V_b$	27

	<u>Page</u>
Figure 8 - Choice of CYDU for Upper Surface Flow	28
Figure 9 - Choice of SL for Downstream Flow	29
Figure 10 - Choice of CYDL for Downstream Flow	30
Figure 11 - Check of Kutta Condition at the Trailing Edge . . .	31
Figure 12 - Second Derivative Spline Fit for an Advanced Airfoil .	32
Figure 13 - Deck Setup for Creation of TASKLOAD File	33
Figure 14 - Deck Setup for a Graphics Run	34
Figure 15 - Flow Chart for the More Important Tasks of the Interactive Graphics Program	35
Figure 16 - Basic Format for Screen Displays	36
Figure 17 - First Screen Display	37
Figure 18 - Screen Display for Upstream Solution	38
Figure 19 - Screen Display for Stagnation Solution	39
Figure 20 - Screen Display for Flow Criticality on Upper Surface .	40
Figure 21 - Screen Display for Initial Solution - Upper Surface .	41
Figure 22 - Screen Display for Airfoil Solution - Upper Surface .	42
Figure 23 - Screen Display for Flow Criticality on Lower Surface .	43
Figure 24 - Screen Display for Airfoil Solution - Lower Surface .	44
Figure 25 - Screen Display for Downstream Solution	45
Figure 26 - Screen Display for Kutta Condition Check	46

ABSTRACT

A computer program that utilizes the method of integral relations has been developed at the Naval Ship Research and Development Center for use in determining the inviscid transonic flows past lifting airfoils. It allows for a change of entropy across the shock wave and accounts for the presence of an oblique or normal shock at the shock foot. Since many iterations of the trial and error type are required to obtain the converged flow solution, the program has been adapted for use on the interactive graphic systems of the CDC 6700 computer. This minimizes the man-machine interaction time involved with such iterations. It has been applied to several airfoil cases with supercritical flow on the upper surface and subcritical flow on the lower surface and takes about 5 to 10 min of computer time per case. The theoretical basis for this program has previously been reported. This report documents the computer program which is written in the language of FORTRAN Extended Version 3.0.

ADMINISTRATIVE INFORMATION

This work was sponsored by the Naval Air Systems Command (NAVAIR-320) and funded under NAVAIR Task R230.201, Work Unit 1-1670-277.

INTRODUCTION

Application of the method of integral relations to solve transonic flow problems has already been developed and the method used in several flow solutions.^{1,2} The present report documents the subroutines used in

1. Tai, T. C., "Application of the Method of Integral Relations to Transonic Airfoil Problems: Part I - Inviscid Supercritical Flow over Symmetrical Airfoil at Zero Angle of Attack," NSRDC Report 3424 (Sep 1970); also presented as Paper 71-98, AIAA 9th Aerospace Sciences Meeting, New York, N.Y. (Jan 1971).

2. Tai, T. C., "Application of the Method of Integral Relations to Transonic Airfoil Problems: Part II - Inviscid Supercritical Flow About Lifting Airfoils with Embedded Shock Wave," NSRDC Report 3424 (Jul 1972); also presented as Paper 73-658, AIAA 6th Fluid and Plasma Dynamics Conference, Palm Springs, California (Jul 1973).

computing transonic flows and illustrates their use with two examples: transonic flow past an NACA 0015 airfoil at $\alpha = 4.0$ deg and transonic flow past an advanced airfoil at $\alpha = 1.5$ deg.

The solution procedure consists of ten well-defined steps in accordance with necessary iteration processes. The completion of each step must satisfy certain flow conditions before the next step is undertaken. Actually, there are only three major iteration processes which form the bulk of the flow integration, and each process can be computed rapidly and efficiently. The main drawback to this method is that each step must be computed separately and that the output of one step is needed before the next step can proceed. This can be a time-consuming process if done by conventional means.

The use of interactive graphics greatly reduces man-machine interaction time. The input parameters and program execution can be modified by using a system of light registers and light buttons displayed on the CDC 274 graphics console screen. In order to simplify the solution process, only subcritical flow on the lower surface and supercritical flow on the upper surface will be allowed.

The primary inputs to the program are the airfoil coordinates (a maximum of 40 data points) and 32 extraneous and physical flow parameters. During execution of the interactive graphics program, 18 of these flow parameters may be changed, but ordinarily only one or two are used to iterate on a particular flow solution to satisfy a particular flow condition. The remainder of the flow solution parameters may be properly determined subject to the necessary constraints.

The importance of a well-defined airfoil shape cannot be stressed too strongly. This highly sensitive technique requires great accuracy in first and second derivative information from the airfoil surface. The spline function is one highly recommended method for representing airfoil surfaces. It can attain very accurate first and second derivatives from the airfoil surface if certain constraints are chosen judiciously. The method is explained in detail in Appendix A.

However, one fact should be borne in mind before attempting to use this program to solve transonic flows; it is not a "black box" computer program which generates output for a given set of input data. It requires special attention during execution to ensure that certain flow requirements are met. If the calculated flow is unsatisfactory, one of the input parameters should be changed to yield a satisfactory result. Luckily, it can be seen from inspection whether the value of a parameter is too large or too small, and input changes can be made accordingly.

DESCRIPTION OF COMPUTER PROGRAM

Application of the method of integral relations for transonic flow problems involves three major flow solutions:

1. Upstream solution
2. Airfoil solution
3. Downstream solution

These solutions must be computed sequentially, that is, the upstream solution must be computed before proceeding to the airfoil solution, and the airfoil solution must be computed before proceeding to the downstream solution. These steps are shown in Figure 1. The order of operations within the airfoil solution is immaterial; either the upper surface flow or the lower surface flow can be computed first.

The input to the program is only an approximation to the correct input which would yield a satisfactory solution. During the course of the solution, the input is modified to satisfy certain flow conditions. For instance, in the case of supercritical flow in the airfoil solution, the initial condition parameter CYD is changed until calculations show that the velocity gradient is continuous through the sonic point. Other inputs are modified in reply to the questions shown in Figure 1. When all the flow conditions are met satisfactorily and the solution is complete, the calculated pressure distribution is the serendipitous result of the solution process.

ORDER OF OPERATIONS

The flow chart of Figure 2 gives a more detailed analysis of the order of operations of the more important subroutines. A list of these subroutines and their function is given below.

UPSTRM = performs upstream flow integration
STAGNA = calculates stagnation streamline geometry and cross velocity gradient for given stagnation point XS
UPRCRIT = calculates Mach number conditions along initial portion of upper surface
LWRCRIT = calculates Mach number conditions along initial portion of lower surface
UPRINIT = calculates initial conditions on upper surface for a selected initial point and CYD
LWRINIT = calculates initial conditions on lower surface for a given initial point and CYD
SUBCRT1 = performs subcritical flow integration on initial portion of either upper or lower surface
SUBCRT2 = performs subcritical flow integration on either upper or lower surface
SPRCRT1 = performs supercritical flow integration on initial portion of upper surface
SPRCRT2 = performs supercritical flow integration on upper surface
DWNSTRM = performs downstream flow integration
AKUTTA = provides outputs of calculated upper and lower surface pressure distributions

Subroutines UPSTRM and STAGNA correspond to the upstream solution, and subroutines DWNSTRM and AKUTTA correspond to the downstream solution of Figure 1. The rest of the subroutines correspond to the airfoil solution. The details of the subroutines are given in Appendix B, and a flow chart of each subroutine is given in Appendix C.

Eight of the more important decision points are numbered in Figure 2. The dotted lines indicate the parameter changes needed for satisfactory results. Each decision point requires some attention, either a

modification of the input parameters or a decision on which course to follow in the computation.

An overview of the solution process which consists of various steps is given in Figure 3. Since the flow solution on the upper surface is much more interesting than that on the lower surface, only upper surface flow is discussed here in detail.

The numbered stars around the airfoil correspond to certain subroutines in Figure 2:

- 1 UPSTRM
- 2 STAGNA
- 3 UPRINIT-SPRCRT1
- 4 SPRCRT2
- 5 DWNSTRM
- 6 AKUTTA

The output for a particular subroutine is on either side of the corresponding number in the figure. The trial solution to the left could be improved on; the arrow indicating the parameter changes needed to improve the solution, and the corrected or acceptable solution to the right represents a completed step. Once this is completed, the program begins executing the next step.

The output from the first step shows a plot of Y versus Mach number. This velocity profile is taken from the final integration station of subroutine UPSTRM. The number of strips used to integrate the flow solution in the trial solution proved inadequate, and more strips were added to yield the corrected solution.

The second step is concerned with the selection of a stagnation point. The stagnation point for the trial solution was chosen at the nose of the airfoil; this yielded unrealistic stagnation streamline geometry for a lifting airfoil. A more satisfactory location of the stagnation point is given in the corrected solution. The selection of the stagnation point is most critical to later calculations.

The first major iteration process is given in the third step. In the trial solution the initial condition parameter CYD, which depends on assumed velocity profile shape ahead of the airfoil, did not yield velocity

gradients which were continuous through the sonic point. In the case of $CYD = 1.0$, the flow accelerated too rapidly before the sonic point, and in the case of $CYD = 1.010$, the flow decelerated before the sonic point. $CYD = 1.005$ for the corrected solution, and the velocity gradients were continuous through the sonic point. This step calculates the flow on the initial portion on the upper surface. The fourth step calculates the remainder of the flow.

In the fourth step, the only requirement for a satisfactory solution is the selection of a shock location which allows the flow calculations to proceed to the trailing edge. The shock location must be chosen so that the flow behind it remains subcritical throughout to the trailing edge. The exact shock location is determined by satisfying the downstream flow condition as outlined in the fifth step. The two initial guesses in the trial solution show cases of flow which become supercritical again after the shock wave. The corrected solution indicates where a case flow remains subcritical behind the shock location.

The third and fourth steps constitute the airfoil solution on the upper surface. For the lower surface of the airfoil, a solution is sought which allows flow integration to proceed to the trailing edge. Once the airfoil solutions for the upper and lower surfaces have been obtained, the downstream solution may be calculated.

The fifth step is concerned with flow calculations downstream from the airfoil. In the trial solutions the pressures diverged from the free-stream pressures quite rapidly. Thus it was necessary to return to the fourth step and select a new shock location which would yield downstream pressures bracketing the free-stream values. It can be seen in the corrected solution that the final shock location was between 0.50 and 0.51; the pressure was slightly greater than free-stream pressure for one value and slightly less for the other.

The final step of the solution process is to check the calculated pressure distributions on the upper and lower surfaces of the airfoil. If the pressures at the trailing edge do not match on the upper and lower surfaces, the Kutta condition is not met, and program control should be transferred to the second step for the selection of a new stagnation point. If the stagnation point is judiciously chosen, the pressure distribution in the corrected solution should appear.

ILLUSTRATIVE EXAMPLES

A description of the order of operations of this computer program is best presented by illustrating its application to a particular airfoil.

NACA 0015 Airfoil

The NACA 0015 airfoil at an angle of attack of 4 deg and a free-stream Mach number of 0.729 are used here for purposes of illustration. Experimental results have shown that at these flow conditions, the flow is supercritical on the upper surface and subcritical on the lower surface.³

The five input flow parameters of greatest importance to the solution process are:

DVOOI $(dV_o/ds)_o$, the estimated cross velocity gradient at the stagnation point,

XS, the X-coordinate of the stagnation point,

CYDL, the initial condition parameter for the lower surface flow,

CYDU, the initial condition parameter for the upper surface flow, and

SL, the location of the shock foot for the upper surface flow.

Decision point 1 comes after subroutine STAGNA, the calculation of stagnation streamline geometry and the cross velocity gradient at the selected stagnation point. It is important to select a stagnation point

3. Graham, D. J. et al., "A Systematic Investigation of Pressure Distribution at High Speeds over Five Representative NACA Low-Drag and Conventional Airfoil Sections," NACA Report 832 (1945).

for which the streamline geometry appears most reasonable because this solution is most critical to later calculations. The middle streamline shown in Figure 4 was chosen, and the calculated cross velocity gradient for this stagnation point was 4.343. Since this agreed well with the estimated cross velocity gradient of 4.252, this is considered a valid or permissible solution for the upstream flow. If this cross velocity gradient were not correct, another iteration would be needed for the upstream solution with a new estimate of the cross velocity gradient.

The cross velocity gradient DV001 determines the perturbation of the stagnation streamline due to the presence of the airfoil. A greater perturbation is realized with increasing values of DV001.

After decision point 1, there are two possible paths for further flow calculations. The path to the left corresponds to flow integration on the lower surface. For this path, $J=2$ and subroutine LWRCRIT is computed. The path to the right corresponds to flow on the upper surface. For this path, $J=1$ and subroutine UPRCRIT is calculated. Decision points 2 and 3 determine whether subcritical or supercritical flow options are to be taken on the upper or lower surface. A simple test was made for selecting the supercritical or subcritical options. This information is stored in ICRIT(J). Thus $ICRIT(1) = 1$ for supercritical flow on the upper surface and $ICRIT(2) = 2$ for subcritical flow on the lower surface. Once a decision on flow criticality has been made, flow integration may proceed to the flow solutions on either the upper or lower surface.

From decision point 2, the next step in flow calculation is subroutine LWRINIT, the initial solution on the lower surface. Depending on decision point 1, there are two possible paths for further flow integration. The path for $ICRIT(2) = 1$ is invalid since in its present form, the program is not prepared to handle supercritical flow on the lower surface. For $ICRIT(2) = 2$, flow integration is further computed by subroutines SUBCRT1 and SUBCRT2 which calculate subcritical flow. The output of these three subroutines is shown in Figure 5. For a permissible solution, the calculated Mach number along the airfoil surface should return to a value fairly close to the free-stream Mach number of 0.729. Decision point 4 consists of determining an appropriate value for

CYD. Inspection of Figure 5 shows that the value of $CYD = 0.8194$ is appropriate. Here the Mach number increased to a maximum at midchord and decreased to a value of 0.71 at the trailing edge.

An appreciation of the physical significance of the parameter CYD requires knowledge of the stagnation streamline geometry given in Figure 6. The control volume is the one outlined by points b, d, and f. Points f and d represent values which were computed in the upstream integration. The mass flow into the control volume is normal to the line d-f. Since there is no mass flow through the stagnation streamline or normal to the airfoil, the mass flow out of the control volume is normal to line b-d. Hence the mass flow out of the control volume is fixed and is equal to the area under the curve in Figure 7. The ordinate ρV is the mass flux across the line b-d, and the abscissa n is along the line b-d normal to the airfoil. Depending on the value of CYD, the product $\rho_b V_b$ can take on several values. Hence the velocity at the initial point on the airfoil V_b can be varied according to CYD. The initial velocity decreases as CYD increases.

Once an appropriate solution has been found for the lower surface, IGO(J) is set equal to 1 and control is transferred to decision point 5. Both IGO(1) and IGO(2) must equal 1 in order to proceed to DWNSTRM; otherwise control is transferred to decision point 1 and the other path is chosen for flow integration.

In the case discussed so far, the lower surface has already been computed and the upper surface flow remains to be computed. Upper surface flow has been assumed to be supercritical and control can be transferred to subroutine UPRINIT. After initial conditions in subroutine UPRINIT have been calculated, one of two paths can be chosen for upper surface flow integration, depending on the value of ICRIT(J). If $ICRIT(1) = 2$, the flow is assumed to be subcritical and further flow integration proceeds in the same manner as discussed previously. If $ICRIT(1) = 1$, the flow is assumed to be supercritical and control is transferred to SPRCRT1. Subroutines UPRINIT and SPRCRT1 compute the initial flow solution on the upper surface. The varying parameter for flow integration is CYDU. Decision point 6 is concerned with determining a value for CYDU so that

the velocity gradients are continuous through the sonic point. The graphed output of this iteration is shown in Figure 8. A value of $CYDU = 1.074974$ determines continuity of the velocity gradient through the sonic point and is a satisfactory solution for decision point 6.

Once the initial solution has been completed, calculation of the flow integration is undertaken for the upper surface including the effects of the shock foot. The appropriate value of $CYDU$ has already been determined in subroutine `UPRINIT` and the flow should return to near free-stream values if the stagnation point and the shock location have been chosen judiciously.

In some cases it may be desirable to modify the flow solution during some intermediate step. The velocity distribution along y which is output from one step may not be appropriate, and some adjustment of the y -component velocity calculated near the airfoil surface may be made by using a Lagrangian or a parabolic curve fit along the y coordinates.

Once again, decision point 5 is encountered and since both upper and lower surfaces have been computed, control can be transferred to subroutine `DWNSTRM`. Subroutine `DWNSTRM` is concerned with the calculation of downstream flow conditions. If the value of SL (the shock location on the upper surface of the airfoil) is correct, flow will return to near free stream values. If this value is incorrect, subroutines `SPRCRT2` and `DWNSTRM` must be reiterated with varying values of SL . The results of such an iteration process are shown in Figure 9. The downstream flows based on two shock locations should bracket the free-stream value ten chord lengths downstream from the body ($P/P_\infty = 1$ at $x/c = 10$). As shown in Figure 9, the exact shock location lies between $x/c = 0.57$ and 0.58 .

When the downstream flow conditions most nearly approximate free-stream values for the upper surface, parameter $CYDL$ can be varied for the lower surface to find the value which most nearly approximates free-stream flow conditions downstream of the airfoil. In this case, subroutines `LWRINIT`, `SUBCRT1`, `SUBCRT2`, and `DWNSTRM` are iterated to find a value for

CYDL which most nearly approximates free-stream conditions downstream of the airfoil. The results of this iteration process are shown in Figure 10. The downstream flow conditions most nearly approximate free-stream values at $CYDL = 0.8131$, and this value of $CYDL$ is chosen to compute the lower surface flow conditions.

There is one remaining step in the solution process, namely, to check the calculated pressure distributions and determine whether the Kutta condition is met at the trailing edge. The upper and lower surface pressure distributions are shown in Figure 11. Since the pressures calculated at the trailing edge for upper and lower surfaces have less than 3-percent error, the assumed stagnation point is correct. If these pressures had not matched at decision point 9, a change would have been required for the stagnation point and the solution process would proceed again from decision point 2.

The upper surface pressure distribution depends greatly on the value of β , the oblique shock angle of the shock foot. The shock location moves forward with decreasing values for β . In this particular example, a change of entropy was allowed through the shock wave and the angle of β was assumed to be 70 deg.

Other Airfoils

The procedure for calculating the transonic flows over other airfoils is basically the same as above except that a change has to be made in subroutine ARFL. An analytic function does not exist for airfoils other than NACA 4-digit series, and some method of airfoil representation must be used. The method used for this program is the spline fit (see Appendix A). The method requires a given set of data points and the first derivatives at the beginning and end points of that set. The coordinates of the airfoil should be very accurate for a smooth curve fit. It is possible to find an airfoil shape with a smooth second derivative fit by varying the beginning and end slopes of the airfoil.

Figure 12 shows the fitted curve for a particular airfoil, and a plot of the second derivatives for this curve. The smooth fit for the second derivatives ensures that the airfoil curvature is pretty well represented.

APPLICATION OF INTERACTIVE GRAPHICS

The subroutines previously described have been incorporated into an interactive graphics program so that program execution can be accomplished most efficiently. The interactive graphics program has been written with the help of Graphic Pac, an NSRDC-developed software package for use with graphics facilities.* The Graphic Pac features include virtual memory data management for both graphic and nongraphic data and a comprehensive collection of interactive facilities; program control is modified during execution by the use of subroutine WAITE. When a call is made to this subroutine, execution stops and the program awaits input from an attention source. Attention sources are the light buttons and text entities which appear on the screen, and these may be signalled by the light pen.

When Graphic Pac is used, all subroutines have to be compiled into a relocatable binary format by PRELOAD, an NSRDC-developed utility.** Once the graphics program and the subroutines have been compiled by PRELOAD, they are loaded into a new task format by TSKLOAD, another NSRDC-developed utility program. It is the TSKLOAD format which is executed. When this program is loaded by using IGSGO, it makes nominal demands on the CDC 6700 computer. The control cards needed to create the taskload file are shown in Figure 13, and those required to make a graphics run are shown in Figure 14.

*Reported informally in NSRDC Technical Note CMD 42-28 (Graphic Pac - A Subroutine Package for Interactive Graphic Application Programming), August 1973.

**Reported informally in NSRDC Technical Note CMD 51-72 (PRELOAD - A Binary Deck Library Loader for the CDC 6700 Computer), October 1972.

The CDC 6700 central processor should be specified to compile and load the program most efficiently. During loading, the program uses approximately 400 CPU sec, has a field length of 110000 Octals, and resides in central memory for about 1 hr. During execution, the program has a field length of 20000 Octals.

The structure of an interactive graphics program is somewhat different from a program used in batch processing. In order to have maximum control over the program and to allow input changes when necessary, there are many points in the program where program execution pauses and waits for a signal from one of the attention sources. An attention source can be a light register used to type in new input information or an asterisk used to signal execution of a new batch of coding. The flow chart in Figure 15 indicates the possible paths for program execution. The nodes indicate possible input changes.

Each of the tasks in the program perform a well-defined function. Half of them display information calculated by a MIR subroutine and the other half maintain the screen displays. A brief description of each task is given in Appendix D. The subroutines used by these tasks and their functions are given in Appendix B.

According to Figure 15, there are many possible paths for the program to follow. However, it is not necessary to use all these paths in the solution process. In some cases, a decision box could have been used instead of a node. In order to avoid a complex logic diagram, however, the format of Figure 15 was chosen. This figure at least gives an indication of the versatility of the interactive graphics program which allows many possible paths instead of two or three from a particular program control point.

BASIC FORMAT

Figure 16 gives the basic format for the graphic output of a step. Most of the screen display is given to the plot of currently computed output. Sometimes two plots may appear in this area of the screen. If for any reason at all, it is impossible to perform the integration

at this step, a large X will cover the graph display; if only a partial integration is possible, the message INTEGRATION INCOMPLETE will flash on the screen. There are two columns of light registers in the lower right-hand corner of the screen; the first gives information on flow conditions at the currently computed step and the second contains the input variables. The variables are light pen detectable, and the values in them can be changed. A current value can be erased and replaced with a blank by touching a light register with a light pen and depressing the handle of the pen. A new value can then be inserted by typing it in on the keyboard and pressing the keyboard release button. When the COMPUTE button at the bottom of the column is touched, the program will attempt to execute the step with the current input. The asterisks surrounding the airfoil in the lower left-hand corner signify the steps of the flow solution; they are coded in Figure 16. The currently computed step is identified by a flashing asterisk. The asterisks will appear only when the program is ready to execute the program step which they represent. Program control can be transferred to any other step by signalling the appropriate asterisk with the light pen. The program can be terminated at any time by using the light pen to signal the STOP button in the far left-hand corner.

The input to the graphics program consists of 32 flow solution parameters and a maximum of 40 airfoil data points and the first derivatives at these data points. These airfoil data points and their first derivatives have been chosen to ensure a smooth second derivative curve fit in accordance with Appendix A. A description of the input data is given in Appendix E. Many of the flow solution parameters assume the values suggested in the appendix.

ILLUSTRATIVE EXAMPLE

Just as an illustrative example of flow past an NACA 0015 airfoil was used to describe the MIR program subroutines, an illustrative example of flow past an advanced transonic airfoil will describe the use of IGS. The first display to appear on the screen is that shown in Figure 17.

The four light registers contain the free-stream flow conditions and certain initial conditions:

ALPHA = Angle of attack
MACH NO. = Mach number
YI(UPR) = Location of outermost strip in upper surface
(given in chord length)
YI(LWR) = Location of outermost strip in lower surface
(given in chord length)

If these flow conditions are satisfactory, control may be transferred to the first step in the flow solution by signalling the light button PROCEED.

The first step in the solution is the calculation of the upstream flow conditions. The necessary parameters for the upstream solution are the number of strips used in integration and X00, the distance from free-stream flow conditions to the stagnation point on the airfoil. The parameter NN indicates the number of strips used for the bulk of integration, and NA indicates the number of additional strips used in the vicinity of the airfoil. For greater accuracy, it is recommended that eight strips be used in the vicinity of the airfoil. Figure 18 indicates the screen display corresponding to this solution.

The flashing light ahead of the airfoil in the lower left-hand corner of the screen display indicates that the upstream solution is ready for execution. When the COMPUTE light button at the bottom of the second column of light registers is signalled, this step will be executed by using the input values currently in the light registers. The computed values of YSO and DE will be displayed in the first column. These values should be less than 0.1. The graphic output shows Y versus M, the velocity profile at the final station of upstream integration, and M_0 versus X, the variation of Mach number along the stagnation streamline. These two graphs are characteristic of an appropriate solution.

If the computation of the upstream solution is complete, the program may proceed to the stagnation solution. The necessary parameters used to

iterate on this stagnation solution are XS, the X-coordinate of the stagnation point, YSO, the distance that the stagnation streamline is perturbed by the airfoil, and DVOO(I), the cross velocity gradient used in the upstream solution. The screen display is shown in Figure 19.

If DVOO(F), the cross velocity gradient calculated at the particular stagnation point, does not agree with DVOO(I), then DVOO(I) must be changed to the newly calculated value, and the upstream solution must be recalculated. By signalling the light far to the left of the airfoil, control is transferred back to the upstream solution which is computed by using the new DVOO(I). When the streamline geometry seems reasonable and the cross velocity gradients agree at the stagnation point, the program may proceed to the step which determines flow criticality on either the upper or lower surface. For example, consider the flow on the upper surface. Control is transferred to this step by signalling the light just above the leading edge of the airfoil.

The screen display shown in Figure 20 determines the type of flow present on the upper surface. In this case the Mach number reaches a value of 0.96 in a relatively short distance, and so it is safe to assume that supersonic flow is present on the upper surface. By signalling the SUPERSONIC light button, program control is transferred to the next step which computes the initial conditions on the upper surface.

The screen display of Figure 20 also indicates the light button LAGRANGIAN. When it is signalled, the normal velocity component at the innermost strip at the initial step will be corrected using a Lagrangian curve fit. The light button LAGRANGIAN will disappear and the light button PARABOLIC will appear in the same area on the screen. Similarly, when the latter is signalled, the normal velocity component at the innermost strip at the initial step will be corrected using a parabolic curve fit. If neither light button is signalled, the normal velocity component at the innermost strip will not be modified during the flow integration.

The necessary parameters for calculation of the initial solution are XA, the initial point of flow integration, and CYD, which determines the initial velocity profile shape. The screen display of Figure 21

illustrates the iterative process used to satisfy the flow conditions in this step. After an initial point has been chosen, the parameter CYDU is varied until the velocity gradient DUDX is continuous through the sonic point.

The following additional information is included to help proceed to a converged solution. The value of RBUB ($\rho_b V_b$ in Figure 7) should be less than 1.1 and CYDU should be increased until this requirement is met. If CYDU is too large, the velocity gradients will become negative and the flow will become subsonic, prohibiting further integration. If the solution still does not converge, the number of strips NN should be decreased by one. When an appropriate CYD value is chosen and integration is completed, a light above the airfoil will signal that the upper surface airfoil solution is now ready to be computed. Further refinements to the initial solution can now be made or control can be transferred to the next step by signalling the light above the airfoil.

The screen display of Figure 22 indicates the airfoil solution on the upper surface. The location of the shock foot should be chosen so that flow integration may proceed from the initial solution to the trailing edge of the airfoil. If the shock location is chosen too close to the nose of the airfoil, the flow will accelerate to supersonic again after the shock wave, prohibiting further integration; if the shock location is chosen too close to the trailing edge of the airfoil, the flow becomes over expanded before the shock foot, prohibiting further integration. A careful choice of shock foot will allow integration to proceed to the trailing edge.

If the solution on the upper surface is completed, control may be transferred to the step which determines flow criticality on the lower surface by signalling the light under the leading edge of the airfoil. The screen display for this step is shown in Figure 23. Since the local Mach number is below 0.6 for at least 5 percent of the airfoil surface, it is safe to assume that subcritical flow exists on the lower surface of the airfoil. The program now proceeds to the step which computes the airfoil solution on the lower surface.

The screen display of Figure 23 also shows the light button LAGRANGIAN. Correction to the innermost strip y-component velocity can be made by signalling this light button in the same manner as indicated for Figure 20.

The screen display for the airfoil solution is shown in Figure 24. The parameters for this solution are the same as for the initial solution on the upper surface. If the chosen value of CYDL is too small, the message FLOWS NOT MATCHED will appear where $UB = 0.699485$ now appears on the screen. When the value of CYDL is increased, the value of RBUB will decrease and flow integration may proceed. A particular choice for CYDL will allow integration to proceed to the trailing edge. Further improvements can be made to the airfoil solution or control may be transferred to the downstream solution. The upper surface and lower surface can be computed in any order, but the downstream solution cannot be computed until both upper and lower surfaces are computed.

The screen display of Figure 25 will appear when the light to the right of the airfoil is signalled. A satisfactory solution for this step would be one in which the graph of PO versus X has values fairly close to one, meaning that the computed pressures are fairly close to free-stream pressures downstream. Since control was transferred to this step from the lower surface, the downstream solution considers the flow regime from the slip streamline to the outermost strip on the lower surface. In order to find a solution which will yield free-stream flow conditions in this regime, an iteration must be made on the lower surface airfoil solution and the downstream solution by varying the value of CYDL. Once a satisfactory solution has been found, control may be transferred to the airfoil solution on the upper surface by signalling the light just above the airfoil.

The screen display for the airfoil solution on the upper surface is the same as previously shown in Figure 22. Since both upper and lower surfaces have been computed, control may be transferred to the downstream solution by signalling the light to the right of the airfoil.

Since control was transferred to this step from the upper surface, the downstream solution considers the flow regime from the slip streamline

to the outermost strip on the upper surface. In order to find a solution which yields free-stream flow conditions downstream, an iteration must be made on the upper surface airfoil solution and the downstream solution by varying the value of SL. When an appropriate solution has been found, control may be transferred to the final program by signalling the light which appears on the airfoil.

Figure 26 illustrates the screen display of the final program step. The validity of the solution can be checked by inspecting the pressure distributions computed in the airfoil solution for both upper and lower surfaces. (Pressures on the upper and lower surfaces should match at the trailing edge in order to satisfy the Kutta condition.) Inspection of Figure 26 shows that this condition has not been met (there is a 10-percent discrepancy between trailing edge pressures) and that further action should be taken to correct this situation. Program control can be transferred to the stagnation solution for the selection of a new stagnation point. Then the whole solution procedures described above should be repeated.

Solutions exist for each of the four major iteration processes which have been presented. Failure to find a bracketed solution for a particular iteration process indicates the need for further refinement in the strip arrangement of the flow field. Computational experience further indicates that special attention should be given to spline fitting the leading edge of the airfoil to ensure that the curvature of the airfoil is smoothly continuous in the region of the sonic point to avoid difficulties in attaining converged solution.

CONCLUDING REMARKS

The use of interactive graphics enables a practical application of the method of integral relations to solve transonic flow problems past lifting airfoils. For instance, 5 to 10 min of actual computer time and about 1 hr of interactive graphics time are required to determine the converged solution, i.e., pressure distribution about the given airfoil for a given flow condition. With experience, these times could be reduced still more.

Experience at NSRDC during the development of the application indicates that care must be exercised in the strip arrangement of the flow field and in the spline fitting of the airfoil coordinates, particularly near the leading edge or sonic point area in order to ensure numerical stability and accuracy.

The use of interactive graphics for this program is minimal. Further refinements might include hard copies of the output from the Cal Comp plotter. The only output now saved is that on the line printer. Use of light registers might also make it possible to keep track of previous guesses on a particular iteration.

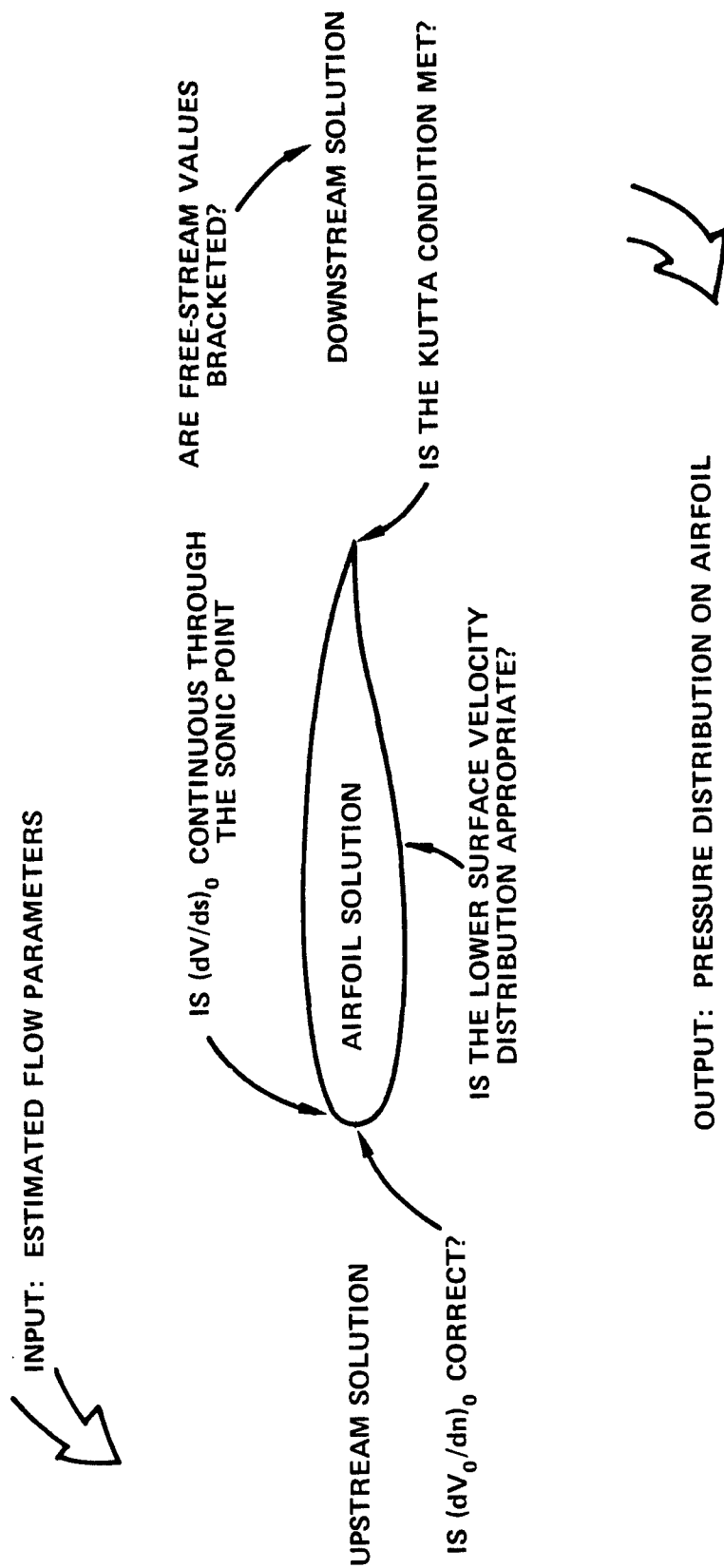


Figure 1 - The Solution Procedures for Transonic Flow Problems

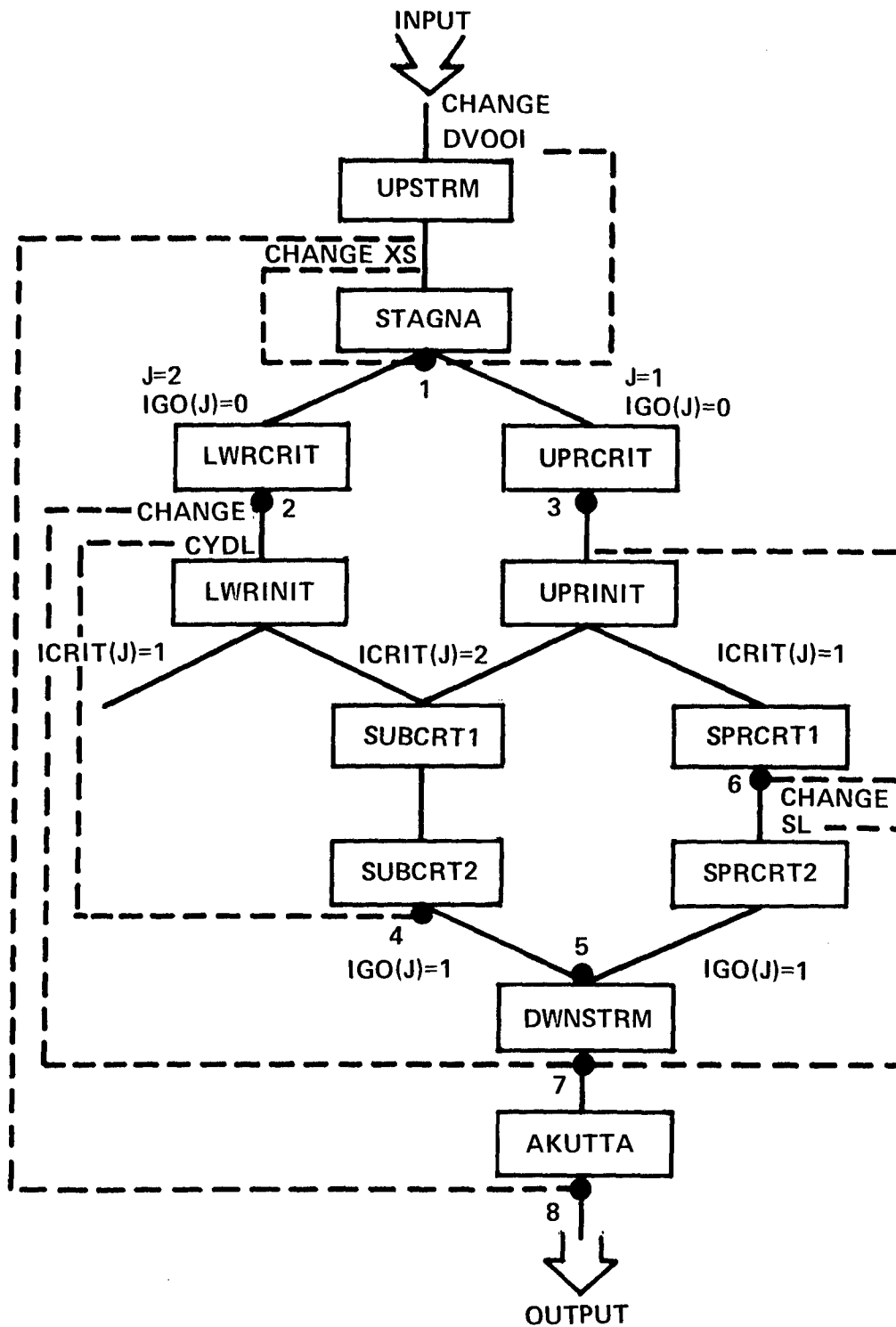


Figure 2 - Flow Chart for the More Important Subroutines

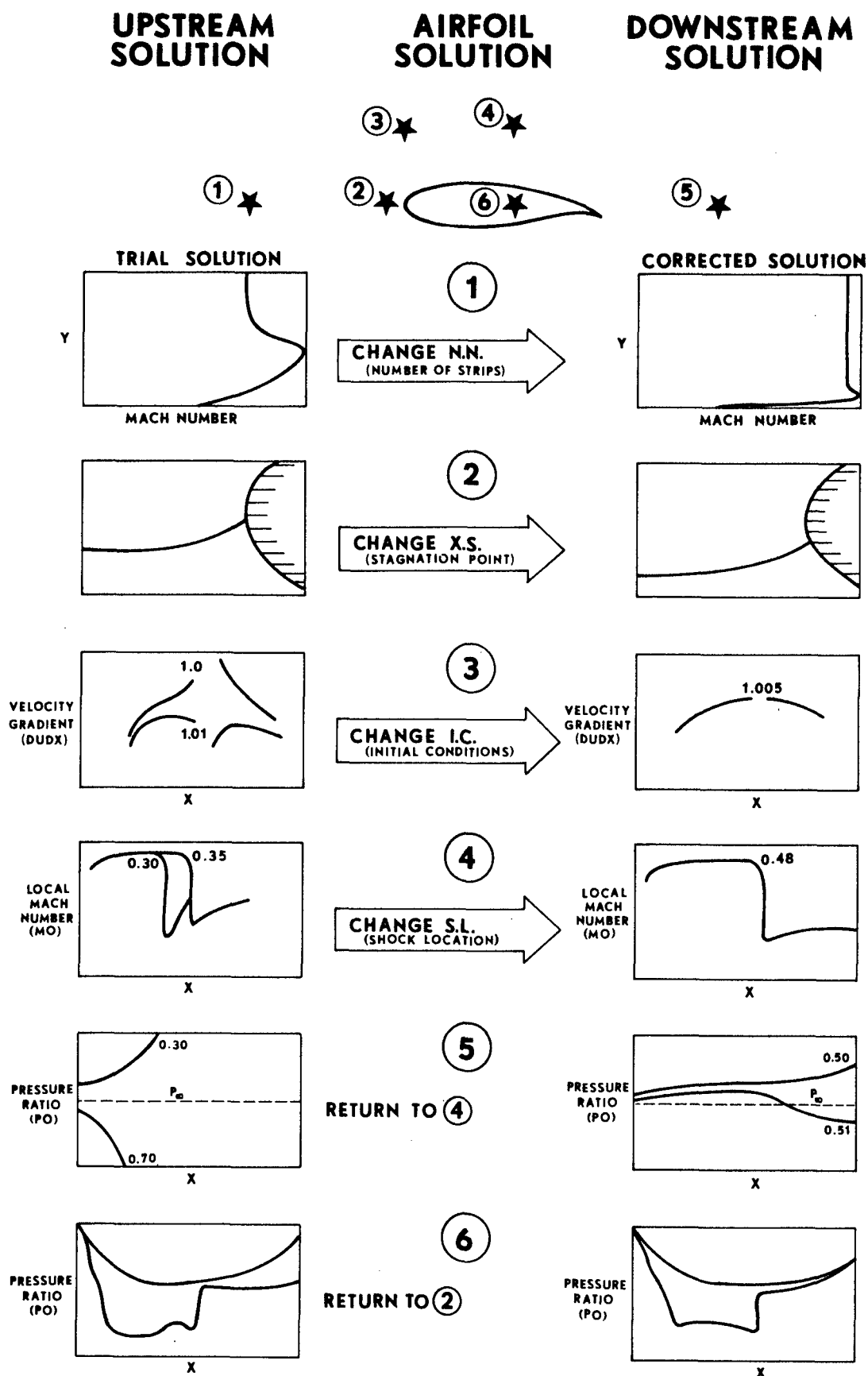


Figure 3 - Overview of the Solution Process

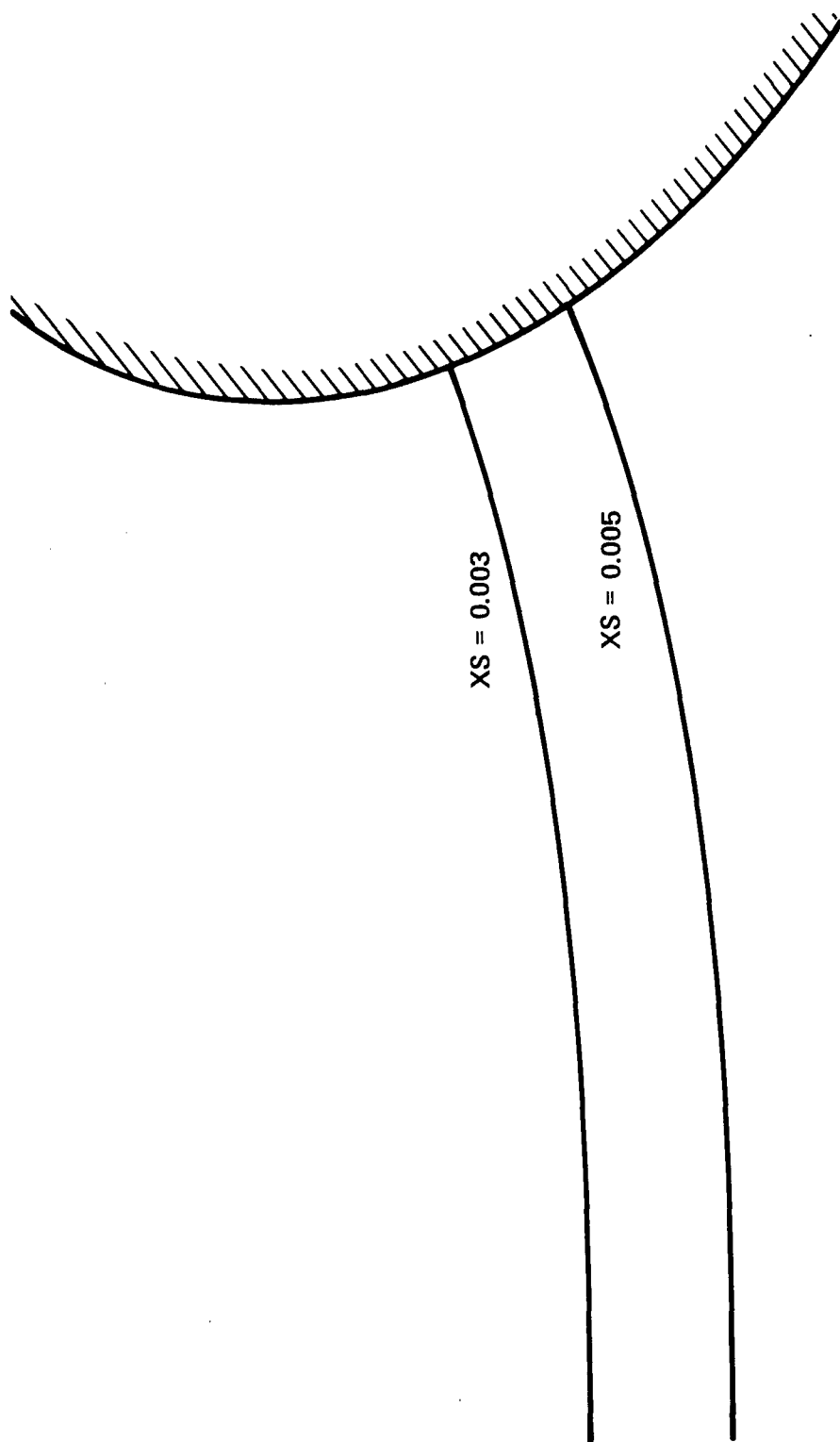


Figure 4 - Choice of Stagnation Point

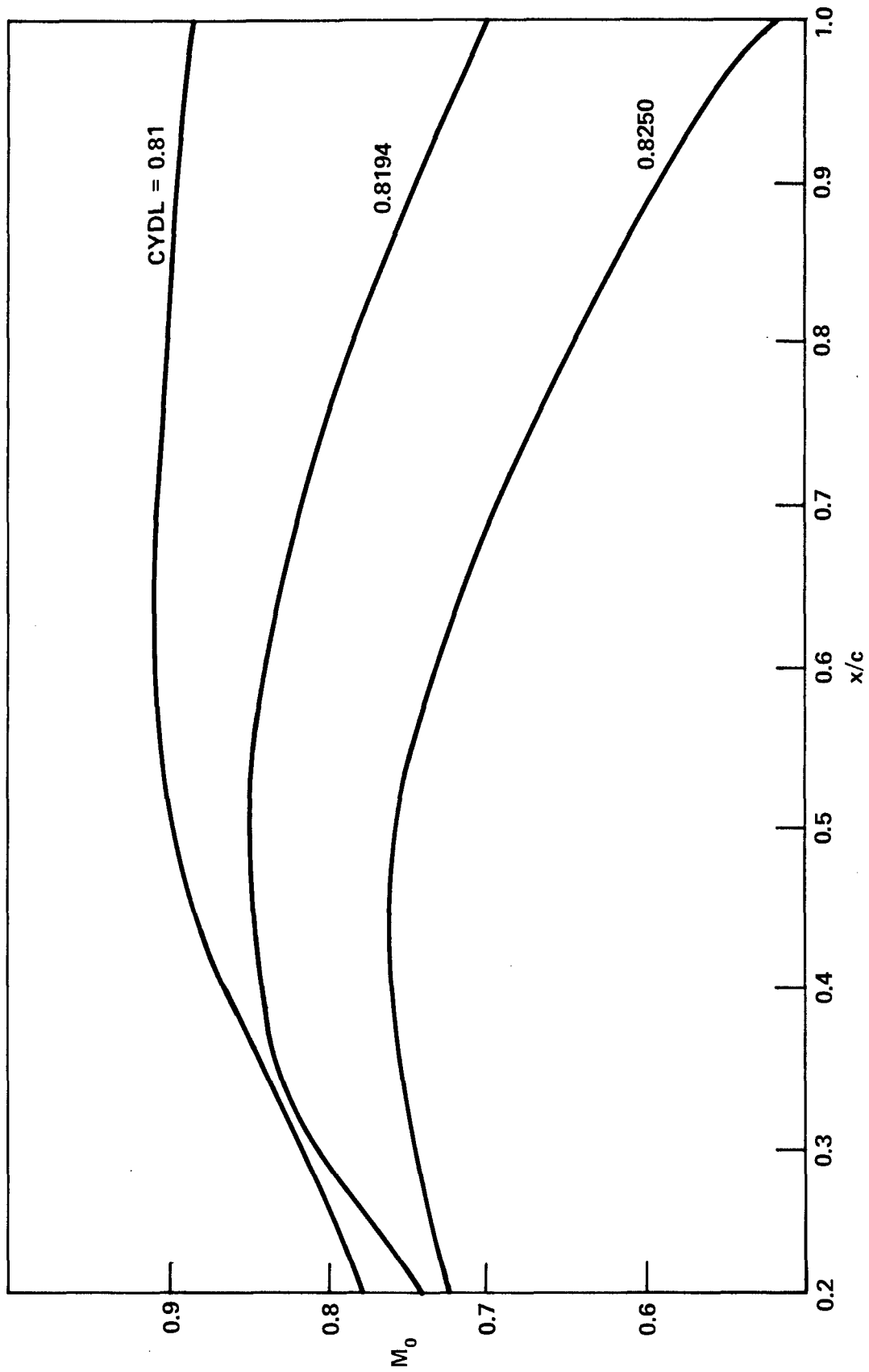


Figure 5 - Choice of CYDL for Lower Surface Flow

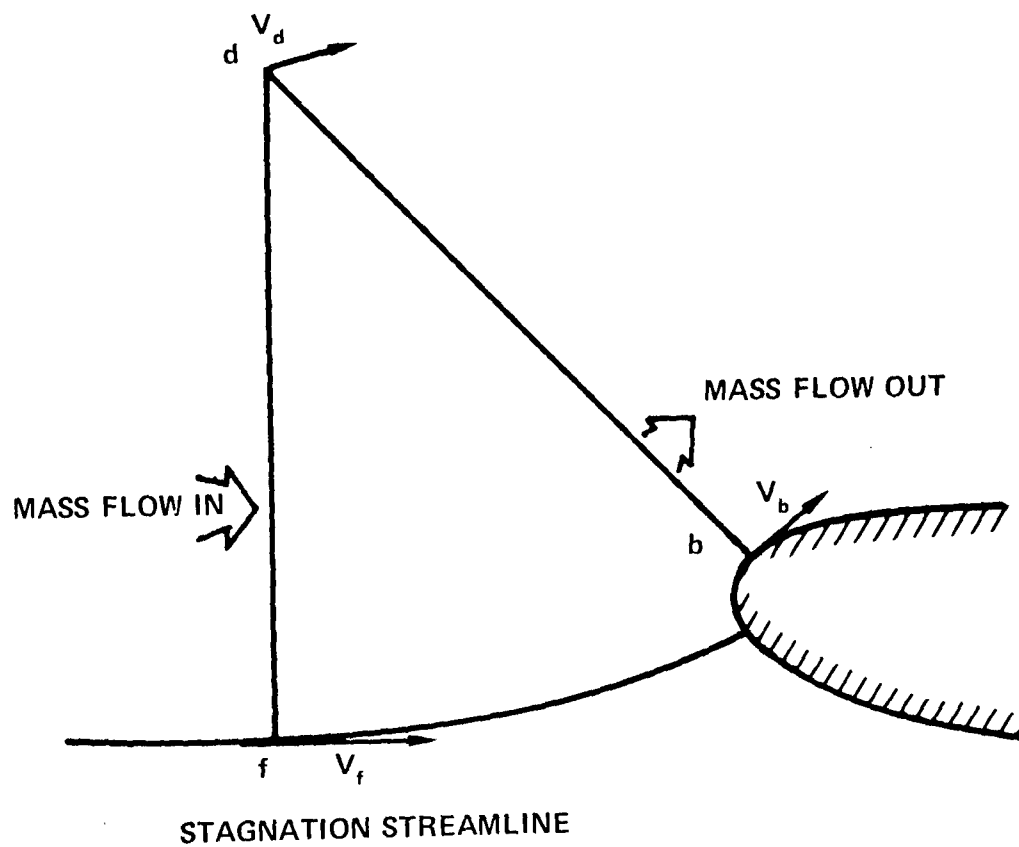


Figure 6 - Control Volume Used to Determine Initial Velocity on Airfoil Surface

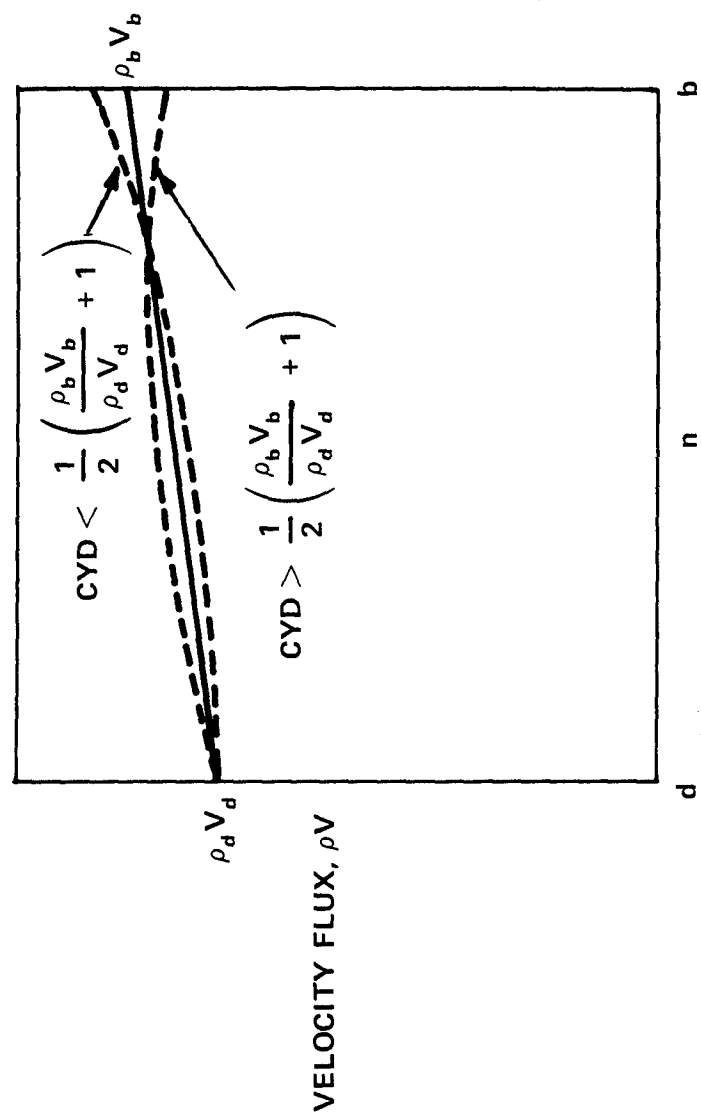


Figure 7 - Effect of CYD on $\rho_b V_b$

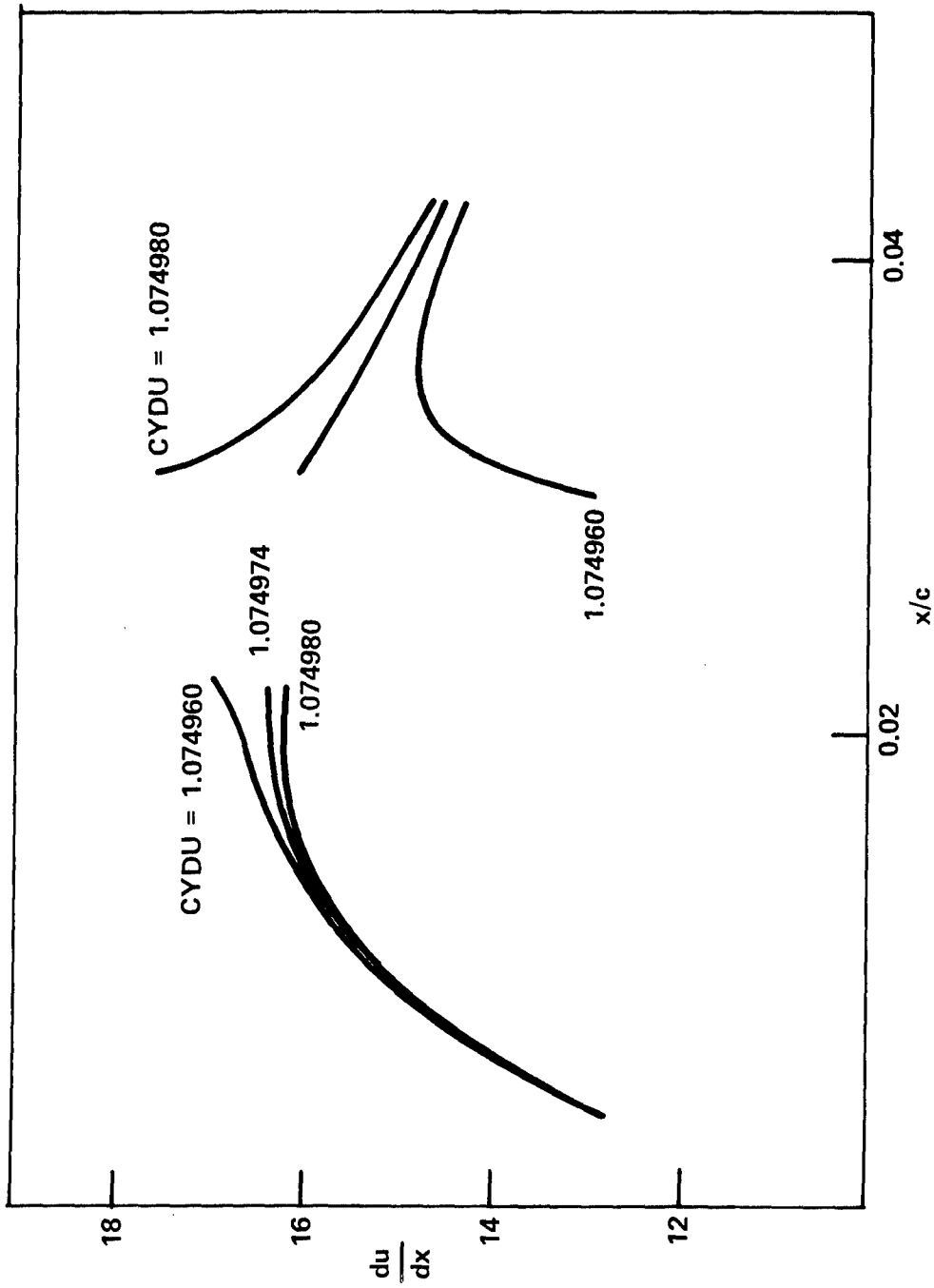


Figure 8 - Choice of CYDU for Upper Surface Flow

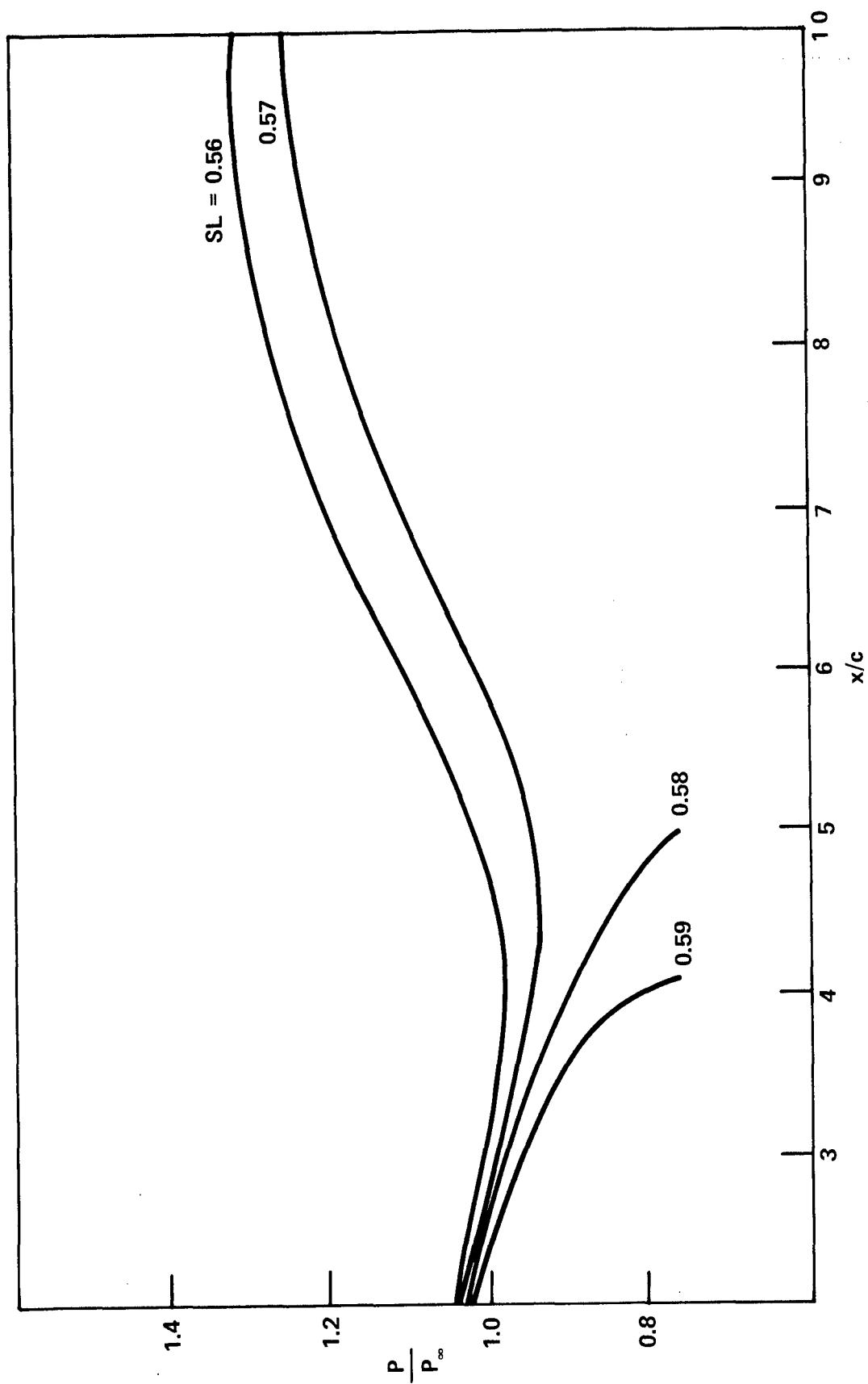


Figure 9 - Choice of Shock Location for Downstream Flow

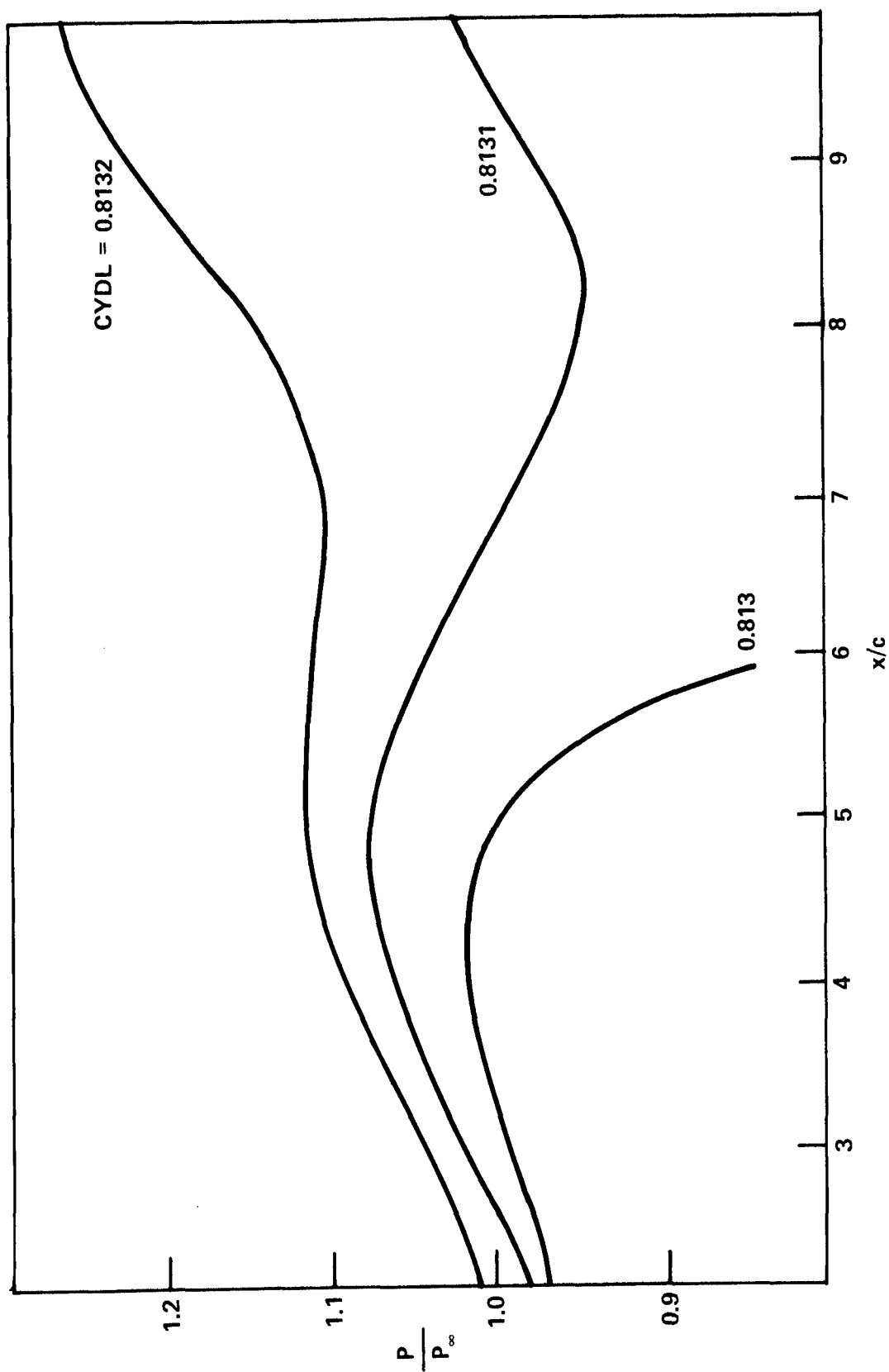


Figure 10 - Choice of CYDL for Downstream Flow

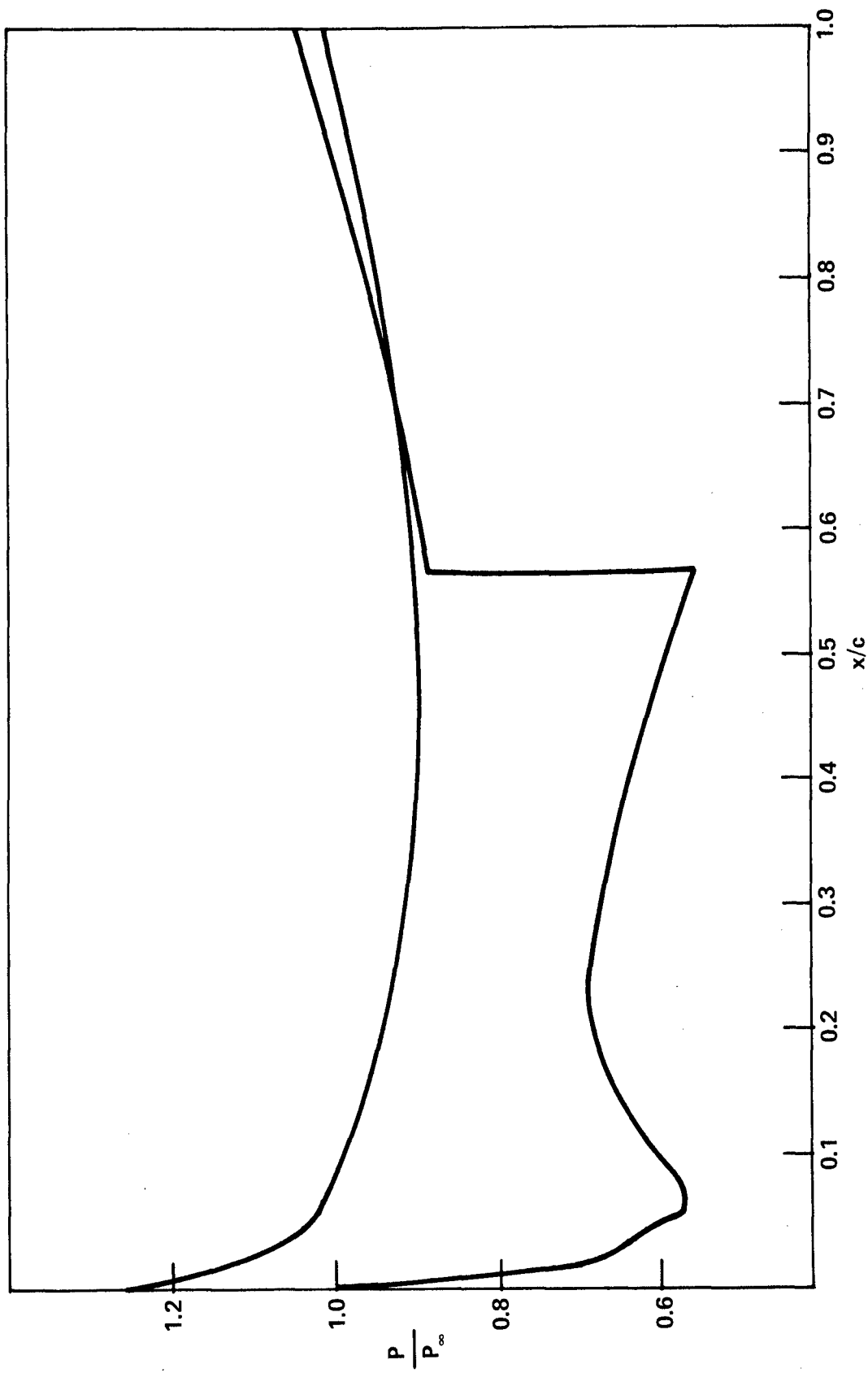


Figure 11 - Check of Kutta Condition at the Trailing Edge

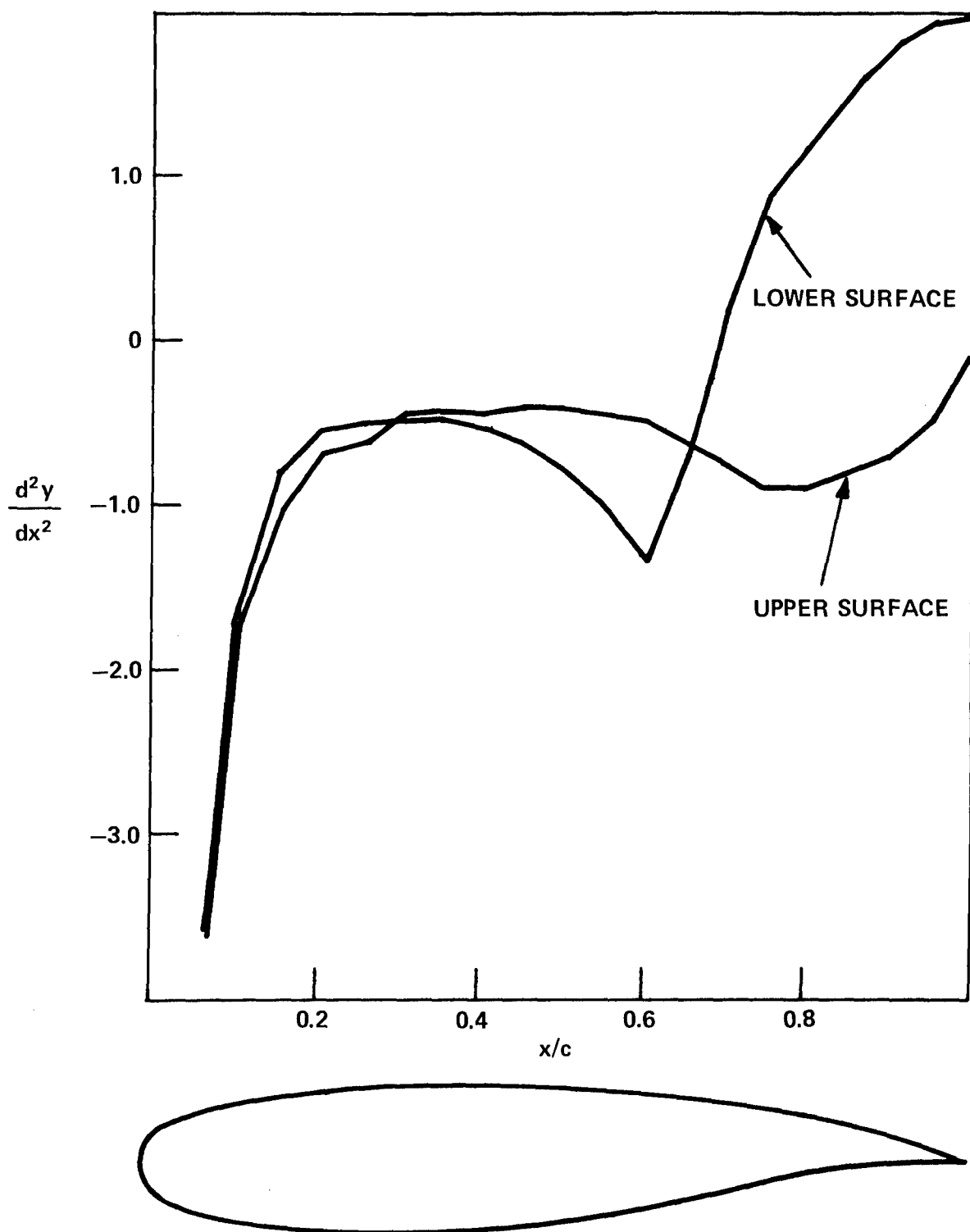


Figure 12 - Second Derivative Spline Fit for an Advanced Airfoil

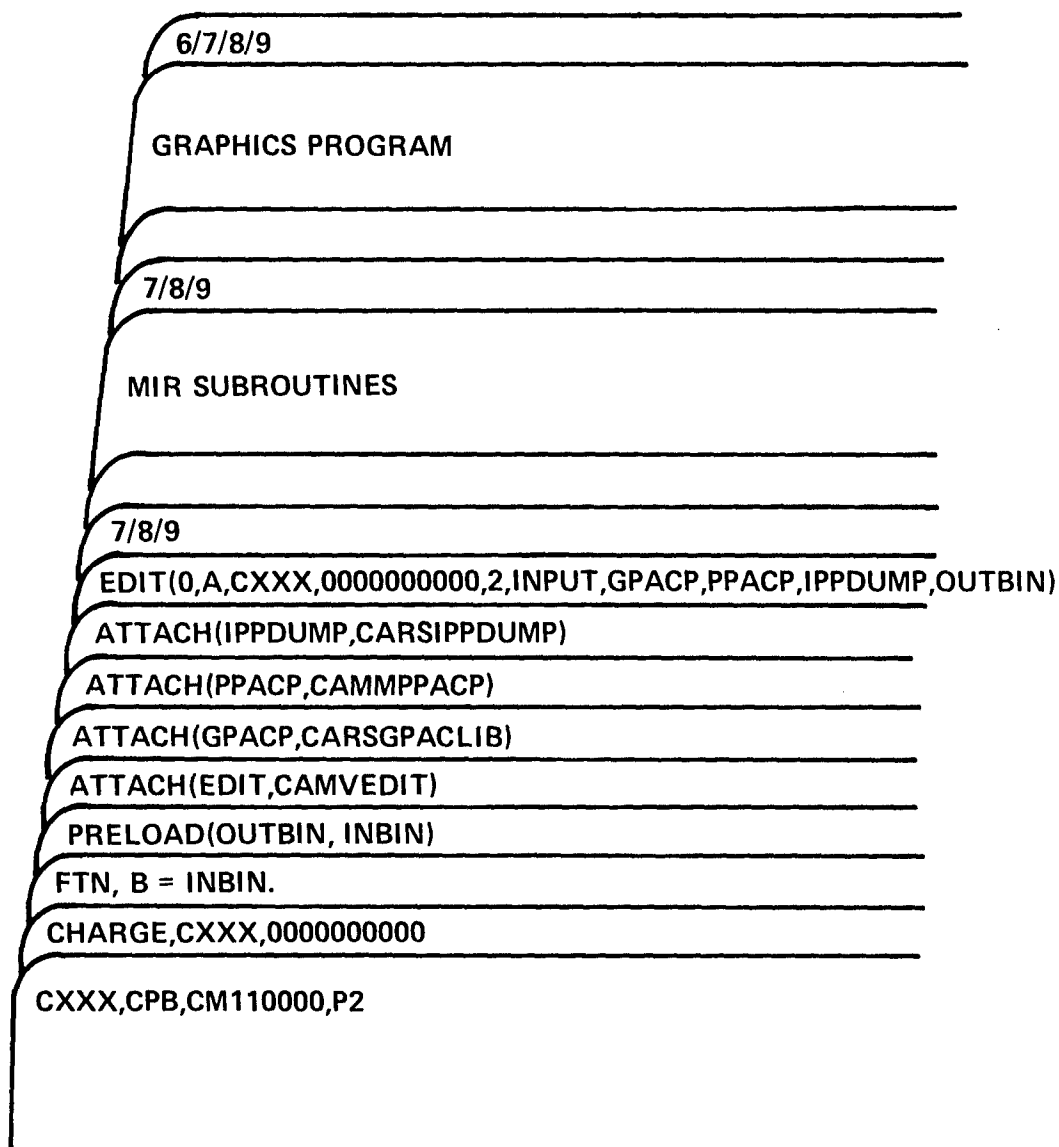


Figure 13 - Deck Setup for Creation of TASKLOAD File

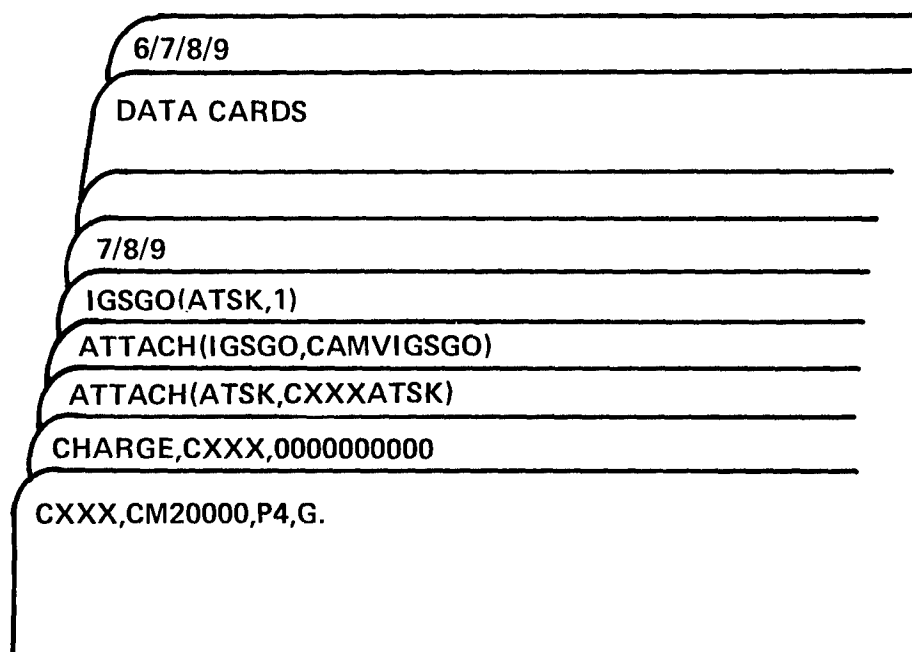


Figure 14 - Deck Setup for Graphics Run

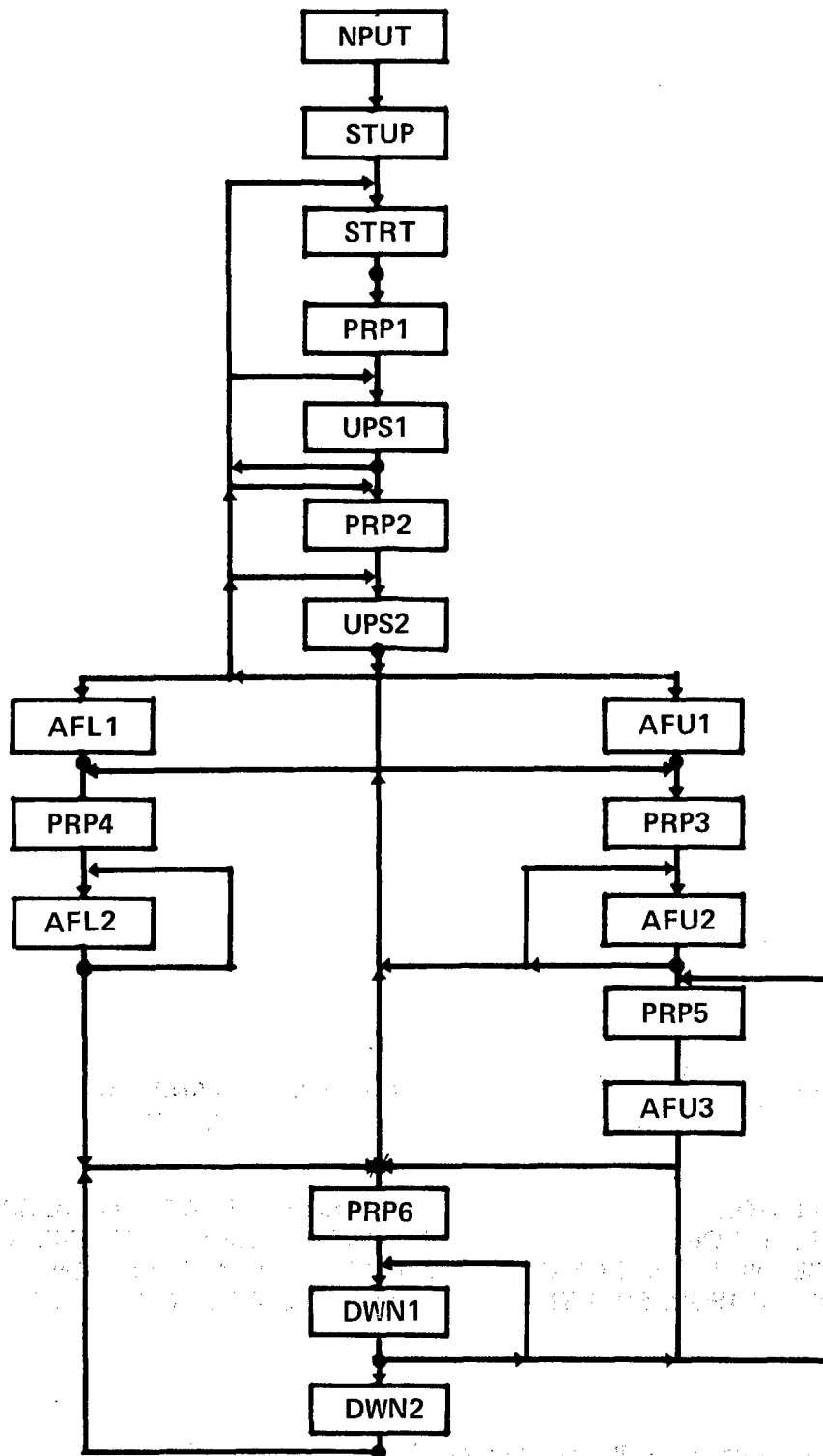


Figure 15 - Flow Chart for the More Important Tasks of the Interactive Graphics Program

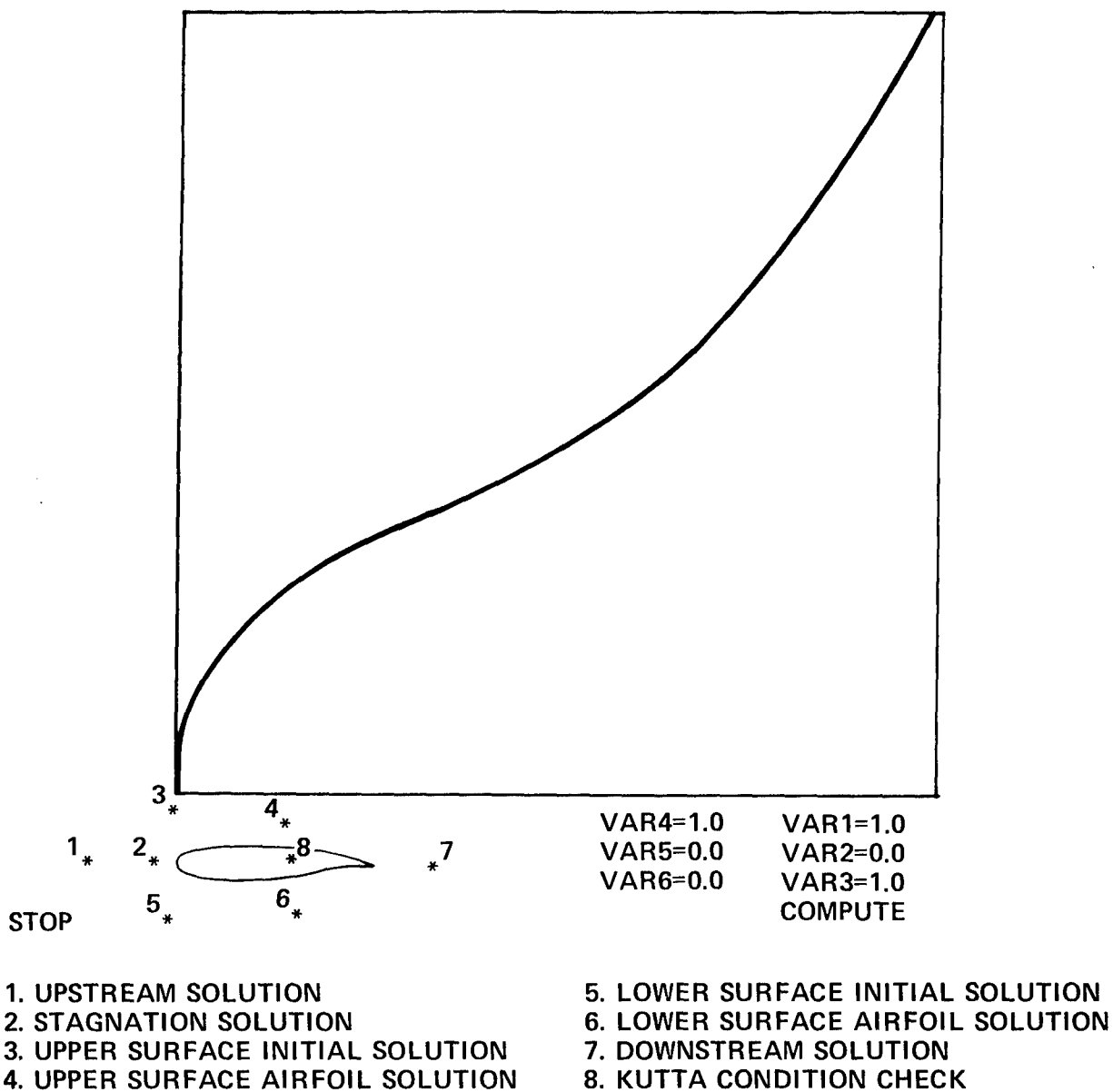
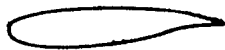


Figure 16 - Basic Format for Screen Displays

STOP



PROCEED

MACH NO.=0.7
ALPHA=1.5
YI(UPR)=7.0
YI(LWR)=7.0

Figure 17 - First Screen Display

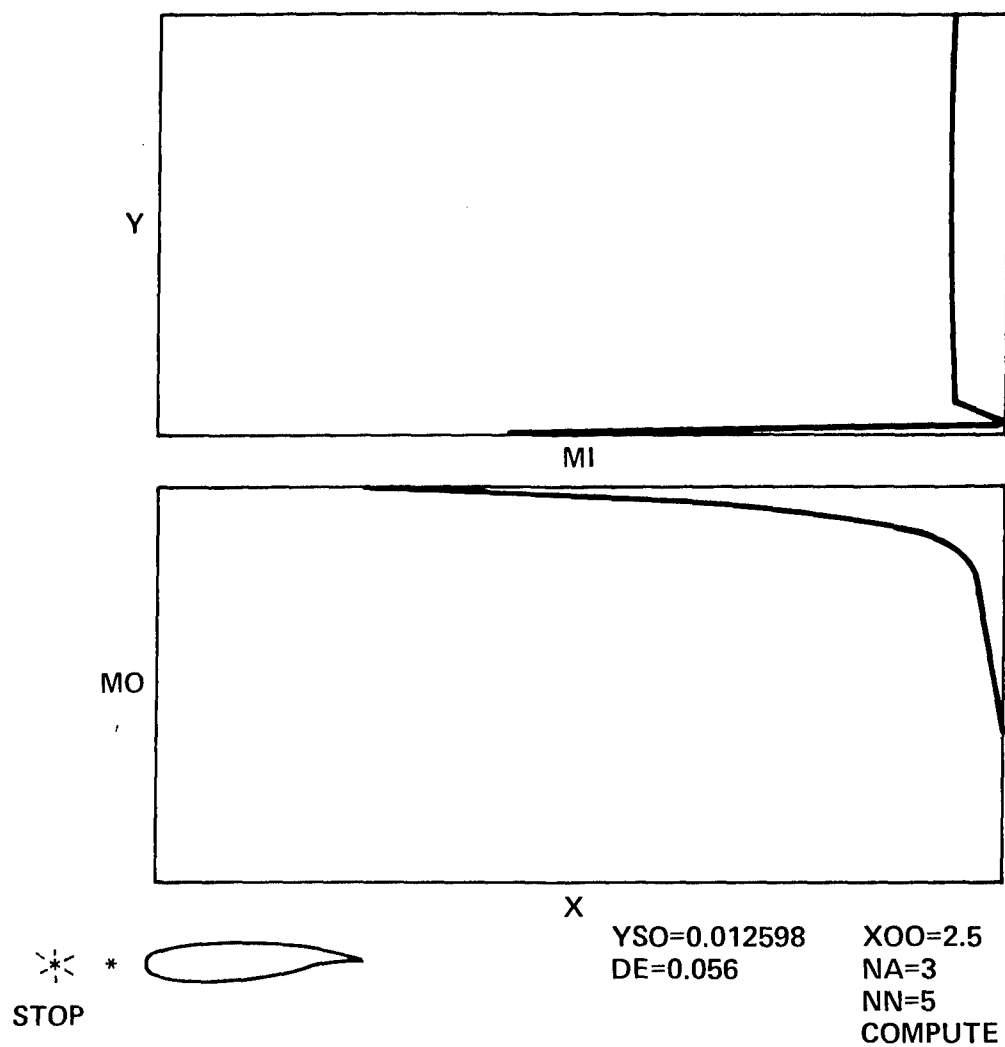


Figure 18 - Screen Display for Upstream Solution

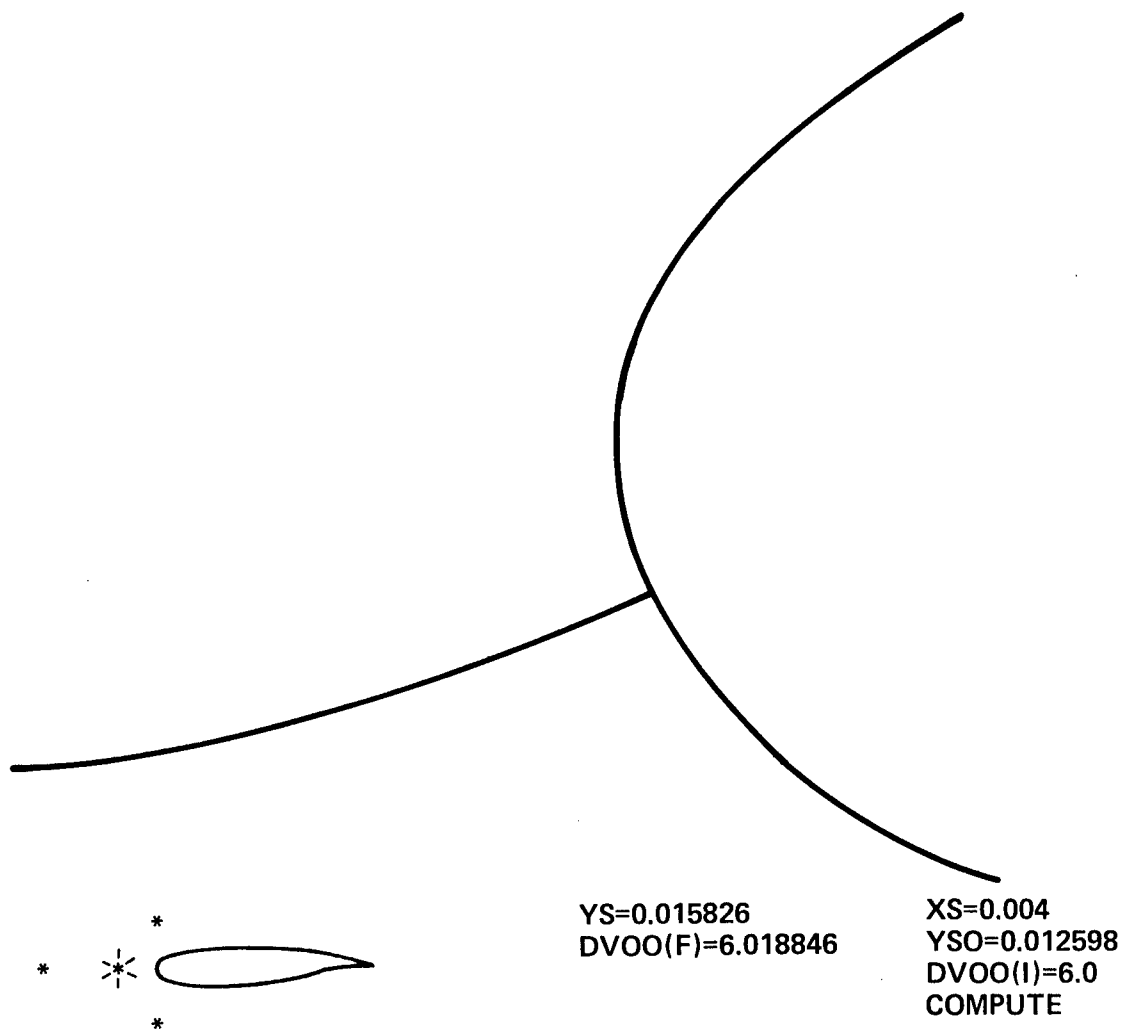


Figure 19 - Screen Display for Stagnation Solution

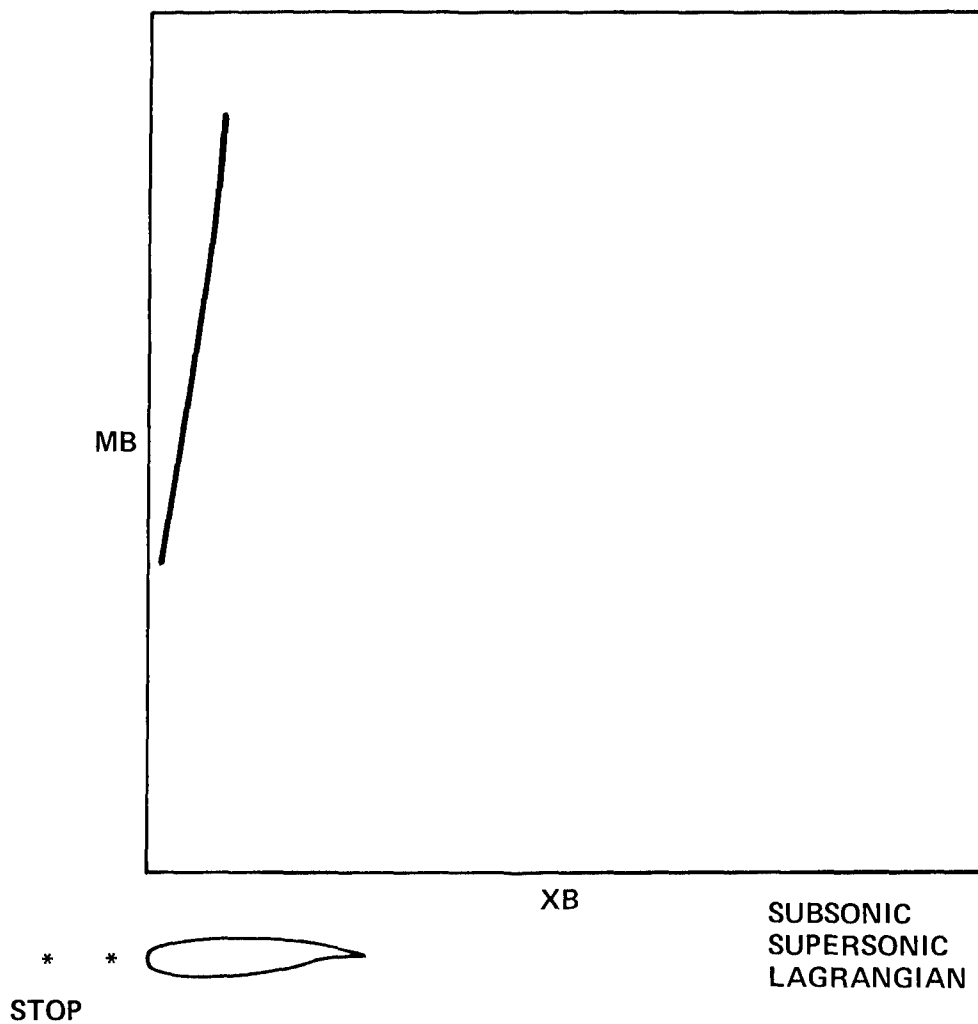


Figure 20 - Screen Display for Flow Criticality on Upper Surface

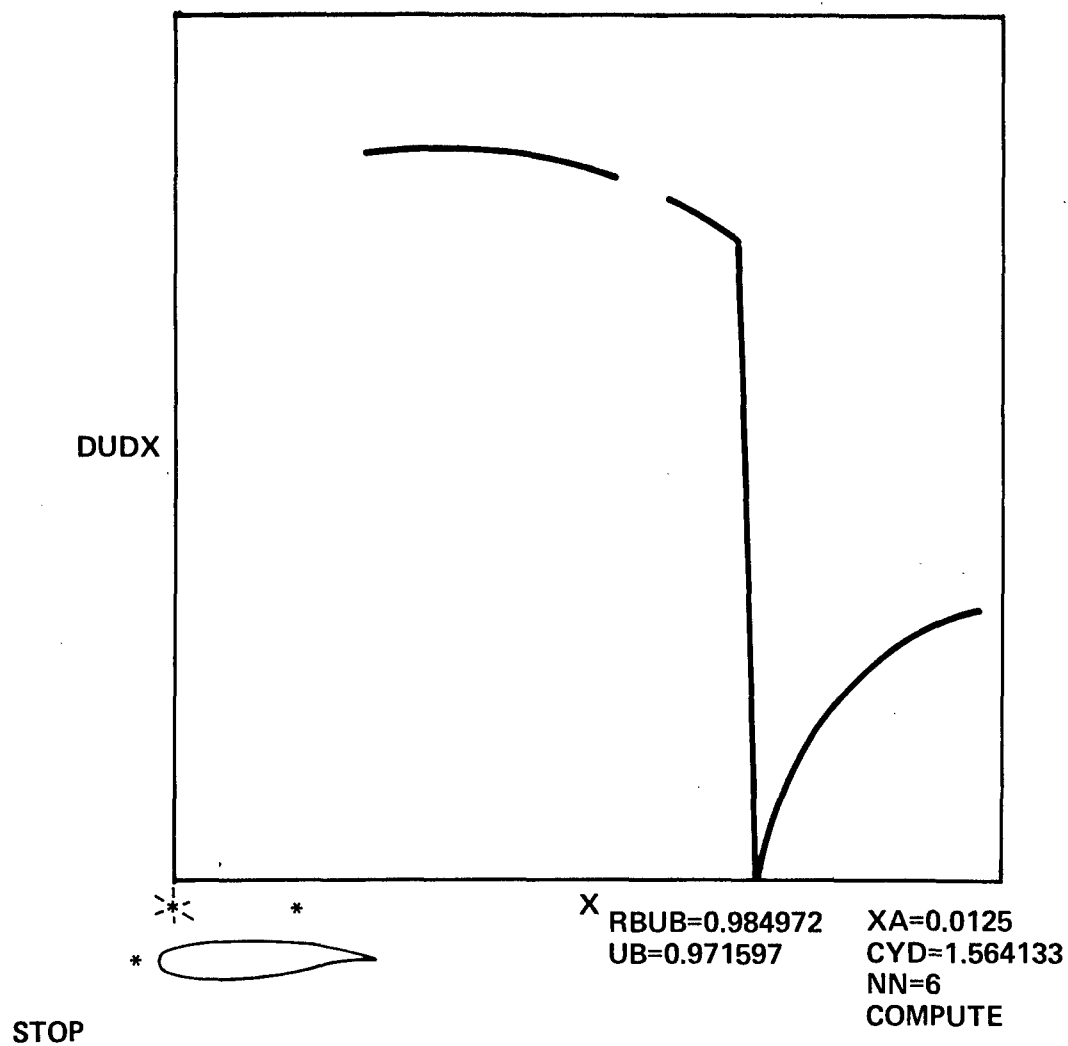


Figure 21 - Screen Display for Initial Solution - Upper Surface

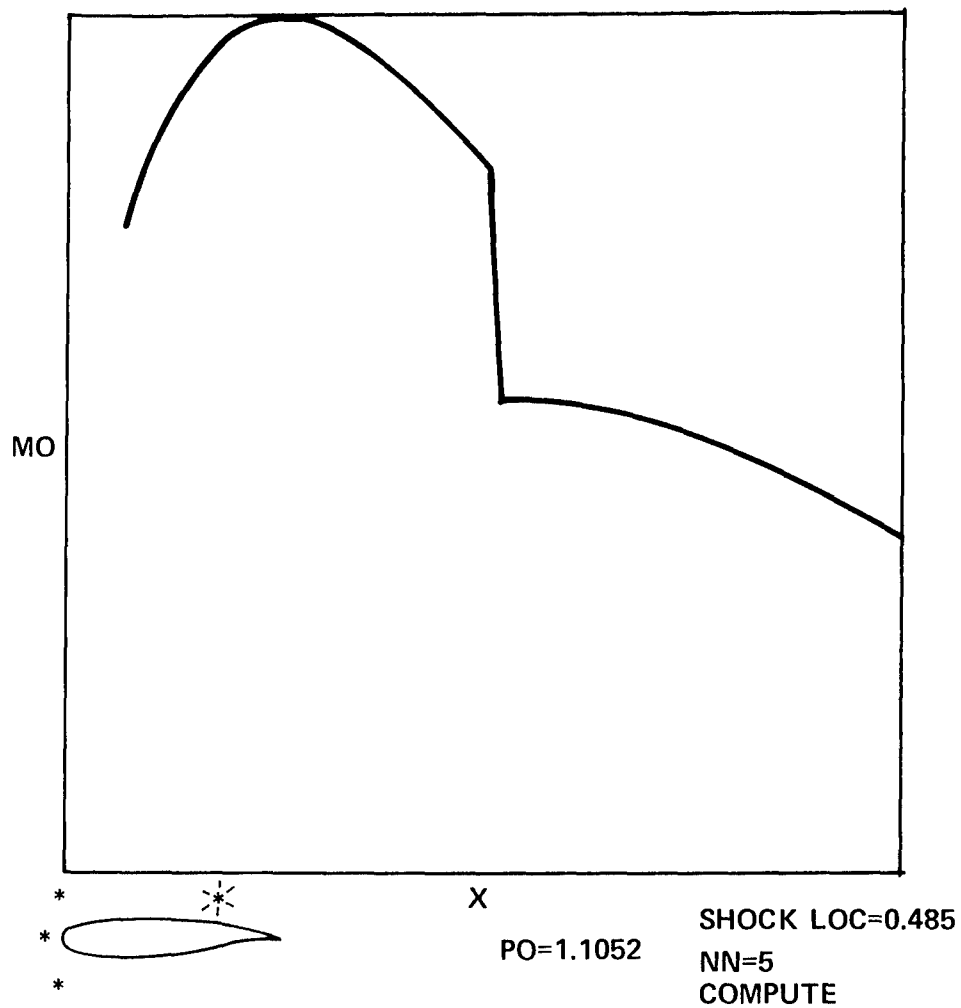


Figure 22 - Screen Display for Airfoil Solution - Upper Surface

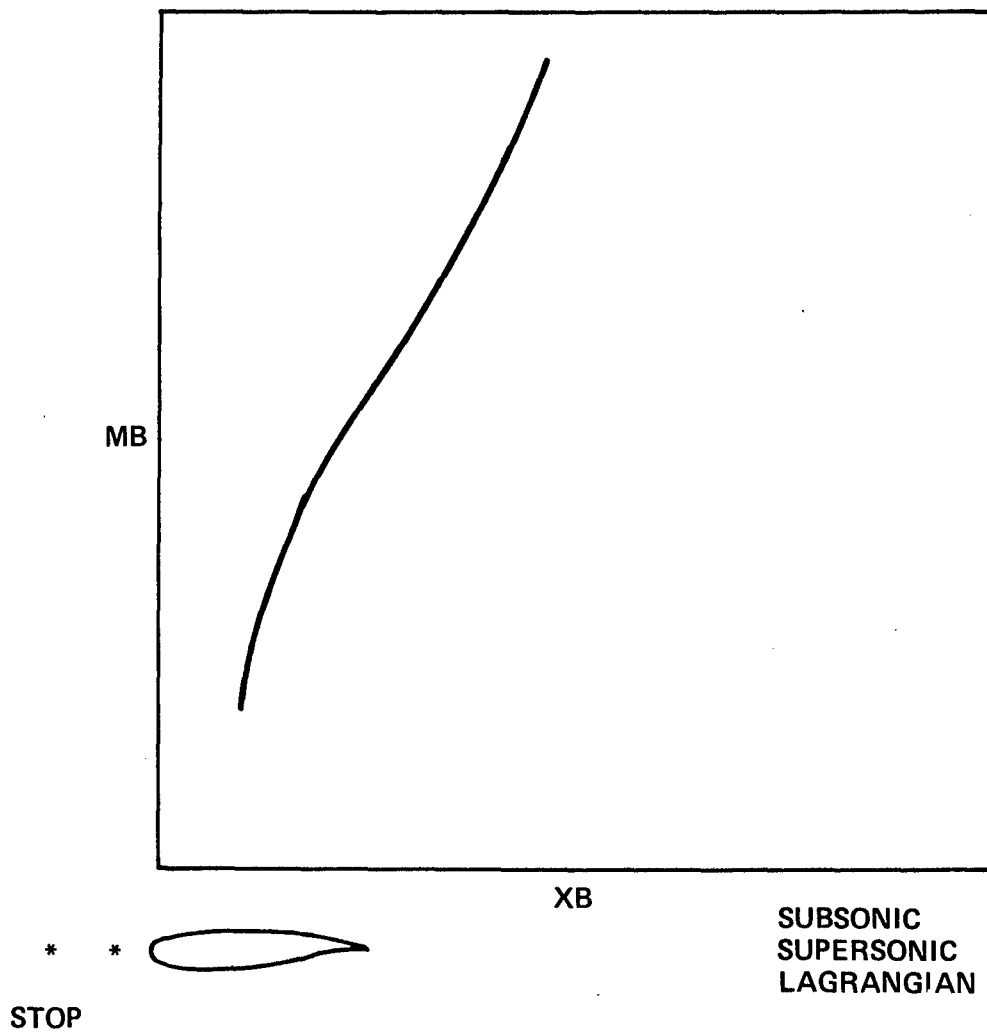


Figure 23 - Screen Display for Flow Criticality on Lower Surface

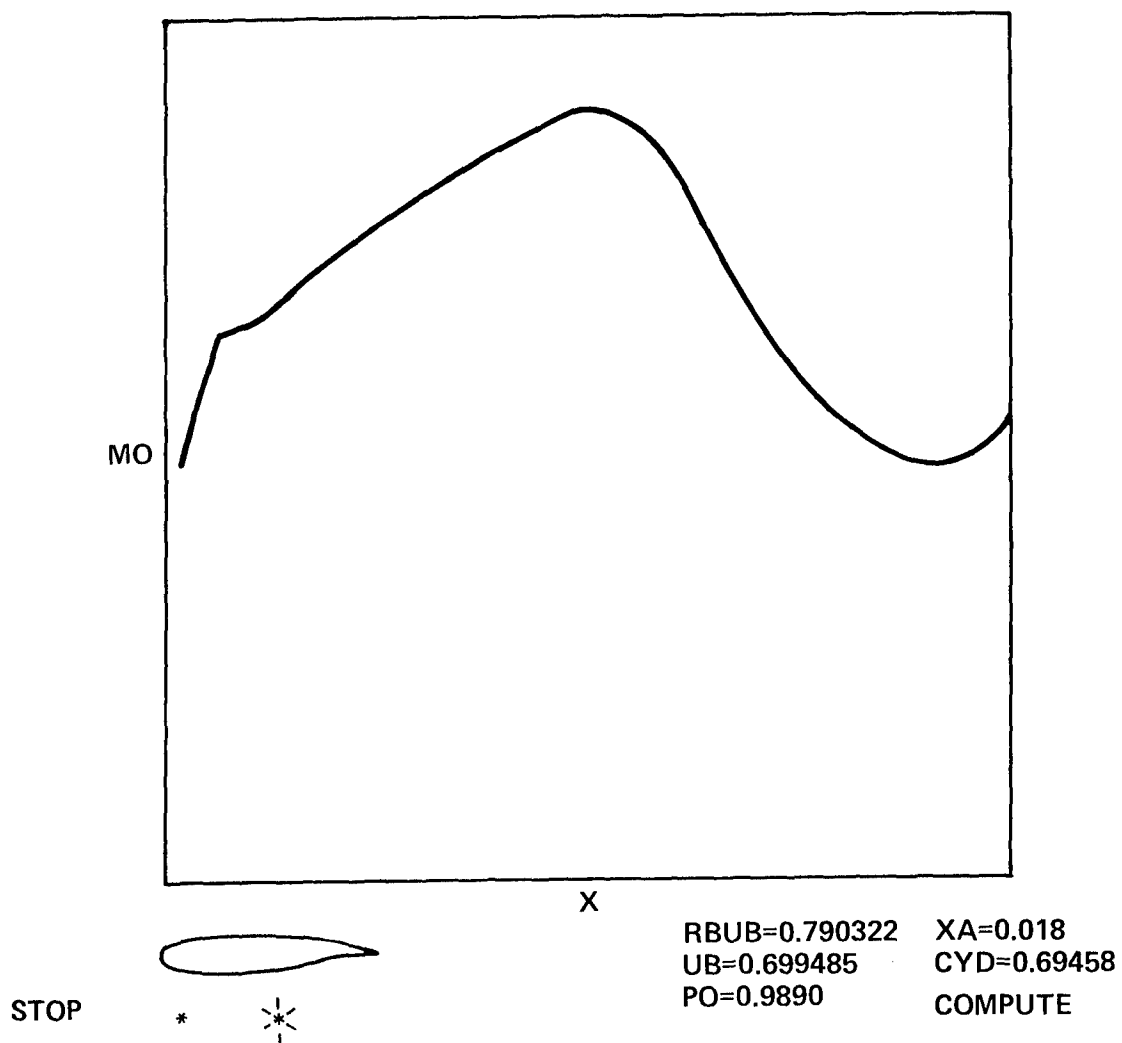


Figure 24 - Screen Display for Airfoil Solution - Lower Surface

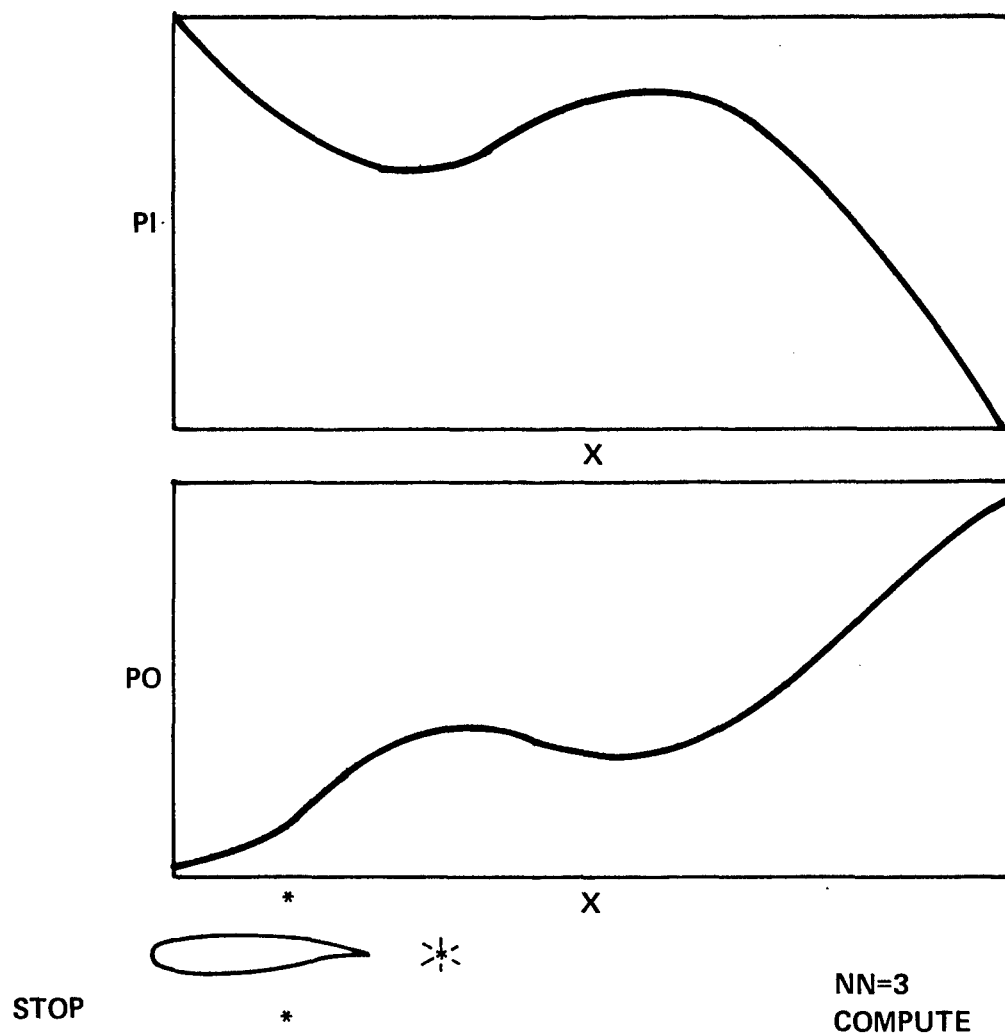


Figure 25 - Screen Display for Downstream Solution

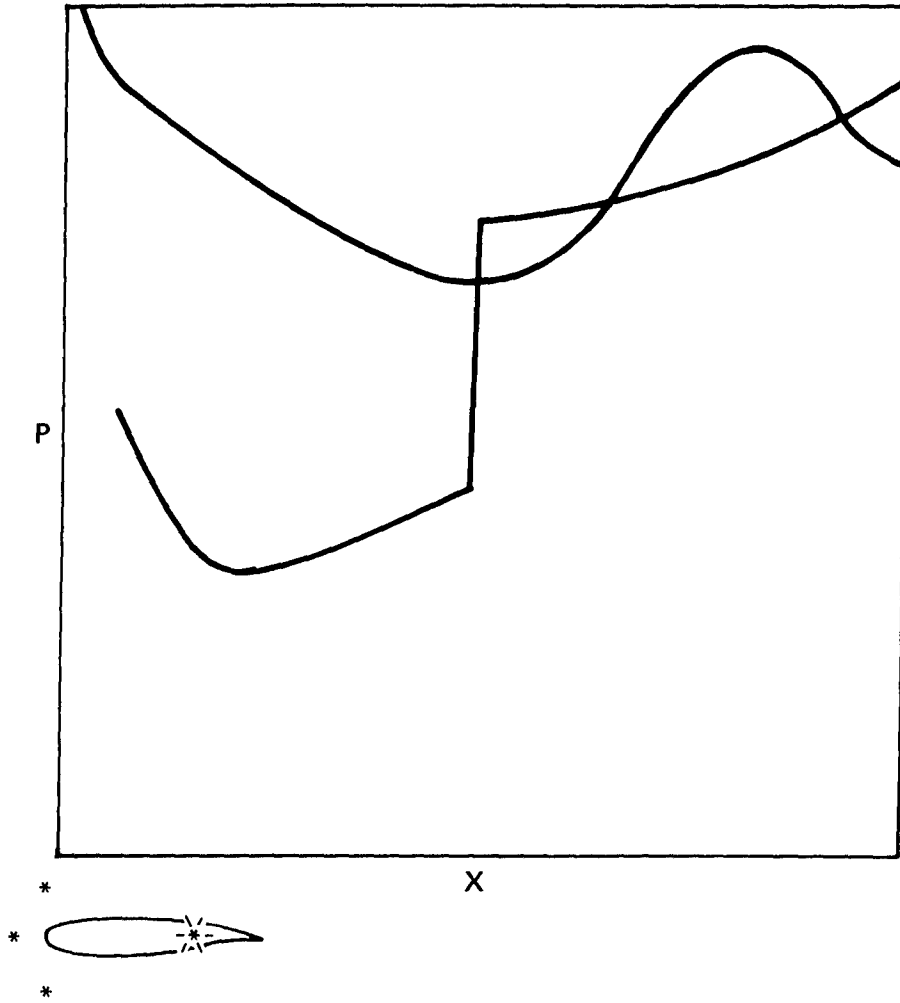


Figure 26 - Screen Display for Kutta Condition Check

APPENDIX A AIRFOIL REPRESENTATION BY SPLINES

In the analysis of arbitrary airfoil shapes, very accurate first and second derivative information of the airfoil surface is needed to complete flow analysis. The use of a nonperiodic cubic spline in airfoil representations provides a function which has linear changes in the second derivative between points on the airfoil. In order to fit a cubic spline to the points on an airfoil, very accurate data input is necessary. Also necessary to generating an accurate cubic spline function are the initial and final slopes of the airfoil.

The determination of the coefficients m_j for a cubic spline function is given by the system of equations:⁴

$$\begin{bmatrix} 2 & \mu_0 & 0 & \dots & 0 & 0 & 0 \\ \lambda_1 & 2 & \mu_1 & \dots & 0 & 0 & 0 \\ 0 & \lambda_2 & 2 & \dots & 0 & 0 & 0 \\ & & & \ddots & & & \\ & & & & \ddots & & \\ 0 & 0 & 0 & \dots & 2 & \mu_{N-2} & 0 \\ 0 & 0 & 0 & \dots & \lambda_{N-1} & 2 & \mu_{N-1} \\ 0 & 0 & 0 & \dots & 0 & \lambda_N & 2 \end{bmatrix} \begin{bmatrix} m_0 \\ m_1 \\ m_2 \\ \\ \\ m_{N-2} \\ m_{N-1} \\ m_N \end{bmatrix} = \begin{bmatrix} C_0 \\ C_1 \\ C_2 \\ \\ \\ C_{N-2} \\ C_{N-1} \\ C_N \end{bmatrix}$$

where C_j are the y-coordinates of the airfoil data points and m_j are the first derivatives at these data points. The coefficients $\lambda_j = h_j / (h_j + h_{j+1})$ and $\mu_j = 1 - \lambda_j$. The variable h_j indicates the mesh spacing; here $h_j = x_j - x_{j-1}$ and x_j are the x-coordinates of the airfoil data points. The first derivatives at the beginning and end points (m_0 and m_N) and the airfoil data points are assumed to be known.

Once the values of m_j have been determined, the cubic spline function can be expressed on (x_{j-1}, x_j) as

$$\begin{aligned}
S(x) = & m_{j-1} \frac{(x_j - x)^2 (x - x_{j-1})}{h_j^2} - m_j \frac{(x - x_{j-1})^2 (x_j - x)}{h_j^2} \\
& + y_{j-1} \frac{(x_j - x)^2 [2(x - x_{j-1}) + h_j]}{h_j^3} \\
& + y_j \frac{(x - x_{j-1})^2 [2(x_j - x) + h_j]}{h_j^3}
\end{aligned}$$

The first derivative can be expressed as

$$\begin{aligned}
S'(x) = & m_{j-1} \frac{(x_j - x)(2x_{j-1} + x_j - 3x)}{h_j^2} - m_j \frac{(x - x_{j-1})(2x_j + x_{j-1} - 3x)}{h_j^2} \\
& + \frac{y_j - y_{j-1}}{h_j^3} 6(x_j - x)(x - x_{j-1})
\end{aligned}$$

The second derivative can be expressed as

$$\begin{aligned}
S''(x) = & -2m_{j-1} \frac{2x_j + x_{j-1} - 3x}{h_j^2} - 2m_j \frac{2x_{j-1} + x_j - 3x}{h_j^2} \\
& + 6 \frac{y_j - y_{j-1}}{h_j^3} (x_j + x_{j-1} - 2x)
\end{aligned}$$

The above represents a revised version of spline program as discussed by Tai.² More information on spline functions can be found in Ahlberg et al.⁴

4. Ahlberg, J. H. et al., "The Theory of Splines and Their Applications," Academic Press, New York (1967).

```

SUBROUTINE SPLNFT(N, SLOPEI, SLOPEF, J)
COMMON/PTARFL/XX(40,2) ,YY(40,2) ,AM(40,2) ,CA ,S
DIMENSION TRID(4,30)
IF(N.NE.2) GO TO 20
5 AM(1,J) =(YY(2,J)-YY(1,J))/(XX(2,J)-XX(1,J))
AM(2,J) = AM(1,J)
RETURN
20 A = XX(2,J)-XX(1,J)
B= XX(3,J)-XX(2,J)
10 C = YY(2,J)-YY(1,J)
D= YY(3,J)-YY(2,J)
TRID(1,1) = 0.0
TRID(2,1) =1.0
TRID(3,1) = 0.0
15 TRID(4,1) = SLOPEI
TRID(1,N) = 0.0
TRID(2,N) =1.0
TRID(3,N) = 0.0
TRID(4,N) = SLOPEF
20 IFIN = N-1
DO 40 I=2,IFIN
TRID(1,I)=A
TRID(2,I) = 2.0 *I*A+B)
TRID(3,I) = B
25 TRID(4,I) = 3.0*(A*D/B+B*C/A)
IF(I-IFIN)35,50,35
35 A=B
B=XX(I+2,J)-XX(I+1,J)
C=D
30 D=YY(I+2,J)-YY(I+1,J)
50 DO 55 I=1,IFIN
TRID(1,I) = TRID(1,I)/TRID(2,I)
TRID(4,I) = TRID(4,I)/TRID(2,I)
TRID(2,I+1) = TRID(2,I+1) -TRID(3,I+1)*TRID(1,I)
35 55 TRID(4,I+1)=TRID(4,I+1)-TRID(4,I)*TRID(3,I+1)
TRID(4,N) = TRID(4,N)/TRID(2,N)
AM(IFIN,J) = TRID(4,N-1)-TRID(1,N-1)*TRID(4,N)
DO 60 I=2,IFIN
NN = N-I
40 60 AM(NN,J)= TRID(4,NN) - TRID(1,NN)*AM(NN+1,J)
AM(N,J) = TRID(4,N)
RETURN
END

```

APPENDIX B
DESCRIPTION OF SUBROUTINES

VARIABLES IN ACOM

The following variables refer to the dividing streamline, that is, the strip which proceeds from the upstream solution to the stagnation point and follows the upper and lower airfoil surfaces to the trailing edge of the body and from the trailing edge of the body to nine chord lengths downstream from the airfoil.

YO = y-coordinate normalized with respect to chord length

PO = pressure ratio P/P_{∞}

RO = density ratio ρ/ρ_{∞}

UO = velocity component in x, u/u_{∞}

VO = velocity component in y, v/v_{∞}

RMO = Mach number

DUO = velocity gradient $(du/dx)_0$

The following variables refer to the intermediate NN strips in flow integration:

Y(2,10) = y-coordinate normalized with respect to chord length

P(2,10) = pressure ratio P/P_{∞}

R(2,10) = density ratio ρ/ρ_{∞}

U(2,10) = velocity component in x, u/u_{∞}

V(2,10) = velocity component in y, v/v_{∞}

RM(2,10) = Mach number

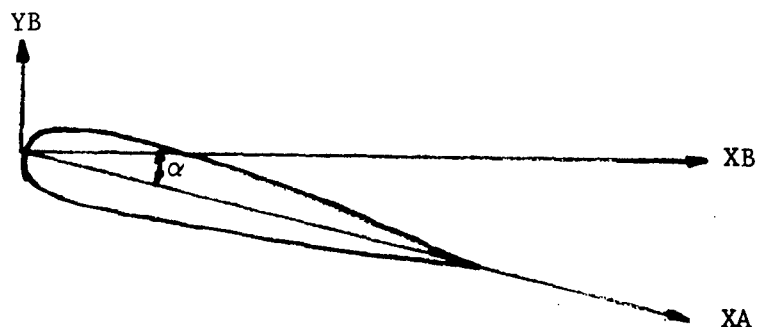
DU(2,10) = velocity gradient $(du/dx)_0$

The first subscript references either upper or lower surface and the second subscript references a particular strip. For instance, Y(1,1) references the outermost strip on the upper surface and Y(2,1) references the outermost strip on the lower surface. If five strips are being used to perform the flow integration, Y(1,5) would reference the innermost strip on the upper surface. Suppose we chose in free-stream condition an outermost strip seven chord lengths away from the body; then $Y(1,1) = 7.0$. Intermediate strips are spaced half as far away from the dividing streamline as the previous strip. Hence,

Y(1,2) = 3.5
Y(1,3) = 1.75
Y(1,4) = 0.875
Y(1,5) = 0.4375

All of the flow variables are normalized by free-stream values.

VN = velocity component at airfoil surface normal to airfoil
VS = velocity component at airfoil surface, tangential to airfoil
X = X-coordinate
XA = distance along airfoil chord
XB = distance along airfoil parallel to X axis
H = integration step size



VARIABLES IN COMMON/AINPUT/

AIN(1) DVOOI = estimated cross velocity gradient at stagnation point
AIN(2) XS = stagnation point on airfoil
AIN(3) XAO = initial point upper surface
AIN(4) CYDU = parameter indicating shape of final velocity profile
of final upstream integration station for upper
surface
AIN(5) XAI = initial point lower surface
AIN(6) CYDL = parameter indicating shape of final velocity profile
of final upstream integration station for lower
surface
AIN(7) SL = shock location

AIN(8)	XOO ≈ 4.0	= parameter used in calculating DVOO for UPSTRM
AIN(9)	RMT ≈ 7.0	= Mach number used in UPSTRM
AIN(10)	CDY ≈ 0.1	= upper limit for slope of stagnation streamline in UPSTRM
AIN(11)	YU ≈ 0.7	= location of outermost strip on upper surface
AIN(12)	YL ≈ 7.0	= location of outermost strip on lower surface
AIN(13)	CX ≈ 0.5	= X-coordinate for last integration step in SUBCRT1
AIN(14)	RMC ≈ 0.92	= upper limit for Mach number on innermost strip in SPRCRT1
AIN(15)	BETAD	= shock wave angle
AIN(16)	DELS	= entropy change through shock foot in SPRCRT2
AIN(17)	CDDQ ≈ 11.0	= upper limit for d^2q/dx^2 in SPRCRT2
AIN(18)	RKI ≈ 5.0	= value of RK for DWNSTRM
AIN(19)	XASPR	= X-coordinate for initial point in SPRCRT2
AIN(2)	DE	= distance from final station of upstream integration to airfoil surface
AIN(21)	YSO	= distance which stagnation streamline is perturbed by the airfoil
AIN(22)	YS	= y-coordinate of stagnation point
AIN(23)	CSI	= value of CS in DWNSTRM
AIN(24)	CZI	= value of CZ in DWNSTRM
NNI(1)		= number of strips used for the bulk of flow integration in UPSTRM
NNI(2)		= number of additional strips used near stagnation point in UPSTRM
NNI(3)		= number of strips used in UPRINIT
NNI(4)		= number of strips used in LWRINIT
NNI(5)		= number of strips used in SPRCRT2
NNI(6)		= number of strips used in DWNSTRM
NNI(7)		= dummy variable used in IOUPRIN and IOLWRIN
H(1)		= step size in UPSTRM
H(2)		= step size in SPRCRT1
H(3)		= step size in SUBCRT1
H(4)		= step size in SUBCRT2
H(5)		= step size in SPRCRT2
H(6)		= step size in DWNSTRM

VARIABLES IN COMMON/YUVSAV/

These variables contain the flow conditions output from one step and input to another. The flow conditions are y, the distance from the airfoil surface to this particular strip, u, the horizontal velocity component, and v, the vertical velocity component.

For subroutine UPSTRM, the output variables are stored in arrays YI, UI, and VI, and the number of strips is stored in NNI. These variables are input to subroutines UPRCRIT, UPRINIT, LWRCRIT, and LWRINIT.

For subroutine SPRCRT1, the output variables are stored in arrays YSPR, USPR, and VSPR, and the number of strips is stored in NNSPR. These variables are input to subroutine SPRCRT2.

For subroutine SPRCRT2 or SUBCRT2, the output variables are stored in arrays YU, UU, VU, and YL, UL, and VL, and the number of strips is stored in NNDWN. The flow conditions for the dividing streamline are stored in arrays YO, UO, and VO. These variables are input to subroutine DWNSTRM.

VARIABLES IN BLANK COMMON

$$C = 1 + 5/M^2$$

$$CK = 5/7M^2$$

$$RS = (1/7CK + 1)^{2.5}$$

$$FM = M = \text{Mach number}$$

$$ALPHA = \alpha = \text{angle of attack}$$

OUTPUT SUBROUTINES

No references are made to read and write units in the subroutines which actually perform the flow integration processes. The output variables are stored in arrays and are output on the line printer in subroutines beginning with the letters IO. The output subroutines and the corresponding flow integration subroutine are:

IOUPSTM	UPSTRM
IOSTGNA	STAGNA
IOUPRCT	UPRCRIT
IOUPRIN	UPRINIT,SPRCRT1
IOSPCT2	SPRCRT2
IOLWRCT	LWRCRIT
IOLWRIN	LWRINIT,SUBCRT1,SUBCRT2
IODNSTM	DWNSTRM

FLOW INTEGRATION SUBROUTINES

Subroutine UPSTRM

This subroutine performs the upstream integration from free-stream conditions to the stagnation point on the airfoil. The primary outputs of the subroutine are given in COMMON/OUTCOM.

AXA = x stations along stagnation streamline
ARMO = Mach number along stagnation streamline
AY = y stations at final integration station
ARM = Mach numbers at final integration station

Other important variables are

CSO = Mach number
CS1 = Mach number at which more strips are added to the flow solution
DYO = local slope of the stagnation streamline

Integration proceeds from the free-stream conditions to a point where the Mach number on the stagnation streamline is considerably lessened. This part of the integration uses subroutine DIST which

includes the effects of the cross velocity gradient DV001. When the Mach number RMO reaches a particular value of RMT, the flow integration uses subroutines STMR and LUMR depending on the slope of the stagnation streamline, DY0. The value of RMD should decrease until it reaches a value of CS0; at this point, flow values are stored for future use. If this is the first time that flow variables are stored, more strips are added to the flow integration. The flow integration now includes a total of NN + NA strips and the stagnation streamline. The parameter CS0 is decreased by a value of 0.05, and flow integration continues to the point where RMO reaches this value. The flow values are stored at this point, and the process is repeated until flow values are stored at four points. By using a Lagrangian, values of RMD are extrapolated to the point where RMO = 0, the point where the stagnation streamline meets the airfoil. The value of DE, the distance from the last computed station of upstream integration to the stagnation point on the airfoil, can now be computed. Upstream integration is now complete.

The final section of this subroutine computes airfoil coordinates and 11 points along the stagnation streamline. This information is input to subroutine STAGNA to calculate the stagnation streamline geometry.

Subroutine STAGNA

This subroutine computes the cross velocity gradient at the point XS and the stagnation streamline geometry corresponding to this stagnation point. The primary outputs of this subroutine are given in COMMON/ECOM/ as:

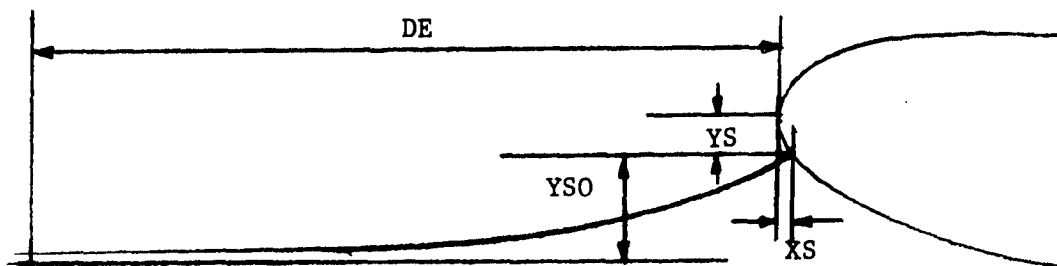
XOU = x-coordinates of airfoil nose
YOU = y-coordinates of airfoil nose
XAF = x-coordinates of stagnation streamline
YAF = y-coordinates of stagnation streamline

Other important variables in this subroutine are:

DE = distance from final station of upstream integration to
airfoil surface

YSO = distance which stagnation streamline is perturbed by the
airfoil

YS = y-coordinate of stagnation point



For a given stagnation point XS, the radius of curvature RA at this point on the airfoil is calculated. The cross velocity gradient DVOOF can then be calculated. The airfoil coordinates and stagnation streamline are then converted to one Cartesian frame of reference.

Subroutine UPRCRIT

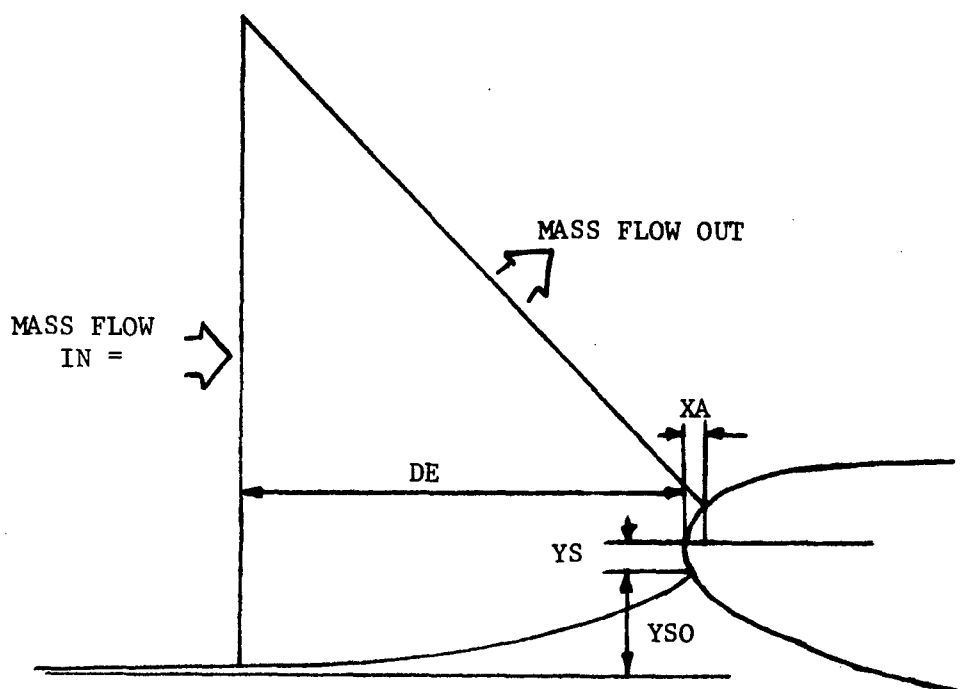
This subroutine determines flow criticality on the upper surface by computing the Mach number at various points along the surface. The primary outputs of this subroutine are given in COMMON/OUTCOM/ as:

AXB = x station on airfoil surface

ARMB = Mach number calculated at airfoil surface

For a given initial point XA, a perpendicular is drawn to the airfoil surface which intersects the final station of upstream integration. Depending on where the perpendicular intersects this station, the mass flow into the control volume is calculated. By using the Newton-Raphson method, the flow out of the control volume is calculated which matches the input flow, and the Mach number at this point is calculated.

The sketch illustrates the control volume and the corresponding geometry.



Subroutine UPRINIT(ICRIT)

This subroutine determine the initial flow conditions on the upper surface for a particular initial point. The solution method is the same as UPRCRIT, but the solution is performed for one point instead of a series of points. Important output variables are given in COMMON/RBUBCM/ as:

RBUB = mass flux at initial point

UBINIT = velocity at initial point

The calculation of RBUB, the mass flux at the surface of the airfoil, includes the term CYD. Increasing the value of CYD decreases the value of RBUB. In some cases the value of UBINIT cannot be calculated because the value of RBUB is too large or too small, but there is a wide range of values of CYD for which a solution exists.

Subroutine SPRCRT1(J)

This subroutine performs the initial integration of flow conditions for supercritical flow. The parameter J indicates airfoil surface. (J = 1 for upper surface, J = 2 for lower surface.) Important output variables are given in COMMON/OUTCOM/ as:

XBO = x stations at airfoil surface

RMBO = Mach number along stagnation streamline

DUBO = velocity gradients along stagnation streamline

The subroutine consists of three main steps:

1. Integration in subsonic region and storage of data during integration to extrapolate through the sonic point.
2. Extrapolation through the sonic point.
3. Integration in supersonic region and extrapolation of data to final station.

Flow integration in this subroutine as well as SUBCRT1 utilizes subroutine INBO to calculate the flow properties at the surface of the airfoil. All other subroutines calculate flow properties along the airfoil surface in subroutine INAS.

A typical flow integration step in subroutine SPRCRT1 has the form

```
CALL OUNS(1,J)
NN1 = NN-1
DO 10 N = 1, NN1
10 CALL INAS(1,J,N,1)
CALL INBO(NN,J)
```

During integration in the subsonic region, checks are made at each integration step on the surface velocity gradient DUB and Mach number RMB. If DUB is less than 5.0 or RMB suddenly becomes greater than 1.0, the trial is aborted. For purposes of extrapolating data through the sonic point, data are saved at points where RMB = 0.9, 0.92, 0.94 and 0.96.

Once data at those four points have been saved, an attempt is made to extrapolate through the sonic point by using a Lagrangian function. The value of XA is incremented until a value for RMB greater than 1.03

is produced. Once this is done, the flow properties at this station are calculated, and integration proceeds to the supersonic region.

During integration in the supersonic region, checks are made at each integration step on the values of DUB and RMB. If DUB is greater than 60.0 or RMB is less than 1.0, the trial is aborted. If the value of the velocity gradient and Mach number at the innermost strip, $DU(J,NN)$ and $RM(J,NN)$, respectively, are greater than specified values, the number of integration strips is reduced by one. Because of different coordinate systems used, a very small gap in the flow field exists between the output station of $SPRCRT1(J)$ and the input station of $SPRCRT2(J)$. Flow properties are extrapolated in this gap by using a Lagrangian function.

Subroutine $SPRCRT2(J)$

This subroutine performs integration for supercritical flow for the bulk of the airfoil surface. The output variables located in `COMMON/OUTCOM/` are:

AXA = integration station XA

ADU = velocity gradient (du/dx) at innermost strip NN

DDQO = $d/dx(dq/dx)$ spatial rate of change of dynamic pressure at innermost strip NN

A typical flow integration step in subroutine $SPRCRT2$ has the form

```
CALL OUNS(1,J)
```

```
DO 10 N = 1, NN
```

```
10 CALL INAS(1,J,N,NN)
```

Flow integration in the upper surface is accomplished in three steps: subcritical, supercritical, and subcritical flow integrations. Subcritical flow is calculated from the leading edge to the sonic line; supercritical from sonic line to shock location SL and finally subcritical from SL to the trailing edge.

During flow integration in the supersonic region, checks are made on the values of DUO and RMO. If DUO is greater than 100 or RMO is less than 1.0, the trial is aborted. If the value of DDQ is greater than the input value of CDDQ, the number of flow integration strips is decreased by one.

Flow integration proceeds to the point where X is greater than SL, and the Rankine-Hugoniot relations are applied there across the designated shock location. If the value of DELS is greater than 0.0, allowances are made for an entropy change through the shock location.

New flow variables are computed at the shock location SL, and flow integration proceeds to the trailing edge. Checks are made on DUO and RMO to ensure that the flow remains subcritical throughout the integration.

Subroutine LWRCRIT

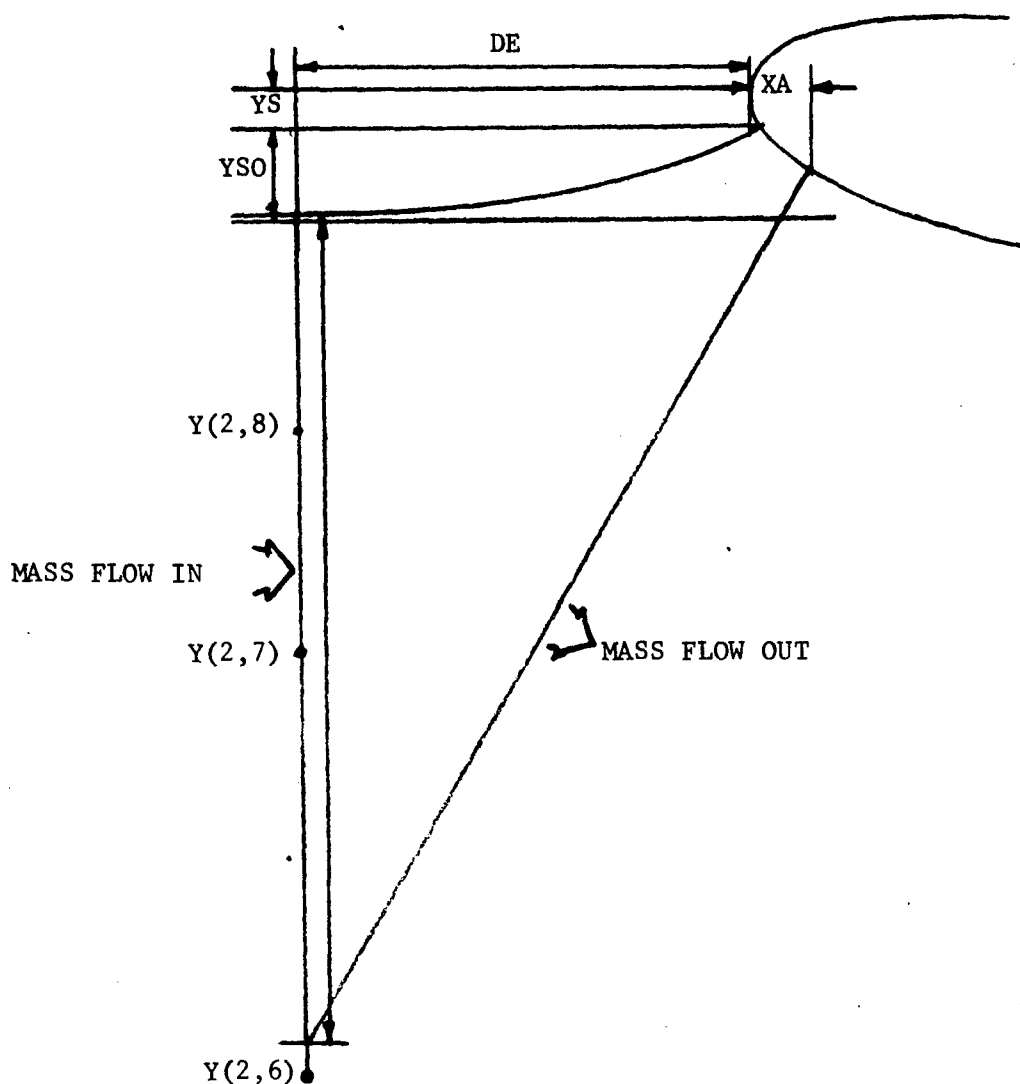
This subroutine determines flow criticality on the lower surface by computing Mach number at various points along the surface. Important output variables given in COMMON/OUTCOM are:

AXB = X stations for Mach number calculations

ARMB = Mach number calculated at airfoil surface

For a given initial point XA, a perpendicular is drawn to the airfoil surface which intersects the final station of upstream integration. Depending on where the perpendicular intersects this station, the mass flow into the control volume is calculated. By using the Newton-Raphson method, the mass flow out of the control volume is calculated which matches the input flow, and the Mach number is calculated.

An illustration of the control volume and the corresponding geometry is shown below; the perpendicular intersects the final station between Y(2,6) and Y(2,7).



Subroutine LWRINIT(ICRIT)

This subroutine determines the initial flow conditions on the lower surface for a particular initial point. The solution method is the same as LWRCRIT, but the solution is performed for one point instead of a series of points. Important output variables given in COMMON/RBUBCM/ are:

$RBUB = \rho_b V_b$ at initial point

$UBINIT$ = velocity at given initial point

The initial flow conditions for lower surface flow are computed in the same manner as subroutine LWRCRIT, and computation proceeds according to the value of ICRIT.

Subroutine SUBCRT1(J)

This subroutine performs the initial integration of flow conditions for subcritical flow. Important output variables are given in COMMON/OUTCOM/ as:

XBO = integration station

RMBO = Mach number along stagnation streamline

DUBO = velocity gradient along stagnation streamline

A typical flow integration step in subroutine SUBCRT1 has the form

```
CALL OUNS(1,J)
```

```
NN1 = NN-1
```

```
DO 10 N = 1, NN1
```

```
10 CALL INAS(1,J,N,1)
```

```
CALL INBO(NN,J)
```

where NN is the number of strips available for integration.

During flow integration, checks are made on the values of RMO and DUB. If RMO is greater than 1.0, the assumption of subcritical flow is invalid and the trial is aborted. The trial is also aborted if the velocity gradient DUB becomes negative near the leading edge of the airfoil.

Data are saved at four stations for use in extrapolation to the output flow conditions at station XB which is fairly close to CXI. The extrapolation is needed to proceed with the integration in subroutine SUBCRT2.

Subroutine SUBCRT2(J)

This subroutine performs integration for subcritical flow for the bulk of the airfoil surface. The output variables located in COMMON/OUTCOM/ are:

AXA = integration station

ARMO = Mach number at surface

ADU = velocity gradient (du/dx) at innermost strip NN

A typical flow integration step in subroutine SUBCRT2 has the form

```
CALL OUNS(1,J)
DO 10 N = 1, NN
10 CALL INAS(1,J,N,NN)
```

During flow integration checks are made on the values of RMO and ADU . If RMO does not lie between 0.4 and 1.0, the trial is aborted and if the absolute value of the velocity gradient $(du/dx)_{NN}$ becomes greater than 2.0, the innermost strip is dropped. At a value of $X = CX = 0.5$, another strip is added between the innermost strip and the airfoil surface, and flow integration continues to the trailing edge of the airfoil, $X = CX = 1.0$.

Subroutine DWNSTRM

This subroutine performs flow integration downstream in the airfoil. The output variables located in `COMMON/OUTCOM/` are:

AX = integration station
 APO = pressure ratios along dividing streamline
 API = pressure ratios on NN strip

A typical flow integration step in subroutine DWNSTRM has the form

```
CALL OUNS(1,1)
CALL INAS(1,1,NN,NN)
```

where NN is the number of the strip used to integrate the intermediate strip.

Subroutine INVELOC(L,J)

This subroutine calculates the velocity component $V(J,NN)$ of the innermost strip. If $L = 2$, this velocity component is computed according to a Lagrangian function; if $L = 3$, this velocity component is computed according to a parabolic function.

Subroutine ARFL(XA,XB,YB,DYB,DDYB,J)

This subroutine determines the y-coordinate and its first and second derivatives at a point on the airfoil. The arguments of this subroutine are:

XA = airfoil x-coordinate

The following values are calculated at the given angle of attack:

XB = x-coordinate

YB = y-coordinate

DYB = first derivative

DDYB = second derivative

J = 1 for upper surface and 2 for lower surface.

These values are determined according to the equations in Appendix A.

Subroutine DIST(M,I,N,DY1,DVS,DV1)

This subroutine performs a flow integration step on the dividing streamline in the upstream solution. The arguments of this subroutine are:

M = ± 1 , indicating direction of integration

I = 1 for upper surface and 2 for lower surface

N = number of innermost strip

DY1 = slope of dividing streamline

DVS = increment in velocity of dividing streamline

DV1 = increment in velocity of vertical component of dividing streamline

This subroutine includes the effect of the cross velocity gradient DV00 in determining the flow conditions far upstream from the airfoil. As the flow integration approaches the airfoil, the Mach number becomes too small; the flow integration must be completed by subroutines STMR and LUMR.

Subroutine STMR(N,T,DY,DVS)

This subroutine performs a flow integration step on the dividing streamline in the upstream solution. The arguments of this subroutine are:

N = number of innermost strip
T = angle of dividing streamline with respect to the horizontal;
$$T = \sin^{-1} DY / \sqrt{1 + DY^2}$$

DY = slope of dividing streamline
DVS = increment in velocity of dividing streamline

This subroutine neglects the effects of changes in the vertical component of the dividing streamline in computing the flow integration. This is valid if $DY > 0.1$.

Subroutine LUMR(M,I,N,DY1,DVS,DV1)

This subroutine performs a flow integration step on the dividing streamline in the upstream solution. The arguments of this subroutine are:

M = ± 1 , indicating direction of integration
I = 1 for upper surface and 2 for lower surface
N = number of innermost strip
DY1 = slope of dividing streamline
DVS = increment in velocity of dividing streamline
DV1 = increment in velocity of vertical component of dividing streamline

This subroutine computes the flow variables in the vicinity of the airfoil when the value of DY1 is less than 0.1.

Subroutine OUNS(M,I)

This subroutine performs a flow integration step on the next to the outermost streamline. The arguments of the subroutine are:

M = ± 1 , indicating direction of integration
I = 1 for upper surface and 2 for lower surface

The flow on the outermost strip is assumed to be undisturbed and this integration is performed on the next strip. The remaining strips in the flow field are computed in subroutine INAS.

The gradients calculated in this subroutine are:

$DU(I,2) = du/dx$, velocity in x-direction

$DV1 = dv/dx$, velocity in y-direction

$DY1 = dy/dx$, slope of streamline

as output of the Runge-Kutta integration process. Gradients calculated as input to the next inner strip are:

$DRHU(I) = d/dx(\rho u)$

$DPRU(I) = d/dx(KP + \rho u^2)$

$DRUV(I) = d/dx(\rho uv)$

Subroutine INAS(M,I,N,IJ)

This subroutine performs a flow integration step on the Nth strip.

The arguments of this subroutine are:

M = 1, indicating direction of integration

I = 1 for upper surface and 2 for lower surface

N = strip number

IJ = NN for subroutines SUBCRT2, SPRCRT2, and DWNSTRM

IJ = 1 for all other subroutines

This subroutine performs the bulk of flow integration from the third to the NNth strip. For subroutines SUBCRT2, SPRCRT2, and DWNSTRM, it also performs integration on the dividing streamline. This is accomplished by the use of the parameter ISKIP, which indicates for which subroutine the solution is being computed.

<u>ISKIP</u>	<u>SUBROUTINE</u>
1	SUBCRT2
2	SPRCRT2
3	DWNSTRM

The value of V_0 , the vertical component of the stagnation streamline, is computed differently in these three subroutines.

$v_0 = u_0 * dy/dx$ for SUBCRT2

$v_0 = v_0 + h (dv_0/dx)$ for SPRCRT2 where dv_0/dx is computed according to MIR

$v_0 = v_{0,T.E.} \exp[(1-x)RK]$ for DWNSTRM

The gradients calculated in this subroutine are the same as those for subroutine OUNS.

Subroutine INBO(N,I)

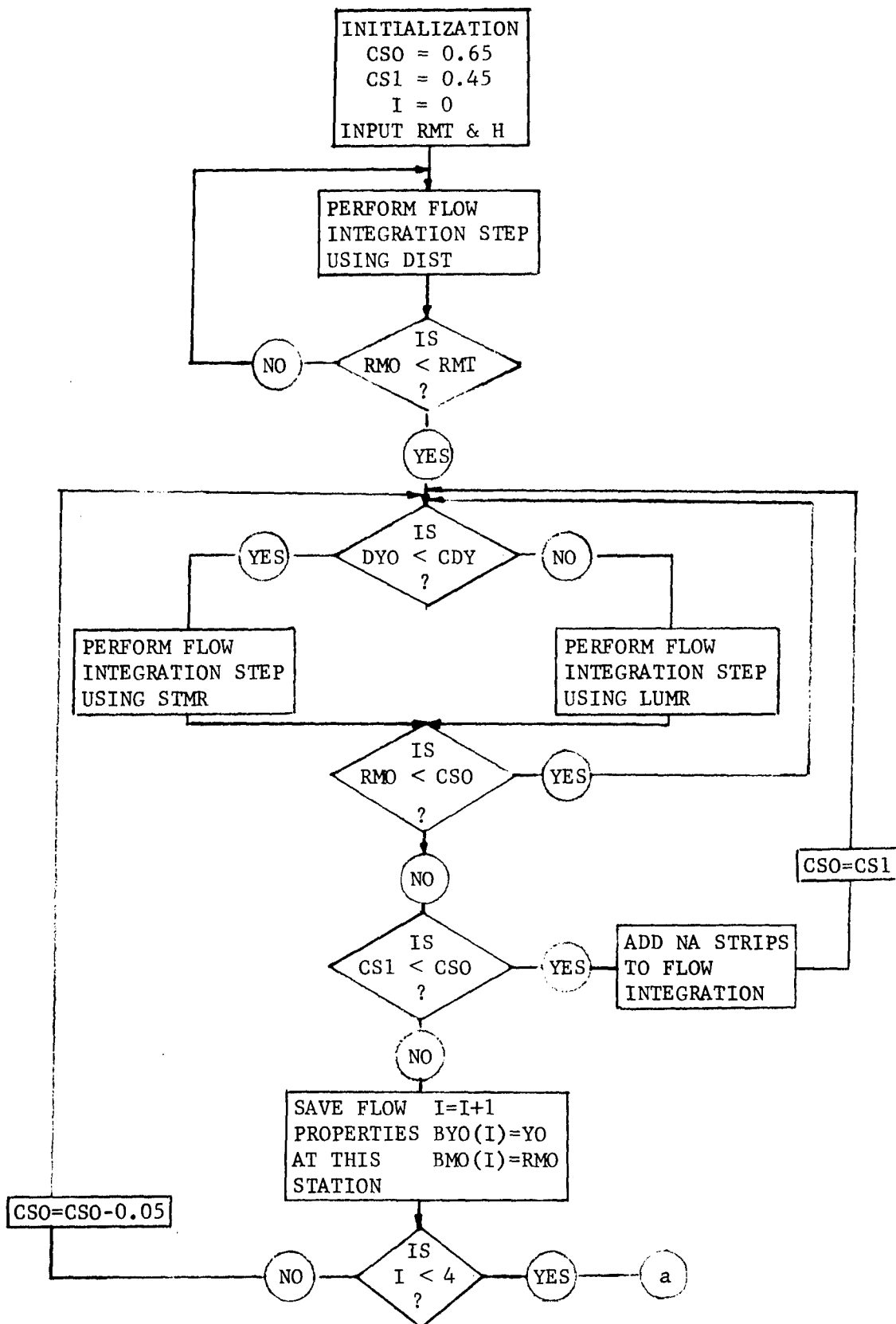
This subroutine performs a flow integration along the dividing streamlines for subroutines SUBCRT1 and SPRCRT1. The arguments of this subroutine are:

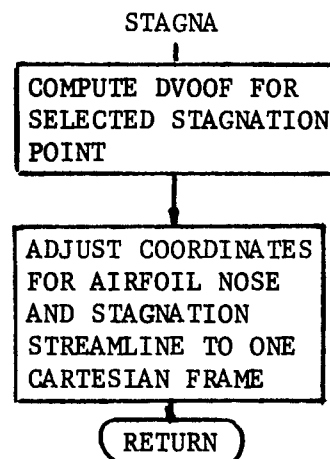
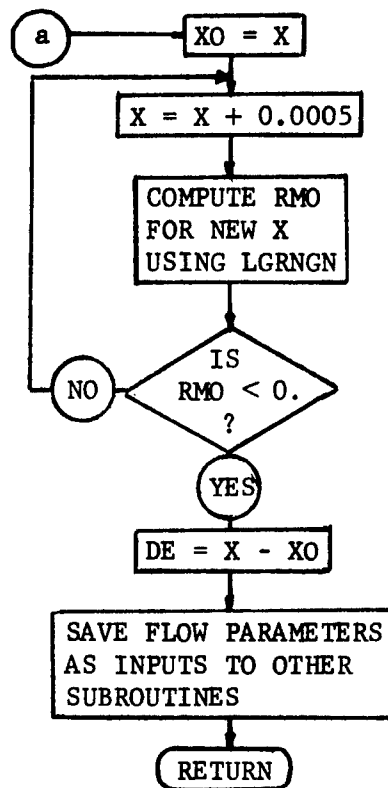
N = number of innermost strip

I = 1 for upper surface and 2 for lower surface

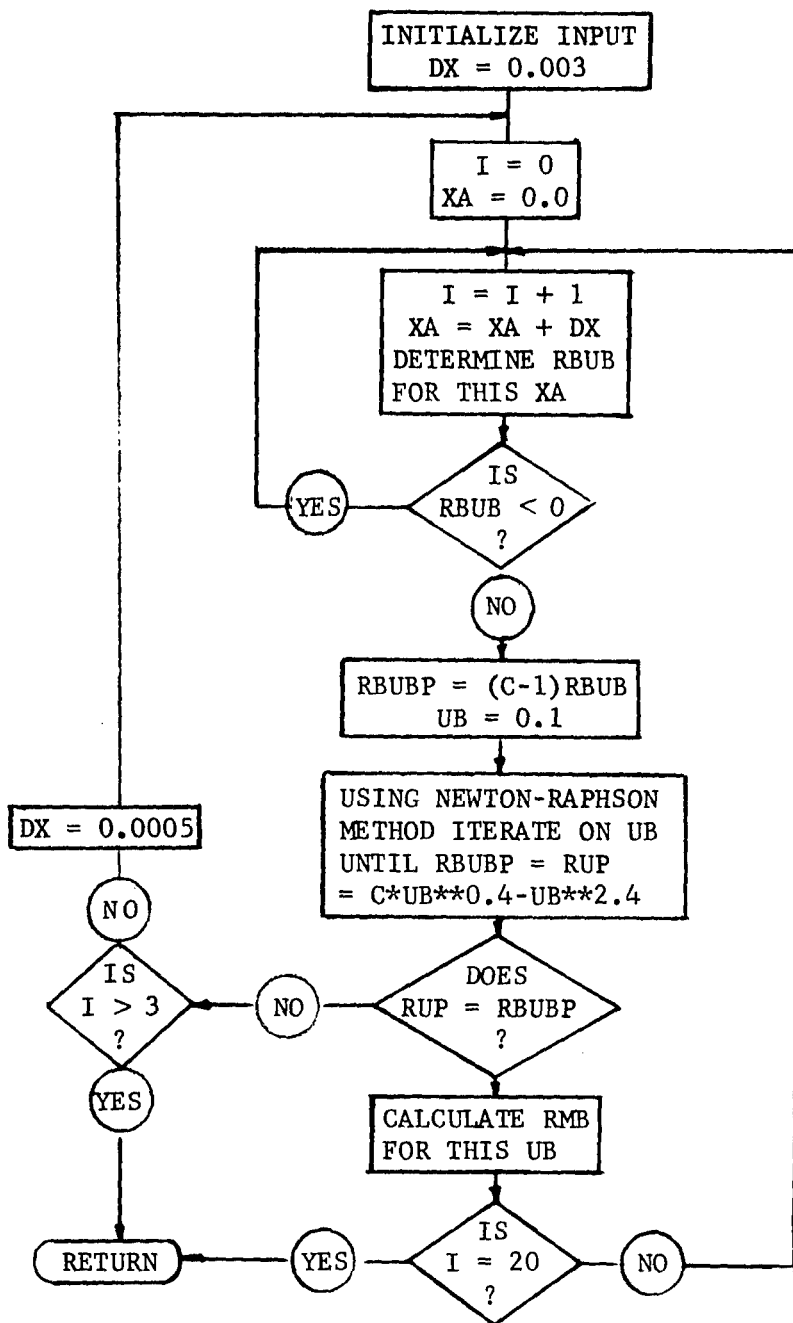
The calculation of a strip between the innermost strip and the airfoil surface is also accomplished here. The parameters Y_0 , U_0 , V_0 , R_0 , and P_0 refer to this strip and the parameter Y_B , U_B , R_B , and P_B refer to the values at the airfoil surface along the dividing streamline.

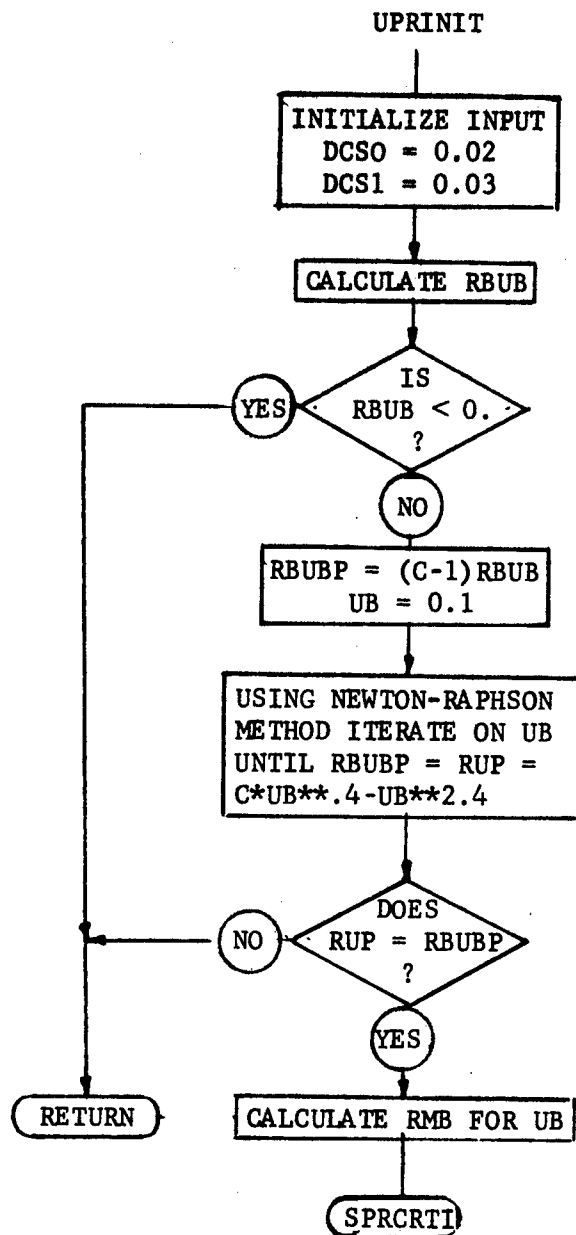
APPENDIX C
SUBROUTINE FLOW CHARTS
UPSTRM



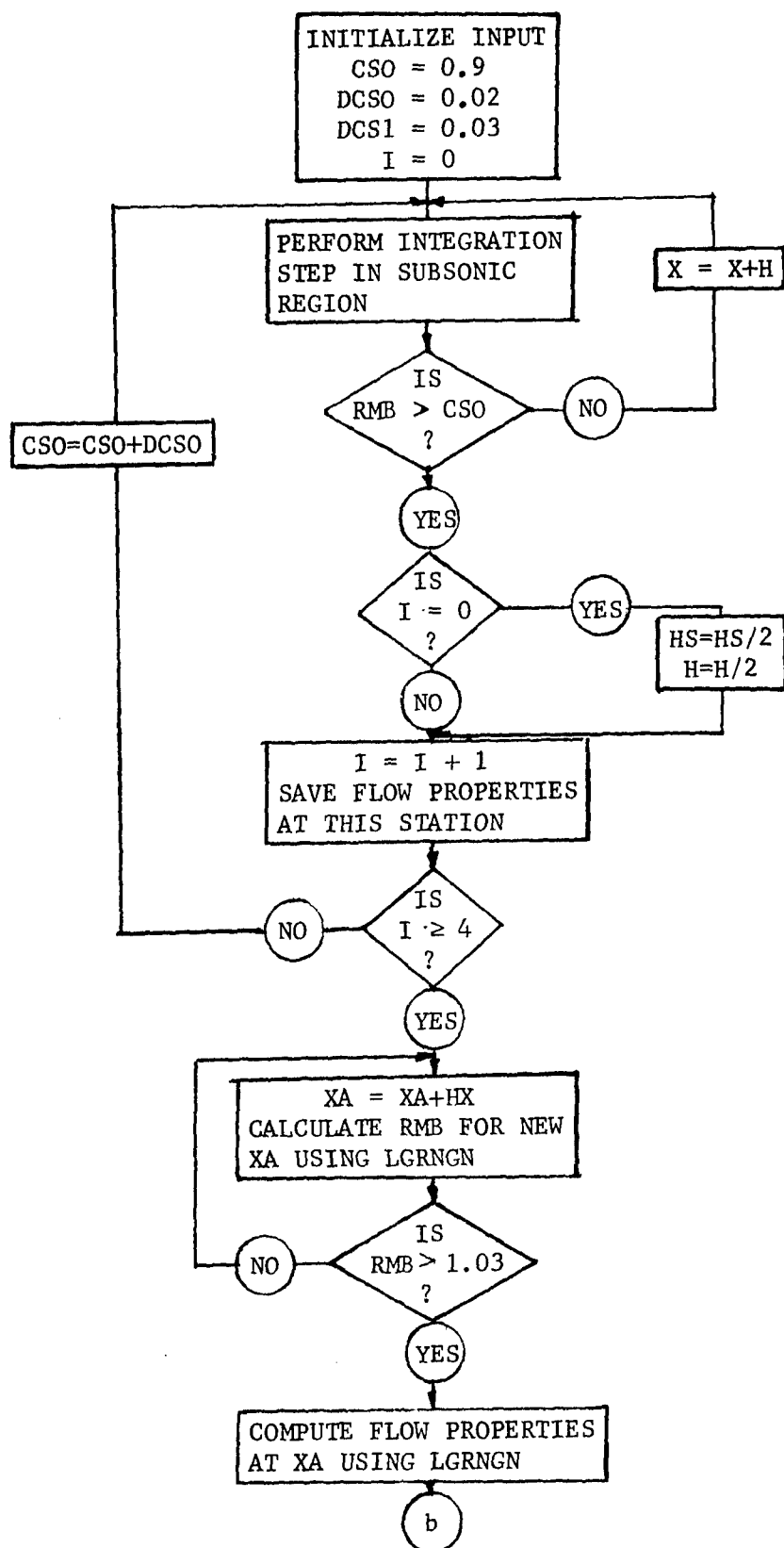


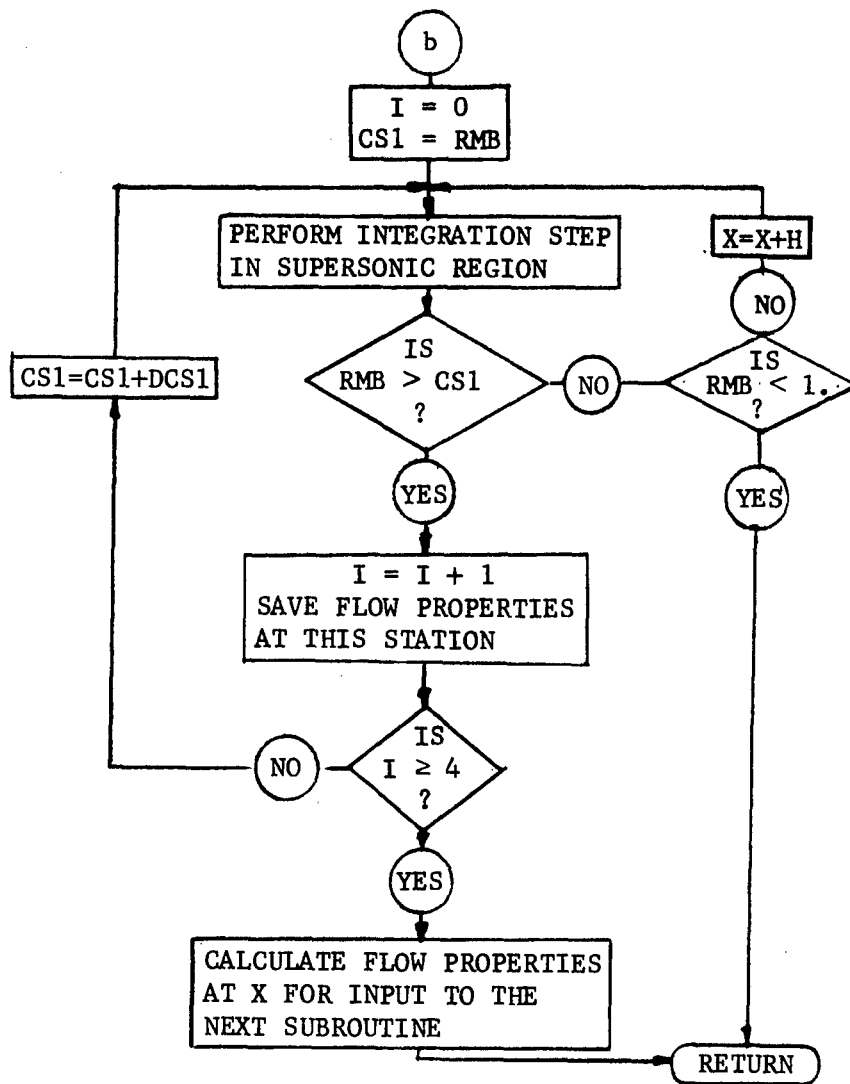
UPRCRIT



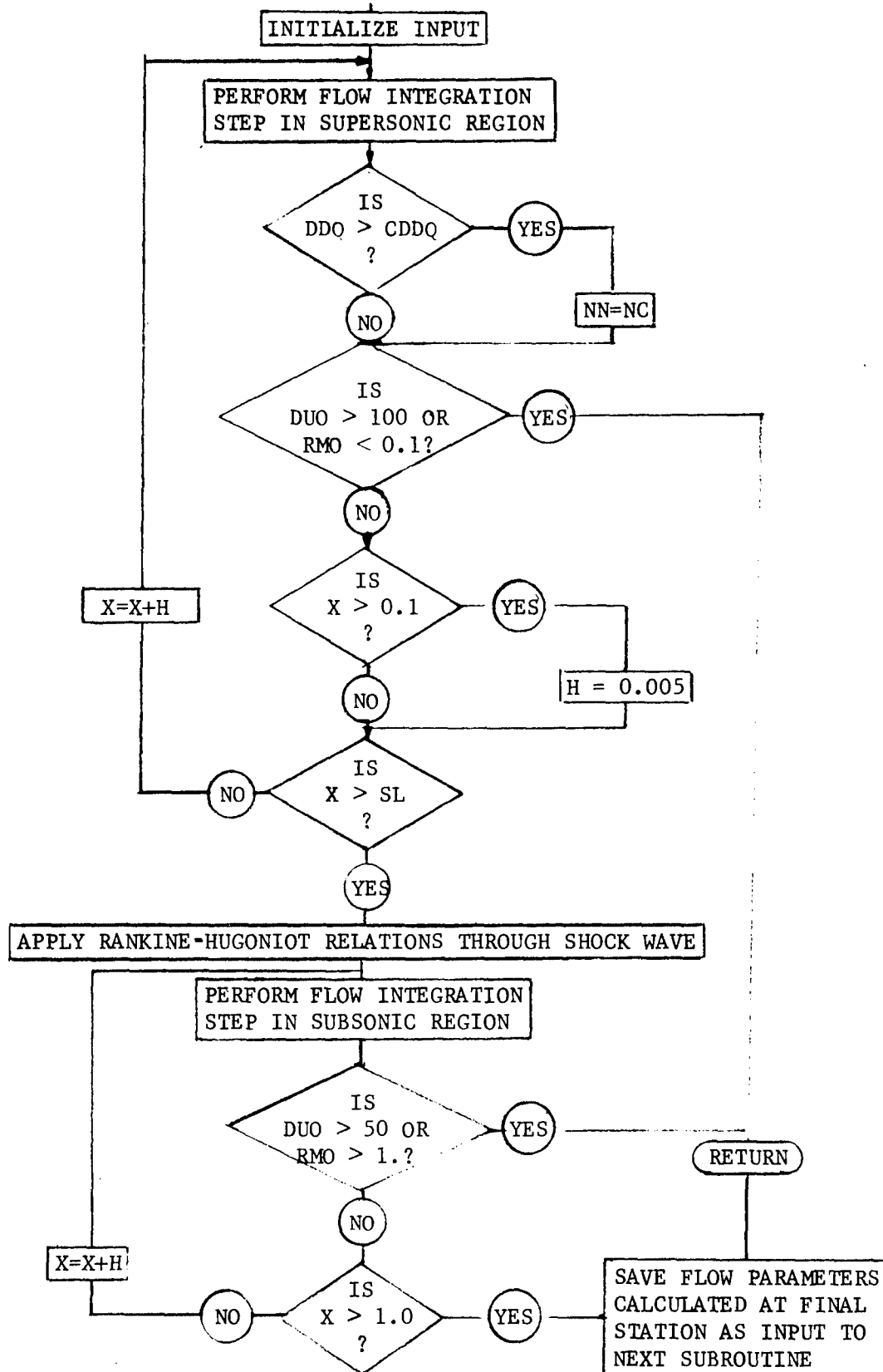


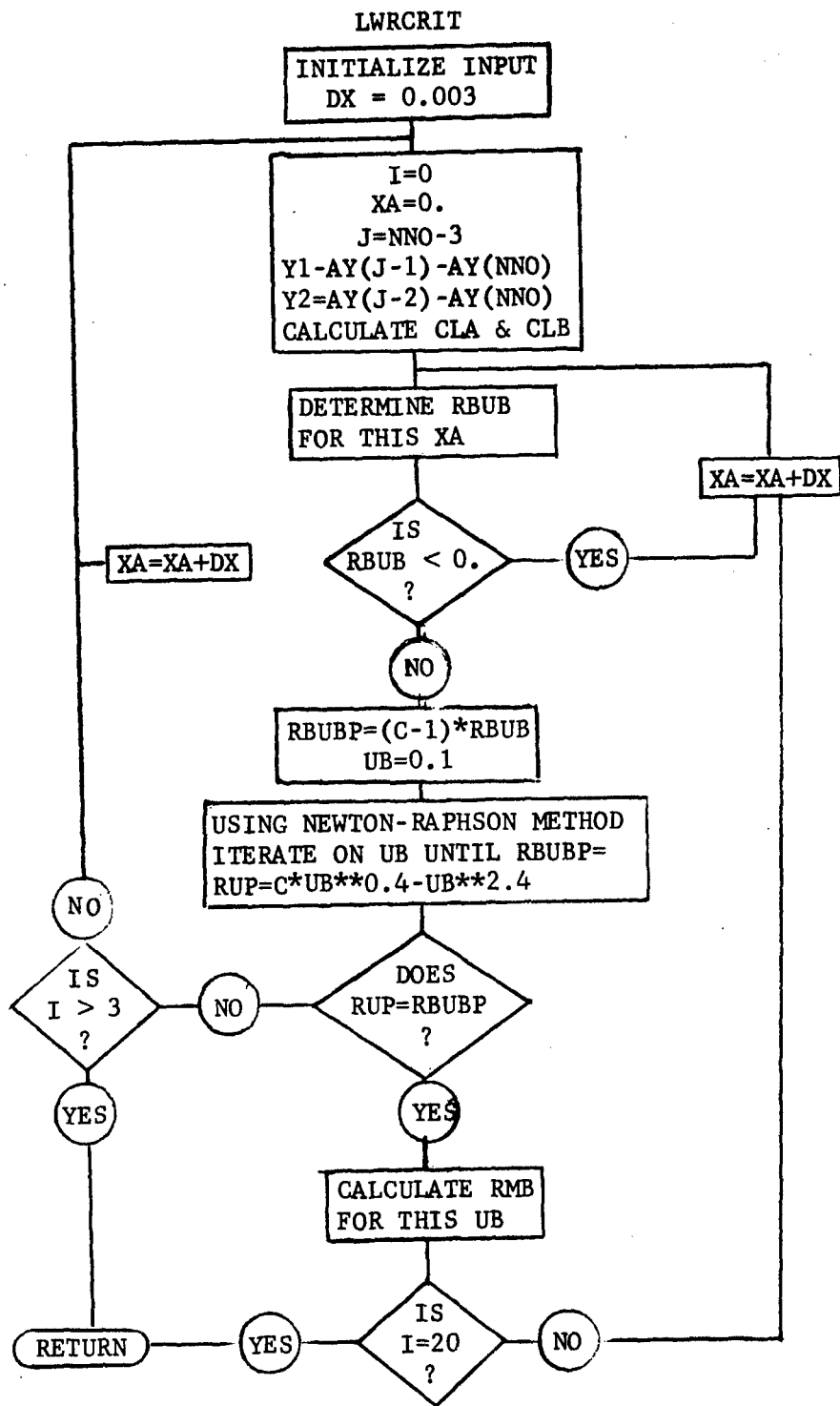
SPRCRT1

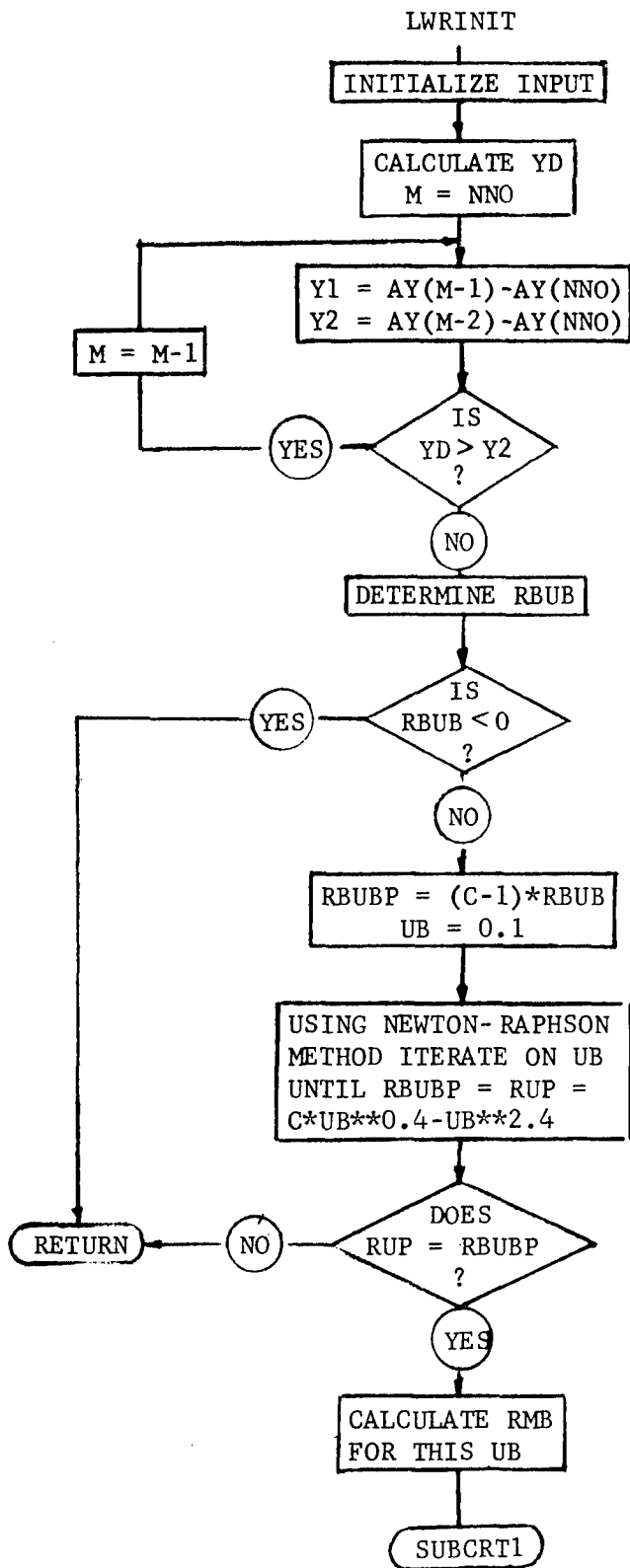




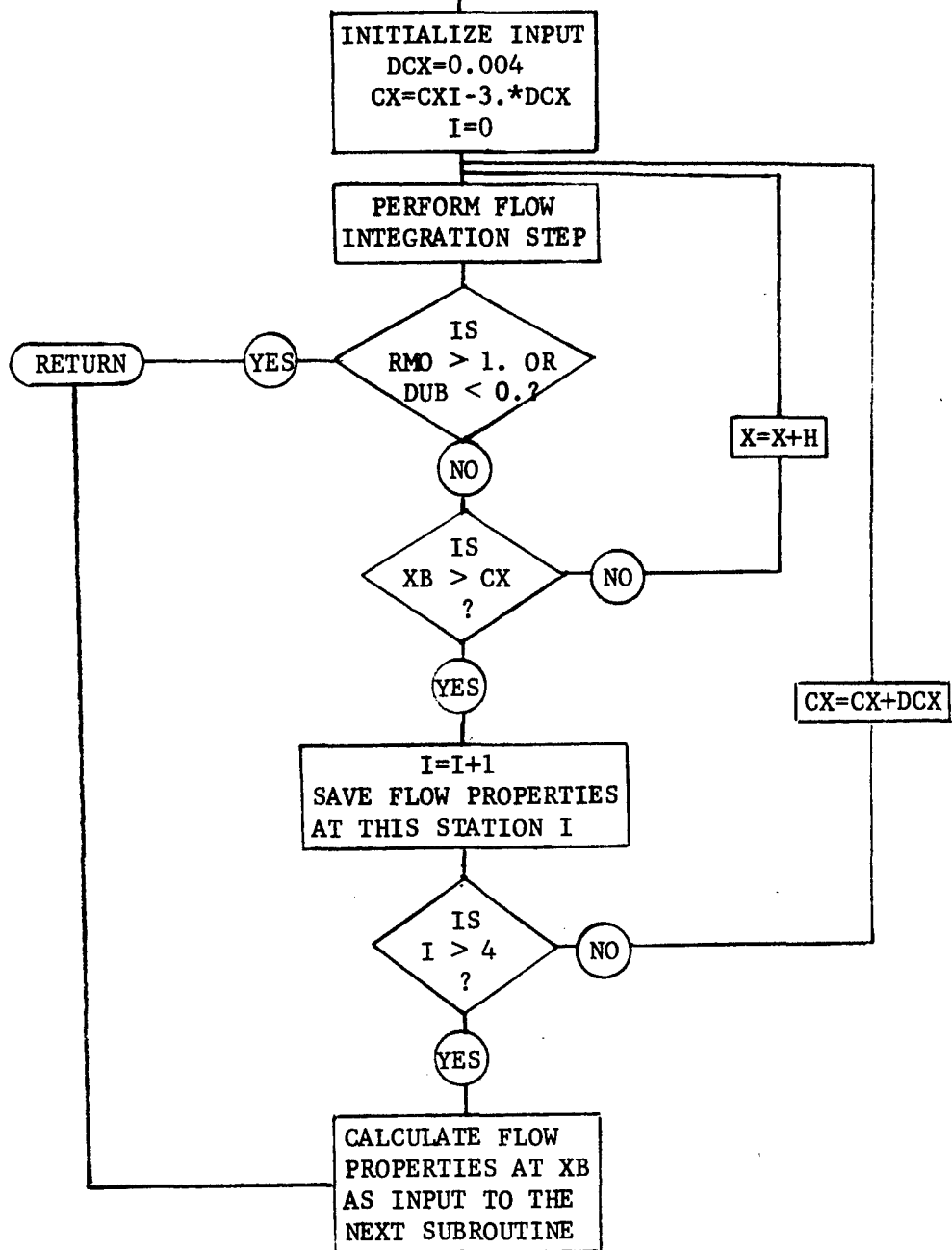
SPRCRT2



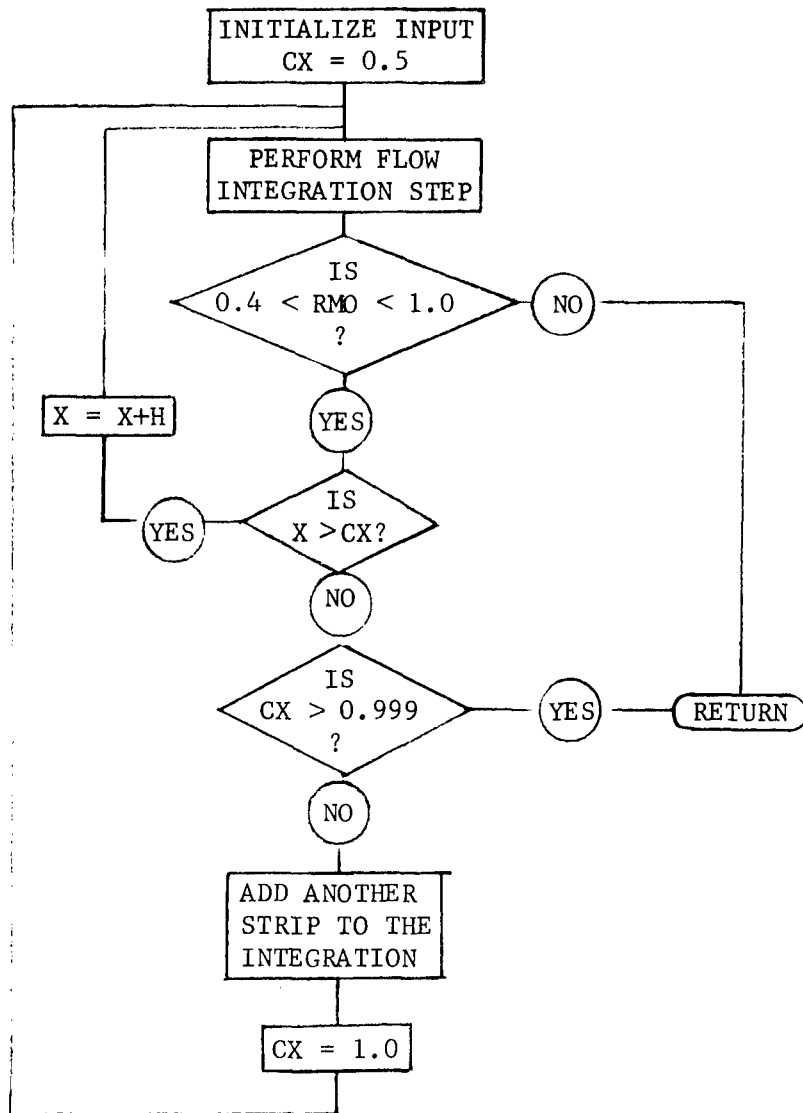


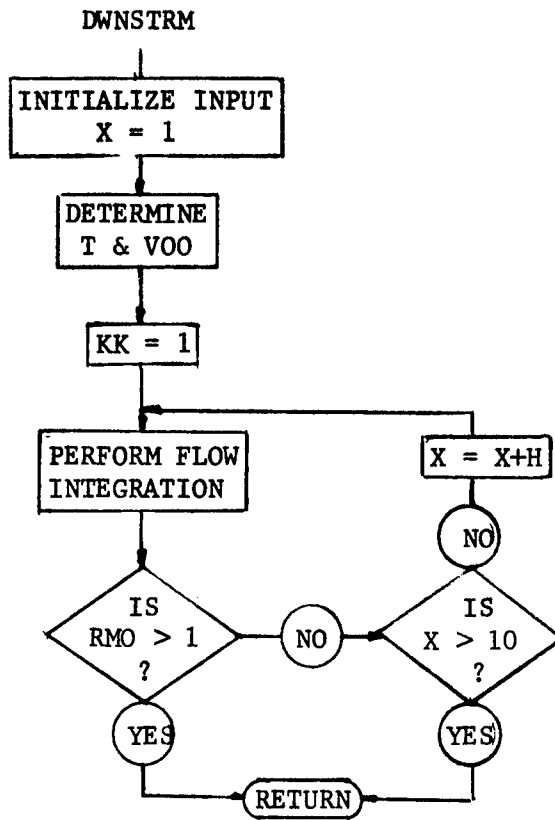


SUBCRT1



SUBCRT2





APPENDIX D

DESCRIPTION OF INTERACTIVE GRAPHICS PROGRAM

A description of the interactive graphics program requires knowledge of the Graphic Pac subroutines.* Such software is invaluable to the applications programmer because it permits him to use the interactive graphics facility with relative ease and simplicity.

Graphic Pac allows the applications programmer to create light buttons, light registers, and text entities which appear on the console screen. The working area of the console screen is a square inscribed within the circular screen area. The lower left-hand corner of the working area has the coordinates (-57, -57) and the upper right-hand corner has the coordinates (57, 57). The light buttons, light registers, and text entities can appear at any of about 13,000 addressable points on the screen. The light buttons and some of the text entities are light pen detectable (i.e., when the area of the screen where they appear is touched with the light pen, the graphics program executes the task overlay which is associated with them).

An inspection of the interactive graphics program listing could serve as an introduction to the workings of the program. The comment cards give a pretty good indication of the items currently being displayed.

Items are displayed by the statement

```
CALL GENDF(ID,0)
```

where ID is a six-integer array identifying a text or polyline entity. These polyline entities are created in previous statements. Three statements commonly used in conjunction are

```
CALL ENSHFT(12HY= ...,2,Y,7H(F10.6))
```

```
CALL MODFY(ID,1,2,12HY=      )
```

```
CALL GENDF(ID,0)
```

These statements take the value Y in format F10.6 and place it after the equals sign of Y= . The text entity ID is then modified to reflect this new information and then this text entity is displayed.

*See NSRDC Technical Note CMD 42-28, August 1973.

BLOCK DATA CGRAF

The block data program assigns six integer values to the arrays to identify each text or polyline entity. It also stores information used in some of the text entities and light registers to display currently computed values. Some of the identifying values in BLOCK DATA CGRAF may be changed during program execution, but most of the values are preserved.

SUBROUTINE PLOTT(X1MIN,X1MAX,Y1MIN,Y1MAX)

This subroutine creates two polyline entities which graphically display the data stored in arrays X1 and Y1. Two polyline entities are created to display these data because of the way in which they were obtained. For example, PROGRAM AFU2 calls this subroutine to display velocity gradients computed in the initial flow integration on the upper surface. Since velocity gradients cannot be computed at the sonic point, calculations are made to a point just before and a point just after the sonic point. The point at which one set of values ends and the other set begins is stored in the word NNI(7). Using this information, the two polyline entities are created and displayed in this subroutine.

The arguments of this subroutine are:

X1MIN = least upper bound for x scaling
X1MAX = greatest lower bound for x scaling
Y1MIN = least upper bound for y scaling
Y1MAX = greatest lower bound for y scaling

If only one value is stored in Y1, a large X covers the graphical display.

SUBROUTINE PLOTT1(X1MIN,X1MAX,Y1MIN,Y1MAX)

This subroutine creates one polyline entity which graphically displays the data stored in arrays X1 and Y1.

The arguments of this subroutine are:

X1MIN = least upper bound for x scaling
X1MAX = greatest lower bound for x scaling
Y1MIN = least upper bound for y scaling
Y1MAX = greatest lower bound for y scaling

If only one value is stored in Y1, a large X covers the graphical display.

SUBROUTINE PLOTT2(X1MIN,X1MAX,Y1MIN,Y1MAX,Y2MIN,Y2MAX,J)

This subroutine creates two polyline entities which graphically display the data stored in X1 and Y1 and X1 and Y2.

The arguments of this subroutine are:

X1MIN = least upper bound for X1 scaling

X1MAX = greatest lower bound for X1 scaling

Y1MIN = least upper bound for Y1 scaling

Y1MAX = greatest lower bound for Y1 scaling

Y2MIN = least upper bound for Y2 scaling

Y2MAX = greatest lower bound for Y2 scaling

J = an indication of whether or not Y2 values shall be displayed

If only one value is stored in array Y1, a large X covers the graphical display.

SUBROUTINE AMXMNI(Y1MAX,Y1MIN)

This subroutine determines the largest and smallest values stored in array Y1.

The arguments of this subroutine are:

Y1MAX = largest value stored in Y1

Y1MIN = smallest value stored in Y1

SUBROUTINE AMXMN2(Y2MAX,Y2MIN)

This subroutine determines the largest and smallest values stored in array Y2.

The arguments of this subroutine are:

Y2MAX = largest value stored in Y2

Y2MIN = smallest value stored in Y2

SUBROUTINE AREA1(XMIN,XMAX,YMIN,YMAX)

This subroutine defines a subscreen area which covers the area defined by the screen coordinates (-40, -40) and (57, 57) and creates a grid display for this subscreen area.

The arguments of this subroutine are:

XMIN = smallest x value

XMAX = largest x value

YMIN = smallest y value

YMAX = largest x value

SUBROUTINE AREA2(XMIN,XMAX,YMIN,YMAX,ID)

This subroutine defines a subscreen area and creates a grid display for this subscreen area.

The arguments of this subroutine are:

XMIN = smallest x value

XMAX = largest x value

YMIN = smallest y value

YMAX = largest y value

ID = subscreen area

One of two subscreen areas can be defined according to the values of ID. If ID = 1, the defined subscreen area is covered by screen coordinates (-40, -40) and (57, 10). If ID = 2, the defined subscreen area is covered by screen coordinates (-40, 17) and (57, 57).

PROGRAM LIEN(INPUT,OUTPUT,TAPE5=INPUT,TAPE6=OUTPUT)

This program comprises the (0, 0) overlay and initiates execution of the graphic display files.

PROGRAM NPUT

This task reads input from punched cards and writes out some of the input on a line printer. The program writes out the label card which identifies the run and the data points and first derivatives at these data points which determine the airfoil shape being analyzed. Control is then automatically transferred to PROGRAM STUP.

PROGRAM STUP

This task creates the text entities and the light registers and light buttons used throughout the interactive graphics program.

The 59 data points required for the creation of the polyline entity NAIRFL are stored in X and Y arrays. When this entity is displayed, the airfoil shape is shown in the lower left-hand corner of the screen.

The text entities stored in COMMON blocks INPUT and NOUT are displayed in the lower right-hand corner of the screen. The 18 light registers corresponding to these text entities are displayed by using the same screen coordinates.

The text entities stored in COMMON blocks NPRCD are displayed in the lower left-hand corner of the screen. These entities display an asterisk which is either blinking or nonblinking. The nonblinking asterisks are light pen detectable and are capable of transferring program control to a particular task. The text entities stored in COMMON block NAXES are displayed in conjunction with the displays of the graphed output of a particular task.

PROGRAM STRT

This task displays the flow conditions in the lower right-hand corner of the screen. The flow conditions are displayed in the four text entities and are light pen detectable. The four text entities contain information in the free-stream Mach number, the angle of attack, and location of the outermost strip on the upper and lower surfaces. Two light buttons are also enabled, one of which allows program control to transfer to PROGRAM PRP1. The program is terminated by a call to subroutine WAITE and awaits an attention interrupt from an enabled attention source.

PROGRAM AFU1

This task erases all previous displays and displays information from subroutine IOUPRCT. The displayed text entities allow program control to be transferred to PROGRAM PRP3 or PRP4, or to PROGRAM STRT or PRP2. The program terminates and awaits an attention interrupt from an enabled attention source.

PROGRAM PRP3

This task retrieves the integer array of the text entity from which program control was transferred. If $ID(3) = 1$, LRSUPR was the attention source and if $ID(3) = 2$, LRSUB was the attention source. If $ID(3) = 2$, the program awaits an attention interrupt. If $ID(3) = 1$, the program erases all previous displays and displays the text entities and light buttons associated with PROGRAM AFU2. The program terminates and awaits an attention interrupt from an enabled attention source.

PROGRAM AFU2

This task displays information from subroutine IOUPRIN corresponding to initial flow integration on the upper surface. The two text entities display values of RBUB and UB, and the polyline entity graphically displays DUDX versus x . If the flow integration is complete, $NN2 = 1$, and the text entity which allows program control to be transferred to task PRP5 is displayed. The other two displayed text entities allow program control to be transferred to task STRT or PRP2. Two light buttons are also enabled, one of which allows program control to be transferred to task AFU2. The program terminates and awaits an attention interrupt from an enabled attention source.

PROGRAM AFL1

This task erases all previous displays and displays information from subroutine IOLWRCT. The displayed text entities allow program control to be transferred to task PRP3 or PRP4, or to task STRT or PRP2. The

program terminates and awaits an attention interrupt from an enabled attention source.

PROGRAM PRP4

This task retrieves the integer array of the text entity from which program control was transferred. If $ID(3) = 1$, LRSUPR was the attention source, and if $ID(3) = 2$, LRSUB was the attention source. If $ID(3) = 1$, the program awaits an attention interrupt. The task erases all previous displays and displays the text entities and light buttons associated with task AFL2. The program terminates and awaits an attention interrupt from an enabled attention source.

PROGRAM AFL2

This task displays information from subroutine IOLWRIN corresponding to flow integration on the lower surface. The three text entities display values of RBUB and UB and PO at the trailing edge, and the polyline entity graphically displays M_o versus x . If the flow integration is complete, $NN2 = 1$, and the text entity which allows program control to be transferred to task AFU1 is displayed. If $NN2 = 1$, the word $IGO(J) = 1$, and if $IGO(J) = 1$ for both upper and lower surfaces, the text entity which allows program control to be transferred to task PRP6 is displayed. The other two displayed text entities allow program control to be transferred to task STRT or PRP2. Two light buttons are also enabled, one of which allows program control to be transferred to task AFL2. The program terminates and awaits an attention interrupt from an enabled attention source.

PROGRAM PRP5

This task erases all previous displays and displays the text entities and light buttons associated with task AFU3. The program terminates and awaits an attention interrupt from an enabled attention source.

PROGRAM AFU3

This task displays information from subroutine IOSPECT2 corresponding to flow integration on the upper surface. The text entity displays the value of PO at the trailing edge and the polyline entities graphically display MO versus X. If the flow integration is complete, NN2 = 1, and the text entity which allows program control to be transferred to task AFL1 is displayed. If NN2 = 1, the word IGO(J) = 1, and if IGO(J) = 1 for both upper and lower surface, the text entity which allows program control to be transferred to task PRP6 is displayed. The three other text entities allow program control to be transferred to tasks PRP2, AFL1; AFU1, or PRP3. The program terminates and awaits an attention interrupt from an enabled attention source.

PROGRAM PRP6

This task erases all previous displays and displays the text entities and light buttons associated with task DWN1. The program terminates and awaits an attention interrupt from an enabled attention source.

PROGRAM DWN1

This task displays information from subroutine IODNSTM corresponding to downstream flow integration. The polyline entities display PO and P1 versus X. If flow integration is complete NN2 = 1, and the text entity which allows program control to be transferred to task DWN2 is displayed. The other four displayed text entities allow program control to be transferred to task PRP2, AFL1, or PRP5. Two light buttons are also enabled which allow program control to be transferred to task DWN1. The program terminates and awaits an attention interrupt from an enabled attention source.

PROGRAM DWN2

This task erases all previous displays and displays information from subroutine AKUTTA which contains the pressure distributions on the upper and lower surfaces. Three text entities are displayed which allow program

control to be transferred to tasks PRP2, AFL1, and AFU1. The program terminates and awaits an attention interrupt from an enabled attention source.

PROGRAM CVLI

This task retrieves the integer array of the text entity from which program control was transferred. The text entity is erased and replaced by a light register which has the same code number as the first integer of the text entity. The task then awaits keyboard information to be typed in. When a new value is typed in and the keyboard release button is activated, the light register will be replaced with a text entity with the typed-in value. The task terminates and awaits an attention interrupt from an enabled attention source.

PROGRAM CVLR

This task is structured identically to task CVLI. The keyboard information is typed in under a different format, however.

PROGRAM STOP

This task erases the screen display and releases the console from the computer.

PROGRAM CHGV

This task computes a new value for the normal velocity component of the innermost strip according to $LL(J)$. If $J = 2$, the Lagrangian function is used, and if $J = 3$, the parabolic function is used.

APPENDIX E INPUT DESCRIPTION FOR INTERACTIVE GRAPHICS

CARD 1 FORMAT(I2,8X,7A10)

Columns	Description
1-2	Console number
11-80	Title for the run

CARD 2 FORMAT(2I2)

Columns	Description
1-2	NP(1) number of data points on upper surface of airfoil
3-4	NP(2) number of data points on lower surface of airfoil

CARDS SET 1 FORMAT(3F20.15)

Columns	Description
1-20	XX(1,1) x-coordinate
21-40	YY(1,1) y-coordinate
41-60	AM(1,1) first derivative at this point

CARDS SET 2

Columns	Description
1-20	XX(1,2) x-coordinate on lower surface
21-40	YY(1,2) y-coordinate on lower surface
41-60	AM(1,2) first derivative at this point

Format is repeated for remainder of airfoil data points

CARD SET 3

CARD 1

Columns	Description
1-10	blank
11-20	DV00I initial cross velocity gradient
21-30	XS stagnation point
31-40	XAO initial point upper surface

CARD SET 3 - CARD 1 (cont.)

Columns	Description
41-50	CYDU flow parameter upper surface
51-60	XAI initial point lower surface
61-70	CYDL flow parameter lower surface
71-80	SL shock location

CARD 2

Columns	Description
1-10	XOO distance from first station of upstream integration to airfoil surface
11-20	RMT Mach number used in upstream flow integration, $\approx 0.95 M_{\infty}$
21-30	CDY ≈ 0.1
31-40	YU location of outermost strip on upper surface
41-50	YL location of outermost strip on lower surface
51-60	CS a point in subcritical flow calculations where a new integration scheme is adopted
61-70	RMC ≈ 0.92 Mach number upper limit for subroutine SPRCRT1
71-80	BETAD angle of shock foot for subroutine SPRCRT2

CARD 3 FORMAT(8F10.6)

Columns	Description
1-10	DELS 0 for isentropic flow and 1 for nonisentropic flow through shock foot in subroutine SPRCRT2
11-20	CDDQ ≈ 11.0 upper limit for DDQ in subroutine SPRCRT2
21-30	RKI ≈ 5.0 exponent for normal velocity component in downstream integration

CARD 4 FORMAT(6I1,4X,7F10.6)

Columns	Description
1	NN1 number of strips used in upstream integration
2	NA2 number of additional strips used near final station of upstream integration
3	NN3 number of strips used in initial solution of upper surface flow integration
4	NN4 number of strips used in initial solution of lower surface flow integration
5	NN5 number of strips used in flow solution along the upper surface
6	NN6 intermediate strip used in calculating downstream flow conditions

EXAMPLE INPUT/OUTPUT

This example corresponds to the output which was given for the demonstration of the interactive graphics program for an advanced airfoil. In a real situation, however, there would be a greater amount of output corresponding to the trial solutions for the various solution processes. The input and output for this example represent only the solutions which are known to be correct.

The following represents a deck for a graphics run:

```

CXXX,CM20000,P4,G.
CHARGE,CXXX,000000000.
ATTACH(IGSGO,CAMVIGSGO)
ATTACH(ATSK,CXXXATSK)
IGSGO(ATSK,1)
7/8/9
01      TRANSONIC FLOW PAST AN ADVANCED AIRFOIL
0.7      1.5
         6.0      .004      .0125      1.564133      .018      .6946      .485
2.5      .68      .1      7.0      7.0      .045      .92      90.0
0.0      11.0      5.0
.536653      0.02      .0002      .002      .005      .02
2222
0.0      0.0      5.400000000000000
.0125      .0304      .879686323493225

```


.05	.0519	.370509412053975
.1	.06529	.194774312423792
.149999999999999	.07893	.098052334572903
.249999999999999	.0832	.073397323457582
.299999999999999	.0863	.050558371596735
.349999999999998	.08826	.0279691901555
.399999999999999	.08912	.006764867781260
.449999999999998	.08912	.006764867781280
.449999999999998	.08896	.013028661280615
.499999999999998	.08782	.032650222658823
.549999999999997	.08568	.053170448084134
.599999999999998	.08247	.075067985004662
.649999999999996	.0723	.132701567406445
.749999999999996	.06476	.169436118476982
.799999999999997	.05533	.207753958685581
.849999999999998	.04899	.245748046780653
.899999999999995	.08078	.282253854191833
.949999999999996	.0159	.310636536452030
.999999999999996	0.0	.321999999999999
0.0	0.0	5.050000000000011
.0125	.03	.992163451845627
.050	.05333	.379092385234589
.1	.06639	.180750933111021
.149999999999999	.07356	.111703882321330
.199999999999999	.07802	.069633537603695
.249999999999999	.0807	.038161967263869
.299999999999999	.08193	.012318593340822
.349999999999998	.08199	.009436340627176
.399999999999999	.08096	.032773230832096
.449999999999998	.07865	.060470736044399
.499999999999998	.0748	.094943824990326
.549999999999997	.069	.13875396399439
.599999999999998	.0607	.196040319032322
.649999999999995	.0495	.247084759876374
.699999999999996	.0366	.261620641462178

.7499999999999996	.024	.236432674274866
.7999999999999997	.0134	.184648661438304
.8499999999999998	.00581	.1163726799718
.8999999999999995	.002	.033860618674168
.9499999999999996	.0026	.059215154668539
.9999999999999996	.00805	.16

TRANSONIC FLOW PAST AN ADVANCED AIROFOIL

X(UPPER)	Y(UPPER)	DY/DX(UPPER)	X(LOWER)	Y(LOWER)	DY/DX(LOWER)
0.000000000000	0.000000000000	5.400000000000	0.000000000000	0.000000000000	5.050000000000
.012500000000	.030400000000	.879686323493	.012500000000	.030000000000	.992163451846
.050000000000	.051900000000	.370509412054	.050000000000	.053330000000	.379092385235
.100000000000	.065290000000	.194774312424	.100000000000	.066400000000	.180750933111
.150000000000	.073250000000	.131393338251	.150000000000	.073560000000	.111703882321
.200000000000	.078930000000	.098052334573	.200000000000	.078020000000	.069633537604
.250000000000	.083200000000	.073397323458	.250000000000	.080700000000	.038161967264
.300000000000	.086300000000	.050558371597	.300000000000	.081930000000	.012318593341
.350000000000	.088260000000	.027969190156	.350000000000	.082000000000	-.009436340627
.400000000000	.089120000000	.006764867781	.400000000000	.080960000000	-.032773230832
.450000000000	.088960000000	-.013028661281	.450000000000	.078650000000	-.060470736044
.500000000000	.087820000000	-.032650222659	.500000000000	.074800000000	-.094943824990
.550000000000	.085680000000	-.053170448084	.550000000000	.069000000000	-.138753963994
.600000000000	.082480000000	-.075067985005	.600000000000	.060700000000	-.196040319032
.650000000000	.078110000000	-.100757611897	.650000000000	.049500000000	-.247084759876
.700000000000	.072300000000	-.132701567406	.700000000000	.036600000000	-.261620641462
.750000000000	.064760000000	-.169436118477	.750000000000	.024000000000	-.236432674275
.800000000000	.055330000000	-.207753958686	.800000000000	.013400000000	-.184648661438
.850000000000	.043990000000	-.245748046781	.850000000000	.005810000000	-.116372679972
.900000000000	.030780000000	-.282253854192	.900000000000	.002000000000	-.033860618674
.950000000000	.015900000000	-.310636536452	.950000000000	.002600000000	.059215154669
1.000000000000	0.000000000000	-.322000000000	1.000000000000	.008050000000	.160000000000

MACH NO.= .700000

ALPHA= 1.500000

***** UPSTREAM SOLUTION *****

NM = 5, NA = 3

DV00(I) = 6.0000, X00 = 2.5000, RMT = .6800, CDY = .1000, H = .0200

YINF(UPPER) = 7.0000, YINF(LOWER) = 7.0000

X	MO	X	MO
0.00000	.700000	1.58000	.664379
.06000	.700000	1.64000	.662260
.12000	.699999	1.70000	.660010
.18000	.699999	1.76000	.657632
.24000	.699963	1.82000	.655128
.30000	.699888	1.88000	.652501
.36000	.699720	1.94000	.649753
.42000	.699396	1.95500	.647770
.48000	.698823	1.97000	.644476
.54000	.697881	1.98500	.639939
.60000	.696420	2.00000	.634252
.66000	.694254	2.01500	.627485
.72000	.691164	2.03000	.619631
.78000	.686901	2.04500	.610553
.84000	.681189	2.06000	.599998
.86000	.678913	2.07500	.587490
.92000	.678489	2.09000	.572452
.98000	.677921	2.10500	.554204
1.04000	.677209	2.12000	.532026
1.10000	.676353	2.13500	.505221
1.16000	.675353	2.15000	.473153
1.22000	.674210	2.16000	.448560
1.28000	.672923	2.17500	.406421
1.34000	.671493	2.18000	.390875
1.40000	.669923	2.19500	.339260
1.46000	.668212	2.20100	.316505
1.52000	.666363	2.20700	.292347

Y	M	Y	M
7.000000	.700000	.234647	.730981
3.502907	.701421	.128829	.733025
1.754687	.700521	.076939	.727602
.883280	.704802	.001139	.292347
.451885	.714635		

DE = .056000

YSO = .012598

INITIAL VELOCITY PROFILE

UPPER SURFACE			LOWER SURFACE		
Y	U	V	Y	U	V
7.000000	1.000000	0.000000	7.000000	1.000000	0.000000
3.502907	1.001827	.006582	3.502907	1.001580	.006585
1.754687	1.000620	.010738	1.754687	1.000252	.010738
.883280	1.006074	.018385	.883282	1.005286	.018396
.451885	1.018548	.029913	.451889	1.017053	.029932
.234647	1.037219	.076927	.234635	1.034252	.077056
.128829	1.031526	.152198	.128809	1.027078	.152380
.076939	1.010017	.229310	.076917	1.004665	.229294
.001139	.432725	.032349	-.001139	.432725	-.032349

*****STAGNATION SOLUTION*****

XS = .004000

FROM THE UPSTREAM SOLUTION, DE = .056000, YSO = .012598

AIRFOIL COORDINATES

X	Y(UPPER)	Y(LOWER)	X	Y(UPPER)	Y(LOWER)
0.000000	0.000000	0.000000	.015000	.032128	-.032781
.000600	.003099	-.002934	.015600	.032605	-.033348
.001200	.005957	-.005655	.016200	.033073	-.033907
.001800	.008587	-.008172	.016800	.033535	-.034457
.002400	.010999	-.010496	.017400	.033989	-.034998
.003000	.013205	-.012637	.018000	.034437	-.035530
.003600	.015218	-.014605	.018600	.034877	-.036054
.004200	.017049	-.016411	.019200	.035311	-.036570
.004800	.018710	-.018065	.019800	.035737	-.037077
.005400	.020212	-.019577	.020400	.036157	-.037577
.006000	.021568	-.020958	.021000	.036570	-.038068
.006600	.022788	-.022217	.021600	.036977	-.038552
.007200	.023885	-.023356	.022200	.037378	-.039027
.007800	.024871	-.024415	.022800	.037772	-.039495
.008400	.025756	-.025373	.023400	.038159	-.039956
.009000	.026554	-.026251	.024000	.038541	-.040409
.009600	.027275	-.027059	.024600	.038917	-.040855
.010200	.027932	-.027809	.025200	.039287	-.041293
.010800	.028536	-.028509	.025800	.039650	-.041725
.011400	.029099	-.029171	.026400	.040009	-.042150
.012000	.029632	-.029834	.027000	.040361	-.042567
.012600	.030148	-.030419	.027600	.040708	-.042979
.013200	.030654	-.031023	.028200	.041049	-.043383
.013800	.031153	-.031618	.028800	.041385	-.043781
.014400	.031645	-.032204	.029400	.041716	-.044173

STAGNATION STREAMLINE

X	Y	X	Y
-.052000	-.027285	-.018400	-.022703
-.046400	-.026975	-.012800	-.021328
-.040800	-.026346	-.007200	-.019735
-.035200	-.025681	-.001600	-.017906
-.029600	-.024863	.004000	-.015826
-.024000	-.023876		

YS = .015826

DV00(F) = 6.018846

*****TEST OF CRITICALITY*****
UPPER SURFACE

FROM THE UPSTREAM SOLUTION, NN = 9, DE = .056000

FROM THE STAGNATION SOLUTION, YS = .015026, YSO = .012598

XB	MB	XB	MB
.0006	.3663	.0033	.6187
.0011	.4120	.0039	.6844
.0017	.4592	.0044	.7661
.0022	.5086	.0050	.9021
.0028	.5612		

***** INITIAL SOLUTION *****
UPPER SURFACE

NN = 6, XAO = .012500, CYD = 1.56413300, RMC = .920000, HS = .000200

RBUB = .984972 UB = .971579

XB	MB	PB	DUDX	XB	MB	PB	DUDX
.0138	.6857	1.0127	16.2850	.0305	.9487	.7772	15.8738
.0142	.6932	1.0061	16.3241	.0308	.9528	.7736	15.8377
.0147	.7007	.9994	16.3604	.0311	.9569	.7700	15.8002
.0152	.7083	.9926	16.3938	.0313	.9609	.7665	15.7613
.0157	.7159	.9858	16.4243				
.0162	.7235	.9789	16.4518	.0362	1.0328	.7049	15.0170
.0166	.7312	.9720	16.4763	.0367	1.0409	.6982	14.9235
.0171	.7389	.9651	16.4977	.0373	1.0489	.6915	14.8216
.0176	.7467	.9581	16.5159	.0378	1.0569	.6849	14.7189
.0181	.7544	.9511	16.5310	.0382	1.0622	.6805	14.6504
.0186	.7622	.9441	16.5429	.0388	1.0701	.6740	14.5481
.0191	.7701	.9370	16.5516	.0393	1.0780	.6675	14.4477
.0196	.7779	.9299	16.5570	.0399	1.0859	.6610	14.3513
.0201	.7858	.9228	16.5591	.0403	1.0912	.6568	14.2907
.0206	.7937	.9156	16.5578	.0408	1.0991	.6504	14.2089
.0211	.8017	.9084	16.5532	.0412	1.1043	.6462	14.1639
.0216	.8097	.9012	16.5452	.0418	1.1020	.6480	-3.9720
.0221	.8176	.8940	16.5337	.0423	1.1000	.6496	-3.3607
.0226	.8257	.8868	16.5187	.0429	1.0984	.6509	-2.7361
.0231	.8337	.8796	16.5001	.0434	1.0971	.6520	-2.1054
.0236	.8417	.8723	16.4780	.0440	1.0962	.6527	-1.4765
.0241	.8498	.8651	16.4522	.0446	1.0956	.6532	-.8575
.0247	.8579	.8578	16.4227	.0451	1.0953	.6534	-.2568
.0252	.8660	.8505	16.3894	.0457	1.0954	.6534	.3178
.0257	.8741	.8433	16.3521	.0463	1.0958	.6531	.8593
.0262	.8822	.8360	16.3106	.0468	1.0965	.6525	1.3616
.0267	.8903	.8288	16.2649	.0474	1.0974	.6518	1.8201
.0273	.8984	.8215	16.2144	.0480	1.0985	.6508	2.2314
.0274	.9011	.8191	16.1965	.0485	1.0999	.6497	2.5934
.0277	.9052	.8155	16.1947	.0491	1.1015	.6485	2.9053
.0280	.9093	.8119	16.1691	.0497	1.1032	.6471	3.1670
.0282	.9134	.8083	16.1427	.0503	1.1050	.6456	3.3795
.0285	.9174	.8047	16.1153	.0508	1.1070	.6441	3.5442
.0287	.9202	.8023	16.0965	.0514	1.1090	.6424	3.6628
.0289	.9242	.7987	16.0676	.0520	1.1111	.6408	3.7624
.0292	.9283	.7951	16.0378	.0526	1.1132	.6391	3.8555
.0295	.9324	.7915	16.0070	.0531	1.1154	.6373	3.9400
.0297	.9365	.7879	15.9752	.0537	1.1176	.6355	4.0163
.0300	.9406	.7843	15.9425	.0543	1.1199	.6337	4.0847
.0303	.9446	.7807	15.9087	.0545	1.1207	.6331	4.1058

***** AIRFOIL SOLUTION *****
UPPER SURFACE

NC = 5

SHOCK LOC. = .485000, BETA = 90.000000, DELS = 0.000000, CDDQ = 11.000000, MO = .003000
FROM INITIAL CONDITIONS, NN = 6, X(INIT) = .053100

INTERMEDIATE VELOCITY DISTRIBUTION USING LAGRANGIAN FUNCTION

Y	U	V	Y	U	V
6.971576	1.000000	0.000000	.856865	1.026044	.017403
3.475218	1.006400	.006529	.426659	1.003837	.183356
1.727478	1.007842	.010959	.051615	1.426226	.463849

X	MO	PO	DUOX	DDQ	X	MO	PO	DUOX	DDQ
.0621	1.1373	.6200	1.1337	-3.7580	.4103	1.3150	.4905	-.0842	-.3130
.0711	1.1585	.6035	1.1038	-3.1607	.4253	1.3022	.4991	-.0895	-.3103
.0800	1.1817	.5858	1.0809	-2.3741	.4403	1.2890	.5081	-.0946	-.3077
.0890	1.2057	.5678	1.0647	-1.4564	.4553	1.2756	.5175	-.0997	-.3051
.0980	1.2298	.5501	1.0570	-.4454	.4706	1.2617	.5272	-.1048	-.3058
.1108	1.2634	.5260	1.0611	.5477	.4856	1.2475	.5373	-.1097	-.3073
.1258	1.3004	.5003	1.0742	1.3344	.5156	.8136	.8977	-.0439	0.0000
.1408	1.3353	.4770	1.0996	2.2770	.5456	.8112	.8998	-.0527	0.0000
.1558	1.3677	.4561	1.1405	3.4859	.5756	.8069	.9037	-.0617	0.0000
.1706	1.3972	.4376	1.2001	4.8571	.6056	.8008	.9093	-.0706	0.0000
.1856	1.4237	.4215	1.2865	7.0045	.6361	.7927	.9165	-.0802	0.0000
.2006	1.4470	.4078	1.4200	10.9717	.6661	.7827	.9256	-.0905	0.0000
.2156	1.4670	.3963	1.6563	20.0125	.6961	.7708	.9363	-.1016	0.0000
.2306	1.4558	.4027	-.0144	-.3461	.7261	.7570	.9488	-.1133	0.0000
.2456	1.4446	.4092	-.0206	-.3391	.7566	.7414	.9629	-.1247	0.0000
.2606	1.4334	.4158	-.0266	-.3333	.7866	.7244	.9782	-.1355	0.0000
.2756	1.4220	.4225	-.0326	-.3346	.8166	.7062	.9945	-.1448	0.0000
.2906	1.4106	.4294	-.0385	-.3358	.8471	.6871	1.0115	-.1525	0.0000
.3056	1.3991	.4364	-.0445	-.3369	.8771	.6674	1.0290	-.1585	0.0000
.3203	1.3875	.4436	-.0503	-.3269	.9071	.6471	1.0468	-.1622	0.0000
.3353	1.3758	.4509	-.0562	-.3342	.9376	.6266	1.0646	-.1632	0.0000
.3503	1.3640	.4584	-.0620	-.3325	.9676	.6060	1.0823	-.1603	0.0000
.3653	1.3520	.4661	-.0677	-.3289	.9981	.5857	1.0996	-.1535	0.0000
.3803	1.3399	.4740	-.0733	-.3237	1.0106	.5790	1.1052	-.1505	0.0000
.3953	1.3276	.4821	-.0788	-.3182					

*****DOWNSTREAM SOLUTION*****

NN = 3, H = .020000, RK = 5.000000

FROM UPPER SURFACE INTEGRATION, SHOCK LOC. = .4850, BETA = 90.0000, CS = 1.0000, CZ = 11.2041

X	MO	PO	P1	X	MO	PO	P1
1.0000	.5775	1.1065	.9936	5.6400	.3328	1.2847	.8840
1.1600	.5759	1.1078	.9932	5.7200	.3275	1.2878	.8790
1.2400	.5742	1.1093	.9927	5.8000	.3224	1.2907	.8739
1.3200	.5724	1.1108	.9922	5.8800	.3175	1.2935	.8688
1.4000	.5704	1.1125	.9918	5.9600	.3127	1.2962	.8636
1.4800	.5683	1.1142	.9913	6.0400	.3080	1.2988	.8584
1.5600	.5662	1.1160	.9908	6.1200	.3036	1.3012	.8532
1.6400	.5639	1.1179	.9902	6.2000	.2993	1.3035	.8481
1.7200	.5615	1.1198	.9897	6.2800	.2953	1.3056	.8430
1.8000	.5591	1.1219	.9892	6.3600	.2915	1.3077	.8381
1.8800	.5565	1.1240	.9886	6.4400	.2879	1.3095	.8334
1.9600	.5538	1.1262	.9880	6.5200	.2845	1.3113	.8289
2.0400	.5510	1.1285	.9874	6.6000	.2814	1.3129	.8247
2.1200	.5481	1.1308	.9868	6.6800	.2785	1.3143	.8208
2.2000	.5452	1.1333	.9862	6.7600	.2759	1.3157	.8172
2.2800	.5421	1.1358	.9855	6.8400	.2735	1.3169	.8141
2.3600	.5389	1.1384	.9848	6.9200	.2713	1.3179	.8114
2.4400	.5356	1.1411	.9841	7.0000	.2694	1.3189	.8092
2.5200	.5322	1.1438	.9833	7.0800	.2676	1.3197	.8074
2.6000	.5287	1.1466	.9826	7.1600	.2661	1.3205	.8062
2.6800	.5251	1.1495	.9817	7.2400	.2648	1.3211	.8053
2.7600	.5214	1.1525	.9808	7.3200	.2636	1.3217	.8049
2.8400	.5176	1.1555	.9799	7.4000	.2626	1.3222	.8047
2.9200	.5136	1.1586	.9790	7.4800	.2618	1.3226	.8049
3.0000	.5096	1.1618	.9779	7.5600	.2611	1.3229	.8052
3.0800	.5055	1.1651	.9768	7.6400	.2604	1.3232	.8056
3.1600	.5012	1.1684	.9757	7.7200	.2599	1.3234	.8061
3.2400	.4968	1.1718	.9745	7.8000	.2595	1.3237	.8065
3.3200	.4924	1.1753	.9732	7.8800	.2591	1.3238	.8069
3.4000	.4878	1.1788	.9718	7.9600	.2588	1.3240	.8071
3.4800	.4831	1.1824	.9703	8.0400	.2585	1.3241	.8072
3.5600	.4783	1.1851	.9688	8.1200	.2582	1.3242	.8071
3.6400	.4733	1.1898	.9671	8.2000	.2580	1.3244	.8069
3.7200	.4683	1.1936	.9654	8.2800	.2578	1.3244	.8064
3.8000	.4632	1.1974	.9635	8.3600	.2577	1.3245	.8057
3.8800	.4580	1.2013	.9616	8.4400	.2575	1.3246	.8049
3.9600	.4527	1.2052	.9595	8.5200	.2575	1.3246	.8038
4.0400	.4473	1.2091	.9573	8.6000	.2575	1.3246	.8027
4.1200	.4418	1.2131	.9550	8.6800	.2575	1.3246	.8015
4.2000	.4363	1.2171	.9525	8.7600	.2577	1.3245	.8003
4.2800	.4307	1.2211	.9500	8.8400	.2579	1.3244	.7991
4.3600	.4250	1.2251	.9472	8.9200	.2583	1.3242	.7981
4.4400	.4192	1.2291	.9444	9.0000	.2588	1.3240	.7973
4.5200	.4135	1.2331	.9414	9.0800	.2594	1.3237	.7969
4.6000	.4076	1.2371	.9382	9.1600	.2602	1.3233	.7969
4.6800	.4018	1.2411	.9349	9.2400	.2613	1.3228	.7974
4.7600	.3959	1.2451	.9315	9.3200	.2625	1.3222	.7984
4.8400	.3900	1.2490	.9279	9.4000	.2640	1.3215	.8000
4.9200	.3841	1.2529	.9241	9.4800	.2656	1.3207	.8022
5.0000	.3782	1.2567	.9202	9.5600	.2676	1.3198	.8050
5.0800	.3723	1.2605	.9162	9.6400	.2697	1.3187	.8083
5.1600	.3665	1.2642	.9120	9.7200	.2721	1.3175	.8120
5.2400	.3607	1.2679	.9076	9.8000	.2748	1.3162	.8162
5.3200	.3549	1.2714	.9032	9.8800	.2777	1.3148	.8206
5.4000	.3493	1.2749	.8986	9.9600	.2808	1.3132	.8254
5.4800	.3437	1.2783	.8938	10.0200	.2841	1.3115	.8303
5.5600	.3382	1.2815	.8890				

*****TEST OF CRITICALITY*****
LOWER SURFACE

FROM THE UPSTREAM SOLUTION, NN = 9, DE = .056000

FROM THE STAGNATION SOLUTION, YS = .015826, YSO = .012598

XB	MB	XB	MB
.0055	.1882	.0171	.6167
.0083	.3657	.0200	.6923
.0112	.4681	.0230	.7805
.0141	.5434	.0259	.9460

*****AIRFOIL SOLUTION*****
LOWER SURFACE

NB = 6

XA = .0180, CYD = .6946, CX = .0450, HSO = .0020, HO = .0050

RBUB = .790322 UB = .699485

XB	MB	PB	DUOX	XB	MB	PB	DUOX
.0185	.4892	1.1777	7.9648	.0328	.5799	1.1045	5.6320
.0200	.5005	1.1690	7.8586	.0345	.5875	1.0981	5.1569
.0215	.5116	1.1602	7.7195	.0362	.5944	1.0923	4.6380
.0231	.5225	1.1516	7.5449	.0380	.6004	1.0871	4.0781
.0246	.5331	1.1430	7.3325	.0397	.6056	1.0827	3.4817
.0262	.5434	1.1347	7.0798	.0415	.6099	1.0791	2.8547
.0278	.5533	1.1266	6.7849	.0433	.6131	1.0762	2.2047
.0294	.5628	1.1188	6.4460	.0451	.6154	1.0743	1.5407
.0311	.5717	1.1114	6.0618	.0451	.6154	1.0743	1.5407

INTERMEDIATE VELOCITY DISTRIBUTION

Y	U	V	Y	U	V
7.028424	1.000000	0.000000	.913593	1.025205	.013297
3.532024	1.006643	.006752	.483282	1.072600	.029165
1.784255	1.007989	.011303	.139683	.814474	.354417

XB	MB	PB	DUOX	XB	MB	PB	DUOX
.0617	.6247	1.0662	.4506	.5472	.9010	.8192	-.3811
.0770	.6364	1.0561	.3804	.5622	.8901	.8289	-.4529
.0920	.6495	1.0447	.3211	.5772	.8748	.8426	-.5305
.1070	.6635	1.0324	.2812	.5920	.8556	.8598	-.6105
.1220	.6772	1.0203	.2502	.6070	.8332	.8800	-.6934
.1372	.6903	1.0087	.2202	.6220	.8082	.9026	-.7619
.1522	.7029	.9974	.1931	.6367	.7820	.9263	-.8084
.1672	.7151	.9865	.1682	.6517	.7556	.9501	-.8341
.1822	.7268	.9760	.1443	.6667	.7294	.9737	-.8415
.1972	.7381	.9659	.1218	.6815	.7039	.9965	-.8291
.2125	.7491	.9560	.1005	.6965	.6796	1.0182	-.8006
.2275	.7597	.9464	.0795	.7112	.6567	1.0384	-.7590
.2425	.7700	.9371	.0586	.7262	.6356	1.0568	-.7093
.2575	.7799	.9281	.0378	.7412	.6163	1.0735	-.6524
.2725	.7895	.9194	.0177	.7560	.5991	1.0883	-.5900
.2875	.7989	.9110	-.0014	.7710	.5840	1.1011	-.5264
.3025	.8081	.9027	-.0194	.7860	.5710	1.1119	-.4622
.3175	.8172	.8944	-.0365	.8007	.5602	1.1210	-.3979
.3325	.8262	.8863	-.0534	.8157	.5514	1.1282	-.3344
.3475	.8352	.8782	-.0701	.8307	.5447	1.1336	-.2697
.3625	.8442	.8701	-.0864	.8457	.5403	1.1372	-.2043
.3775	.8531	.8621	-.1029	.8607	.5383	1.1389	-.1377
.3925	.8619	.8542	-.1196	.8757	.5389	1.1384	-.0696
.4075	.8704	.8466	-.1363	.8905	.5423	1.1356	-.0002
.4225	.8786	.8393	-.1533	.9055	.5489	1.1302	.0738
.4375	.8861	.8325	-.1703	.9205	.5592	1.1218	.1522
.4525	.8929	.8265	-.1875	.9355	.5738	1.1096	.2365
.4675	.8984	.8215	-.2050	.9507	.5937	1.0928	.3304
.4825	.9023	.8181	-.2229	.9657	.6204	1.0700	.4343
.4975	.9041	.8165	-.2412	.9807	.6560	1.0390	.5534
.5022	.9041	.8165	-.2474	.9957	.7051	.9955	.6924
.5172	.9079	.8131	-.2515	1.0020	.7123	.9890	.7440
.5322	.9071	.8139	-.3137				

***** AIRFOIL SOLUTION *****
UPPER SURFACE

MC = 5

SHOCK LOC. = .485080, BETA = 90.000000, DELS = 0.000000, CDDQ = 11.000000, MO = .003000
FROM INITIAL CONDITIONS, MN = 6, X(INIT) = .053100

INTERMEDIATE VELOCITY DISTRIBUTION USING LAGRANGIAN FUNCTION

Y	U	V	Y	U	V
6.971576	1.000000	0.000000	.856865	1.026044	.017403
3.475218	1.006400	.006529	.426659	1.083837	.183356
1.727478	1.007842	.010959	.051615	1.426226	.463849

X	MO	PO	DUOX	DOQ	X	MO	PO	DUOX	DOQ
.0621	1.1373	.6200	1.1337	-3.7580	.4103	1.3150	.4905	-.0842	-.3130
.0711	1.1505	.6035	1.1038	-3.1607	.4253	1.3022	.4991	-.0895	-.3103
.0800	1.1817	.5858	1.0809	-2.3741	.4403	1.2890	.5081	-.0946	-.3077
.0890	1.2057	.5678	1.0647	-1.4564	.4553	1.2756	.5175	-.0997	-.3051
.0980	1.2298	.5501	1.0570	-.4454	.4706	1.2617	.5272	-.1048	-.3058
.1100	1.2634	.5260	1.0611	.5477	.4856	1.2475	.5373	-.1097	-.3073
.1258	1.3004	.5003	1.0742	1.3344	.5156	.8136	.8977	-.0439	0.0000
.1408	1.3353	.4770	1.0996	2.2770	.5456	.8112	.8998	-.0527	0.0000
.1558	1.3677	.4561	1.1405	3.4859	.5756	.8069	.9037	-.0617	0.0000
.1706	1.3972	.4376	1.2001	4.8571	.6056	.8008	.9093	-.0706	0.0000
.1856	1.4237	.4215	1.2865	7.0045	.6361	.7927	.9165	-.0802	0.0000
.2006	1.4470	.4078	1.4200	10.9717	.6661	.7827	.9256	-.0905	0.0000
.2156	1.4670	.3963	1.6563	20.0125	.6961	.7708	.9363	-.1016	0.0000
.2306	1.4558	.4027	-.0144	-.3461	.7261	.7570	.9488	-.1133	0.0000
.2456	1.4446	.4092	-.0206	-.3391	.7566	.7414	.9629	-.1247	0.0000
.2606	1.4334	.4158	-.0266	-.3333	.7866	.7244	.9782	-.1355	0.0000
.2756	1.4220	.4225	-.0326	-.3346	.8166	.7062	.9945	-.1448	0.0000
.2906	1.4106	.4294	-.0385	-.3358	.8471	.6871	1.0115	-.1525	0.0000
.3056	1.3991	.4364	-.0445	-.3369	.8771	.6674	1.0290	-.1585	0.0000
.3203	1.3875	.4436	-.0503	-.3269	.9071	.6471	1.0468	-.1622	0.0000
.3353	1.3758	.4509	-.0562	-.3342	.9376	.6266	1.0646	-.1632	0.0000
.3503	1.3640	.4584	-.0620	-.3325	.9676	.6060	1.0823	-.1603	0.0000
.3653	1.3520	.4661	-.0677	-.3289	.9981	.5857	1.0996	-.1535	0.0000
.3803	1.3399	.4740	-.0733	-.3237	1.0106	.5790	1.1052	-.1505	0.0000
.3953	1.3276	.4821	-.0788	-.3182					

*****DOWNSTREAM SOLUTION*****

NU = 3, H = .020000, RK = 5.000000

FROM UPPER SURFACE INTEGRATION, SHOCK LOC. = .4850, BETA = 90.0000, CS = 1.0000, CZ = 11.2041

X	MO	PO	P1	X	MO	PO	P1
1.0800	.5775	1.1065	.9936	5.6400	.3328	1.2847	.8840
1.1600	.5759	1.1078	.9932	5.7200	.3275	1.2878	.8730
1.2400	.5742	1.1093	.9927	5.8000	.3224	1.2907	.8739
1.3200	.5724	1.1108	.9922	5.8800	.3175	1.2935	.8688
1.4000	.5704	1.1125	.9918	5.9600	.3127	1.2962	.8636
1.4800	.5683	1.1142	.9913	6.0400	.3080	1.2988	.8584
1.5600	.5662	1.1160	.9908	6.1200	.3036	1.3012	.8532
1.6400	.5639	1.1179	.9902	6.2000	.2993	1.3035	.8481
1.7200	.5615	1.1198	.9897	6.2800	.2953	1.3056	.8430
1.8000	.5591	1.1219	.9892	6.3600	.2915	1.3077	.8381
1.8800	.5565	1.1240	.9886	6.4400	.2879	1.3095	.8334
1.9600	.5538	1.1262	.9880	6.5200	.2845	1.3113	.8289
2.0400	.5510	1.1285	.9874	6.6000	.2814	1.3129	.8247
2.1200	.5481	1.1308	.9868	6.6800	.2785	1.3143	.8208
2.2000	.5452	1.1333	.9862	6.7600	.2759	1.3157	.8172
2.2800	.5421	1.1358	.9855	6.8400	.2735	1.3169	.8141
2.3600	.5389	1.1384	.9848	6.9200	.2713	1.3179	.8114
2.4400	.5356	1.1411	.9841	7.0000	.2694	1.3189	.8092
2.5200	.5322	1.1438	.9833	7.0800	.2676	1.3197	.8074
2.6000	.5287	1.1466	.9826	7.1600	.2661	1.3205	.8052
2.6800	.5251	1.1495	.9817	7.2400	.2648	1.3211	.8053
2.7600	.5214	1.1525	.9808	7.3200	.2636	1.3217	.8049
2.8400	.5176	1.1555	.9799	7.4000	.2626	1.3222	.8047
2.9200	.5136	1.1586	.9790	7.4800	.2618	1.3226	.8049
3.0000	.5096	1.1618	.9779	7.5600	.2611	1.3229	.8052
3.0800	.5055	1.1651	.9768	7.6400	.2604	1.3232	.8056
3.1600	.5012	1.1684	.9757	7.7200	.2599	1.3234	.8051
3.2400	.4968	1.1718	.9745	7.8000	.2595	1.3237	.8055
3.3200	.4924	1.1753	.9732	7.8800	.2591	1.3238	.8069
3.4000	.4878	1.1788	.9718	7.9600	.2588	1.3240	.8071
3.4800	.4831	1.1824	.9703	8.0400	.2585	1.3241	.8072
3.5600	.4783	1.1861	.9688	8.1200	.2582	1.3242	.8071
3.6400	.4733	1.1898	.9671	8.2000	.2580	1.3244	.8069
3.7200	.4683	1.1935	.9654	8.2800	.2578	1.3244	.8064
3.8000	.4632	1.1974	.9635	8.3600	.2577	1.3245	.8057
3.8800	.4580	1.2013	.9616	8.4400	.2575	1.3246	.8049
3.9600	.4527	1.2052	.9595	8.5200	.2575	1.3246	.8038
4.0400	.4473	1.2091	.9573	8.6000	.2575	1.3246	.8027
4.1200	.4418	1.2131	.9550	8.6800	.2575	1.3246	.8015
4.2000	.4363	1.2171	.9525	8.7600	.2577	1.3245	.8003
4.2800	.4307	1.2211	.9500	8.8400	.2579	1.3244	.7991
4.3600	.4250	1.2251	.9472	8.9200	.2583	1.3242	.7981
4.4400	.4192	1.2291	.9444	9.0000	.2588	1.3240	.7973
4.5200	.4135	1.2331	.9414	9.0800	.2594	1.3237	.7969
4.6000	.4076	1.2371	.9382	9.1600	.2602	1.3233	.7969
4.6800	.4018	1.2411	.9349	9.2400	.2613	1.3228	.7974
4.7600	.3959	1.2451	.9315	9.3200	.2625	1.3222	.7984
4.8400	.3900	1.2490	.9279	9.4000	.2640	1.3215	.8000
4.9200	.3841	1.2529	.9241	9.4800	.2656	1.3207	.8022
5.0000	.3782	1.2567	.9202	9.5600	.2676	1.3198	.8050
5.0800	.3723	1.2605	.9162	9.6400	.2697	1.3187	.8083
5.1600	.3665	1.2642	.9120	9.7200	.2721	1.3175	.8120
5.2400	.3607	1.2679	.9076	9.8000	.2748	1.3162	.8162
5.3200	.3549	1.2714	.9032	9.8800	.2777	1.3148	.8206
5.4000	.3493	1.2749	.8986	9.9600	.2808	1.3132	.8254
5.4800	.3437	1.2783	.8938	10.0200	.2841	1.3115	.8303
5.5600	.3382	1.2815	.8890				

***** PARTIAL PRESSURE DISTRIBUTION *****

UPPER SURFACE				LOWER SURFACE			
X	PO	X	PO	X	PO	X	PO
.063470	.619965	.412470	.490487	.018529	1.177701	.420090	.839263
.072470	.603469	.427470	.499146	.020009	1.168959	.435090	.832491
.081470	.585753	.442470	.508124	.021517	1.160234	.450090	.826486
.090470	.567763	.457470	.517454	.023051	1.151577	.465090	.821549
.099470	.550092	.472470	.527171	.024612	1.143043	.480090	.818078
.112470	.525961	.487470	.537318	.026199	1.134692	.495090	.816528
.127470	.500328	.517470	.547671	.027812	1.126590	.500090	.816503
.142470	.476999	.547470	.559811	.029449	1.118805	.515090	.813884
.157470	.456071	.577470	.573693	.031109	1.111406	.530090	.813869
.172470	.437612	.607470	.589277	.032792	1.104466	.545090	.819212
.187470	.421536	.637470	.596546	.034495	1.098058	.560090	.828932
.202470	.407762	.667470	.602562	.036219	1.092250	.575090	.842644
.217470	.396282	.697470	.608342	.037962	1.087110	.590090	.859821
.232470	.402678	.727470	.618833	.039721	1.082697	.605090	.879968
.247470	.409169	.757470	.62851	.041497	1.079062	.620090	.902554
.262470	.415782	.787470	.638176	.043287	1.076245	.635090	.926275
.277470	.422528	.817470	.644468	.045090	1.074271	.650090	.950898
.292470	.429411	.847470	1.011465	.045090	1.074271	.665090	.973677
.307470	.436435	.877470	1.028967	.060090	1.066244	.680090	.996525
.322470	.443606	.907470	1.046753	.075090	1.056097	.695090	1.018198
.337470	.450938	.937470	1.064631	.090090	1.044712	.710090	1.038355
.352470	.458437	.967470	1.082333	.105090	1.032385	.725090	1.056828
.367470	.466118	.997470	1.099616	.120090	1.020274	.740090	1.073587
.382470	.474002	1.007470	1.105244	.135090	1.008660	.755090	1.088273
.397470	.482115			.150090	.997403	.770090	1.101875
				.165090	.986527	.785090	1.111949
				.180090	.976032	.800090	1.120956
				.195090	.965859	.815090	1.128218
				.210090	.955970	.830090	1.133649
				.225090	.946373	.845090	1.137233
				.240090	.937082	.860090	1.138864
				.255090	.928106	.875090	1.138398
				.270090	.919421	.890090	1.135687
				.285090	.910968	.905090	1.130228
				.300090	.902668	.920090	1.121767
				.315090	.894449	.935090	1.109628
				.330090	.886292	.950090	1.092828
				.345090	.878183	.965090	1.070824
				.360090	.870108	.980090	1.038968
				.375090	.862097	.995090	.995450
				.390090	.854221	1.000090	.989826
				.405090	.846568		

APPENDIX F MIR SUBROUTINES LISTING

```

SUBROUTINE IOUPSTM
C
C THIS SUBROUTINE PRINTS THE INPUT PARAMETERS AND THE CALCULATED
C OUTPUT FOR SUBROUTINE UPSTRM
5
C
COMMON/UVVSAY/ NNINIT,NNSPR,NNQHN
1 ,YI(10,2),UI(10,2),VI(10,2),VUV(96)
COMMON/AINPUT/ ATN(24),NN(7) ,H(6)
COMMON/OUTCOM/
10
1 AX(160) ,ARMO(160),AY(10) ,ARM(10) ,DUM(140) ,II,II2
DIMENSION ISTAR(5),ITITLE(2)
DATA (ISTAR(I),I=1,5)/5*10H*****/
DATA (ITITLE(I),I=1,2)/10H UPSTREAM ,10H SOLUTION */
WRITE(6,200) (ISTAR(I),I=1,5),(ITITLE(I),I=1,2),(ISTAR(I),I=1,5)
15 ,NN(1),NN(2),ATN(1),(AIN(I),I=*,10),H(1),AIN(11),AIN(12)
IF(H(1).GT.0.005)GO TO 5
WRITE(6,340)
RETURN
5 CALL UPSTRM
20 IF(II.EQ.0) RETURN
IHALF = II/2
J = MOD(II,2)
IHALF1 = IHALF
IF(J.EQ.1) IHALF1 = IHALF+1
25 WRITE(6,400)
IF(II.EQ.1) GO TO 15
DO 10 I=1,IHALF
30 WRITE(6,300) AX(I),ARMO(I),AX(I+IHALF1),ARMO(I+IHALF1)
IF(J.NE.1) GO TO 15
15 WRITE(6,300) AX(IHALF1),ARMO(IHALF1)
15 IF(II2.EQ.0) WRITE(6,260)
IHALF = II2/2
J = MOD(II2,2)
IHALF1 = IHALF
35 IF(J.EQ.1) IHALF1=IHALF+1
WRITE(6,410)
IF(II2.EQ.1) GO TO 25
DO 20 I=1,IHALF
40 WRITE(6,300) AY(I),ARM(I),AY(I+IHALF1),ARM(I+IHALF1)
IF(J.NE.1) GO TO 25
25 WRITE(6,300) AY(IHALF1),ARM(IHALF1)
25 WRITE(6,220) AIN(20),AIN(21)
DO 30 I=1,NNINIT
45 WRITE(6,330) YI(I,1),UI(I,1),VI(I,1),YI(I,2),UI(I,2),VI(I,2)
RETURN
200 FORMAT(1H1,4(/)7X,12A10,
1 ///20X,4HNN =,I2,5H, NA =,I2//20X,9HDOVOO(I) =,
2 F10.4,9H, X00 = F8.4, 9H, RMT = F8.4,
3 9H, CDY = F8.4,7H, H = F8.4//20X,13HYINF(UPPER) =F8.4,
50 4 17H, YINF(LOWER) =F8.4)
250 FORMAT(/20X,39H*****INTEGRATION WAS NOT COMPLETED )
300 FORMAT(30X,2(10X,2F10.6))
320 FORMAT(/47X,4HDE =,F10.6,10X,5HYSO =,F10.6///52X,25H INITIAL VELO
1CITY PROFILE//30X,13HUPPER SURFACE,27X,13HLOWER SURFACE//17X,
55 22(19X,1HY,9X,1HU,9X,1HV))
330 FORMAT(20X,2(10X,3F10.6))
340 FORMAT(/20X,29H*****STEP SIZE TOO SMALL)
400 FORMAT(/27X,2(18X,1HX,9X,2HMO))
410 FORMAT(/26X,2(19X,1HY, 9X,1HM))
60 END

```

SUBROUTINE UPSTRM

THIS SUBROUTINE CALCULATES THE UPSTREAM FLOW CONDITIONS

```

C
C
5      COMMON      C      ,CK      ,RS      ,FM      ,ALPHA
COMMON/ACOM/X      ,XA      ,VN      ,VS      ,H      ,DY
1      ,YO      ,PO      ,RO      ,UO      ,VO      ,RMO      ,DUO
2      ,Y(2,10),P(2,10),R(2,10),U(2,10),V(2,10),RM(2,10),DU(2,10)
COMMON/BCOM/      XO      ,DVOC      ,L
10     COMMON/ECOM/UOSAV ,ROSAB ,XSAV ,DVOCF ,XSTG(11),YSTG(11)
1      ,DUM(22),XAF(50),YAF(50,2)
COMMON/AINPUT/      DVOCF ,DDUM(6),XOO      ,RMT      ,CDY
1      ,YU      ,YL      ,EDUM(7),DE      ,YSO      ,YS      ,FDUM(2)
2      ,NNI      ,NA      ,NDUM(5),HOWN      ,HDUM(5)
15     COMMON/OUTCOM/
1      AX(160) ,ARMO(160),AY(10) ,ARM(10) ,CDUM(140) ,II,NNO
COMMON/YUUSAV/      NNINIT,NNSPR,NNOWN
1      ,YI(10,2),UI(10,2),VI(10,2),YUV(96)
20     DIMENSION BX(6),RYO(6),RMO(6),Y1(2),Y2(2),A1U(2),A2U(2),A1V(2),
1      A2V(2)
C
C      INITIALIZE INPUT
G(AO, A1, A2, Z) = AO + A1*Z + A2*Z*Z
NTERM = 3
25     CSO = FM-.08
CS1 = CSO-.0.2
NN = NNI
DVOC = DVOCF
H = HOWN
30     Y(1,1) = YU
Y(2,1) = YL
II = 0
NNO = 0
RS = (1./(7.*CK) + 1.)**2.5
35     L = 4
XO = XOO
X = 0.0
C
C      INITIALIZE FLOW TO FREESTREAM CONDITIONS
40     DO 10 J=1,2
DO 5 N = 2, NN
Y(J,N) = Y(J,N-1)*0.5
P(J,N) = 1.
R(J,N) = 1.
45     U(J,N) = 1.
V(J,N) = 0.
PM(J,N) = FM
5     DU(J,N) = 0.0
RM(J,1) = FM
50     U(J,1) = 1.0
10    V(J,1) = 0.0
YO = 0.
RO = 1.
PO = 1.
55     UO = 1.
VS = 1.
VO = 0.
RMO = FM
C
60     II = II+1
AX(II) = X
ARMO(II) = RMO
C
DVA = 0.0
DO 26 K=1,100
DO 24 KK=1,NTERM
65
C
C      PERFORM A FLOW INTEGRATION STEP USING SUBROUTINE DIST
ISGN = 1

```

```

70      DO 22 J=1,2
          CALL OUNS(ISGN,J)
          DO 21 N = 3, NN
21      CALL INAS(ISGN,J,N,1)
22      ISGN = -1
75      IF(K.LE.3) GO TO 23
          CALL DIST(-1,1,NN,DYA,DVA,DVA)
23      CALL DIST(1,2,NN,DYO,DVS,DVO)
      C
          X = X + H
80      VS = VS + H*DVS
          VO = VO + H*(DVO - DVA)
          IF(VS.LT.VO)RETURN
          UO = SQRT(VS**2 - VO**2)
          YO = YO + H*DYO
85      RO = ((C - VS**2) / (C - 1.))**2.5
          PO = RO**1.4
          RMO = VS*SQRT(PO/(1.4*CK*PO))
      C
          IF(RMO.LE.RMT) GO TO 25
90      C
24      CONTINUE
      C  CALCULATE CERTAIN FACTORS USED IN DETERMINING RBUB
25      II = II+1
          AX(II) = X
95      ARMO(II) = RMO
      C
          IF (RMO .LE. RMT) GO TO 27
      C
26      CONTINUE
100     C
27      I = 0
      C
28      M = ABS((5.0-X)/H)
      C
105     C  DEPENDING ON DYO (THE SLOPE OF THE STAGNATION STREAMLINE) PERFORM
      C  A FLOW INTEGRATION STEP USING SUBROUTINE STMR OR LUMR
          IF (DYO .GE. CDY .OR. DY .GE. CDY) GO TO 35
          DO 34 K = 1, M
110      DO 31 KK=1,NTERM
      C
      C  PERFORM A FLOW INTEGRATION STEP USING LUMR
          ISGN = 1
          DO 30 J=1,2
115      CALL OUNS(ISGN,J)
          DO 29 N = 3, NN
29      CALL INAS(ISGN,J,N,1)
30      ISGN = -1
          CALL LUMR(-1,1,NN,DYA,DVA,DVA)
120      CALL LUMR(1,2,NN,DYO,DVS,DVO)
      C
          X = X + H
          VS = VS + H*DVS
          VO = VO + H*(DVO - DVA)
125      UO = SQRT(VS**2 - VO**2)
          YO = YO + H*DYO
          PO = ((C - VS**2) / (C - 1.))**2.5
          RO = RO**1.4
          RMO = VS*SQRT(RO/(1.4*CK*PO))
130      IF (RMO .LE. CSO) GO TO 42
          IF(DYO.GE.CDY) GO TO 32
135      31 CONTINUE
          32 II = II+1
          AX(II) = X
          ARMO(II) = RMO

```

```

140      IF (DVO .GE. CSO) GO TO 35

      34 CONTINUE

145      35 T = ATAN(VO/UO)
          DO 40 K = 1, M
          DO 38 KK=1,NTERM
C
C      PERFORM A FLOW INTEGRATION STEP USING STMH
150      ISGN = 1
          DO 37 J=1,2
          CALL OUNS(ISGN,J)
          DO 36 N = 3, NN
155      36 CALL INAS(ISGN,J,N,1)
          37 ISGN = -1
          CALL STMH(NN,T,DY,DVS)
C
C
C      IF RMO (MACH NUMBER AT THE STAGNATION STREAMLINE) IS CONSIDERABLY
160      C      LESSENEO, SAVE FLOW PARAMETERS AT THIS STEP
          IF(RMO.LE.CSO) GO TO 42

      38 CONTINUE
          II = II+1
165      AX(II) = X
          ARMO(II) = RMO
C
          IF (X.GE.7.00R.X.LT.0.00R.DVS.GE.0.0) RETURN
170      40 CONTINUE
          RETURN
C
      42 II = II+1
          AX(II) = X
          ARMO(II) = RMO
175      C
          IF(CS1.LT.CSO) GO TO 43
C
C      SAVE FLOW PROPERTIES AT THIS STEP
180      I = I + 1
          BX(I) = X
          BYO(I) = YO
          BMO(I) = RMO
          IF (I.EQ. 3) H = 0.002
          CSO = CSO - 0.05
185      IF(I-4) 29,60,60
C
C      CS1 IS LESS THAN CSO FOR THE FIRST PASS THROUGH THE LOOP, SO
C      STATEMENT 43 IS EXECUTED ONLY ONCE
190      43 DO 44 J=1,2
          Y1(J) = Y(J,NN)-YO
          Y2(J) = Y(J,NN-1)-YO
          CALL A1SUP(Y1(J),Y2(J),UO,U(J,NN),U(J,NN-1),A1U(J))
          CALL A2SUP(Y1(J),Y2(J),UO,U(J,NN),U(J,NN-1),A2U(J))
          CALL A1SUB(Y1(J),Y2(J),VO,V(J,NN),V(J,NN-1),A1V(J))
195      CALL A2SUB(Y1(J),Y2(J),VO,V(J,NN),V(J,NN-1),A2V(J))
          VO = -VO
          44 YO = -YO
C
C      ADD NA STRIPS TO THE FLOW INTEGRATION PROCESS AT THIS POINT
200      N1 = NN + 1
          NN = NN + NA
          DO 47 J=1,2
          DO 46 N = N1, NN
          Y(J,N) = (Y(J,N-1)-YO)/2.+YO
          U(J,N) = 0.5(UO,A1U(J),A2U(J),Y(J,N)-YO)
          V(J,N) = 0.5(VO,A1V(J),A2V(J),Y(J,N)-YO)
          VSC = U(J,N)*U(J,N)+V(J,N)*V(J,N)
          R(J,N) = ((C-VSC)/(C-1.))**2.5
          P(J,N) = R(J,N)**1.4
205

```



```

210      46 RM(J,N) = SQRT(VSO*R(J,N)/(1.4*CK*P(J,N)))
          V0 = -V0
          47 V0 = -V0
C
          H = H/5.
215      IF (H .LT. 0.005) H = 0.005
          CS0 = CS1
          GO TO28
C
220      C SAVE THE Y STATIONS AND THE MACH NUMBERS AT THE FINAL INTEGRATION
          C STEP
          60 DO I=1,J=1,NN
              AY(J) = Y(1,J)
          61 ARM(J) = RM(1,J)
              NNO = NN+1
225      AY(NNO) = Y0
          ARM(NNO) = RMO
              XO = X
C
          C EXTRAPOLATE RMO TO A VALUE OF ZERO USING THE OUTPUT OF THE FOUR
230      C PREVIOUSLY COMPUTED STEPS
              DO 63 K = 1, 200
                  X = X + 0.0005
                  CALL LGRNGN(BMO(1),BMO(2),BMO(3),BMO(4),
                      1BX(1),BX(2),BX(3),BX(4),X,RMO)
235      IF(RMO.LE.0.0) GO TO 64
          63 CONTINUE
C
          C DE IS THE CALCULATED VALUE FROM THE LAST INTEGRATION STEP TO THE
          C STAGNATION POINT
240      64 DE = X - XO
C
          C EXTRAPOLATE VSO FROM THE OUTPUT OF FOUR PREVIOUSLY COMPUTED STEPS
          C AND THE CALCULATED VALUE OF X
          CALL LGRNGN(BYO(1),BYO(2),BYO(3),BYO(4),
245      1BX(1),BX(2),BX(3),BX(4),X,VSO)
              UOSAV = U0
              ROSAV = R0
              XSAV = XO
              XSTG(1) = -DE
250      XSTAG = XO
              YSTG(1) = Y0
              DXSTAG = DE/10.
C
          C CALCULATE TEN COORDINATES ALONG THE STAGNATION STREAMLINE
255      DO 70 I=2,11
              XSTAG = XSTAG+DXSTAG
              CALL LGRNGN(BYO(1),BYO(2),BYO(3),BYO(4),BX(1),BX(2),BX(3),BX(4),
                  1XSTAG,YSTG(I))
          70 XSTG(I) = XSTG(I-1) +DXSTAG
C
260      C CALCULATE FIFTY POINTS ALONG THE FIRST 3 PER CENT OF THE AIRFOIL
          C NOSE
              DO 76 J=1,2
                  XAF(1) = 0.
265      YAF(1,J) = 0.
              DO 75 I=2,50
                  XAF(I) = XAF(I-1) +.0006
                  CALL ARFL(XAF(I),ADUM,YAF(I,J),BDUM,CDUM,J)
                  IF(J.EQ.2) YAF(I,2) = -YAF(I,2)
270      75 CONTINUE
          76 CONTINUE
C
          C SAVE OUTPUT FLOW PARAMETERS OF THIS SUBROUTINE
275      DO 80 J=1,2
              DO 78 I=1,NN
                  YI(I,J) = Y(J,I)
                  UI(I,J) = U(J,I)
                  78 VI(I,J) = V(J,I)
              NNINIT = NNO

```

```

280      VI(NNO,J) = VO
        UI(NNO,J) = UO
        VI(NNO,J) = VO
        VO = -VO
285      50 VO = -VO
        C
        RETURN
        END

```

```

      SUBROUTINE IOSTGNA
C
C   THIS SUBROUTINE PRINTS THE INPUT PARAMETERS AND THE CALCULATED
C   OUTPUT FOR SUBROUTINE STAGNA
5
C
      COMMON/ECOM/DUM(26),XSTAG(11),YSTAG(11),XARFL(50),YARFL(50,2)
      COMMON/AINPUT/   AIN(24),NM(7)   ,H(6)
      DIMENSION ISTAR(5),ITITLE(2)
      DATA (ISTAR(I),I=1,5)/5*10H*****/
10      DATA (ITITLE(I),I=1,2)/10HSTAGNATION,10H SOLUTION*/
      WRITE(6,200) (ISTAR(I),I=1,5),(ITITLE(I),I=1,2),(ISTAR(I),I=1,5)
      WRITE(6,210) AIN(2)
      WRITE(6,220) AIN(20),AIN(21)
      CALL STAGNA
15      WRITE(6,410)
      DO 10 I=1,25
10      WRITE(6,400) XARFL(I) ,YARFL(I,1),YARFL(I,2),XARFL(I+25),
         1 YARFL(I+25,1),YARFL(I+25,2)
      WRITE(6,430)
20      DO 20 I=1,5
20      WRITE(6,420) XSTAG(I),YSTAG(I),XSTAG(I+6),YSTAG(I+6)
      WRITE(6,420) XSTAG(5),YSTAG(5)
      WRITE(6,370) AIN(22),DUM(4)
      RETURN
25      200 FORMAT(1H1,4(/)7X,12A10)
      210 FORMAT(/20X,4HXS =,F10.6)
      220 FORMAT(/23X,34HFROM THE UPSTREAM SOLUTION,   DE =,F10.6,
         1 9H,   YSD =,F10.6)
      370 FORMAT(/ 4EX,4HYS =,F10.6,10X,9HDOVOO(F) =,F10.6)
30      400 FORMAT(13X,2(10X,3F12.6))
      410 FORMAT(/57X,19HHAIRFOIL COORDINATES//13X,2(18X,1HX,7X,8HY(UPPER),
         1 4X,8HY(LOWER)))
      420 FORMAT( 25X,2(10X,2F12.6))
35      430 FORMAT(/56X,21HSTAGNATION STREAMLINE//21X,2(21X,1HX,11X,1HY))
      END

```

```

      SUBROUTINE STAGNA
C
C THIS SUBROUTINE CALCULATES THE STAGNATION STREAMLINE GEOMETRY AND
C CERTAIN AIRFOIL COORDINATES
5
C
      COMMON      C      ,CK      ,RS      ,FM      ,ALPHA
      COMMON/BCOM/      XO      ,DV00      ,L
      COMMON/ECOM/UO      ,RO      ,X      ,DVOOF      ,XIN(11),YIN(11)
10      1      ,XOU(11),YOU(11),XAF(50),YAF(50,2)
      COMMON/AINPUT/      DV00I      ,XS      ,DUM(17),DE      ,YSO
      1      ,YS      ,DDUM(2),NDUM(7),HDUM(6)
C
C COMPUTE DVOOF FOR SELECTED STAGNATION POINT
      CALL ARFL(XS      ,ADUM,YS,DYS,DYS,2)
15      RA =1./ ABS(DDYS/(1.+DYS**2)**1.5)
      DVOOF = (2./DE+2./(DE+RA)-1./RA)*UO/
      1      (RS/RO+(X/(X+DE))**L*(1.+DE/RA))
C
C ADJUST COORDINATES FOR AIRFOIL NOSE AND STAGNATION STREAMLINE
20      GEOMETRY TO ONE CARTESIAN FRAME
      DO 20 I=1,11
      XOU(I) = XIN(I)+XS
20      YOU(I) = YIN(I)-YS-YSO
      RETURN
25      END

```

```

      SUBROUTINE IOLWRCT
C
C THIS SUBROUTINE PRINTS THE INPUT PARAMETERS AND THE CALCULATED
C OUTPUT FOR SUBROUTINE LWRCRIT
5
C
      COMMON/AINPUT/      AIN(24),NN1(7) ,HI(6)
      COMMON/YUVSAV/NN0,NN2,NN3,YUV(156)
      COMMON/OUTCOM/
1      AXB(160) ,ARMB(160),DUM(160) ,II      ,II2
10     DIMENSION ISTAR(5),ITITLE(4)
      DATA (ISTAR(I),I=1,5)/5*10H*****/
      DATA (ITITLE(I),I=1,4)/10HTEST OF CR,10HITICALITY*,10H  LOWER S,
1      10HURFACE /
      WRITE(6,200) (ISTAR(I),I=1,5),(ITITLE(I),I=1,2),(ISTAR(I),I=1,5),
15     1 (ITITLE(I),I=3,4)
      WRITE(6,220) NN0,AIN(20)
      WRITE(6,230) AIN(22),AIN(21)
      CALL LWRCRIT
      IF(II.EQ.0) RETURN
      IHALF = II/2
      J = MOD(II,2)
      IHALF1 = IHALF
      IF(J.EQ.1) IHALF1 = IHALF+1
      WRITE(6,400)
      IF(II.EQ.1) GO TO 45
      DO 40 I=1,IHALF
25     40 WRITE(6,300) AXB(I),ARMB(I),AXB(I+IHALF1),ARMB(I+IHALF1)
      IF(J.NE.1) GO TO 48
      45 WRITE(6,300) AXB(IHALF1),ARMB(IHALF1)
      48 RETURN
30     200 FORMAT(1H1,4(/),7X,12A10/57X,2A10/)
      220 FORMAT(/20X,34HFROM THE UPSTREAM SOLUTION,   NN =,I2,8H,   DE =,
1      F10.6)
      230 FORMAT(/20X,36HFROM THE STAGNATION SOLUTION,   YS =,F10.6,
35     1 9H,   YSO =,F10.6)
      300 FORMAT(30X,2(10X,2F10.4))
      400 FORMAT(/29X,2(18X,2HXB,8X,2HMB))
      END

```

```

      SUBROUTINE LWRCRIT
C
C   THIS SUBROUTINE CALCULATES MACH NUMBER FOR A SELECTED NUMBER OF
C   POINTS ON THE LOWER SURFACE
5
C   COMMON      C      ,CK      ,RS      ,FM      ,ALPHA
C   COMMON/ACOM/X      ,XA      ,VN      ,VS      ,H      ,DY
1   ,Y0      ,PO      ,RO      ,UN      ,VO      ,RMO      ,DUO
10  2   ,Y(2,10),P(2,10),R(2,10),U(2,10),V(2,10),RM(2,10),OU(2,10)
C   COMMON/AINPUT/      DV001      ,XAS      ,DUM(17),DE      ,YSO
1   ,YS      ,DDUM(2),NN1(7) ,HI(6)
C   COMMON/YUVSAV/      NNO,NNSPR,NNDWN
1   ,VI(10,2),UI(10,2),VI(10,2),YUV(96)
C   COMMON/OUTCOM/
15  1   AXB(150) ,ARMB(160),ADUM(160),II      ,I12
      D(AO, A1, A2, Z) = AO + A1*Z + A2*Z**2
C
C   INITIALIZE INPUT
C   CYD = DUM(4)
20  DO 10 N=2,NNO
      V(2,N) = VI(N,2)+YSO+YS
      U(2,N) = UI(N,2)
      V(2,N) = VI(N,2)
10  R(2,N) = ((C-U(2,N))*U(2,N)-V(2,N)*V(2,N))/(C-1.1)**2.5
25
C   CALCULATE FACTORS USED IN DETERMINING PRUB
C   Y1 = V(2,NNO-1)-YS-YSO-VI(NNO,2)
C   Y2 = V(2,NNO-2)-YS-YSO-VI(NNO,2)
C   CALL A1SUB(Y1,Y2,U(2,NNO),U(2,NNO-1),U(2,NNO-2),A1U)
30  CALL A2SUB(Y1,Y2,U(2,NNO),U(2,NNO-1),U(2,NNO-2),A2U)
C   CALL A1SUB(Y1,Y2,V(2,NNO),V(2,NNO-1),V(2,NNO-2),A1V)
C   CALL A2SUB(Y1,Y2,V(2,NNO),V(2,NNO-1),V(2,NNO-2),A2V)
C   B0 = U(2,NNO)*R(2,NNO)
C   B1 = U(2,NNO-1)*R(2,NNO-1)
35  B2 = U(2,NNO-2)*R(2,NNO-2)
C   CALL A1SUB(Y1,Y2,B0,B1,B2,A1C)
C   CALL A2SUB(Y1,Y2,B0,B1,B2,A2C)
C   CALL ARFL (XAS, XBS, YS, DYBS, DDYBS, 2)
C   DBS = (DE + XBS)*SQRT(1. + DYBS**2)/DYBS
40  YDS = (DE + XBS)/DYBS - YSO - VI(NNO,2)
C   UO = O(U(2,NNO),A1U,A2U,YDS)
C   VO = O(V(2,NNO),A1V,A2V,YDS)
C   VSQ = UO*UO + VO*VO
C   IF((C-VSQ).LE.0) RETURN
45  RO = ((C-VSQ)/(C-1.1))**2.5
C   VS = (UO + VO*DYBS)/SQRT(1. + DYBS**2)
C   CLA= DBS *RO*VS/2.
C   CLR = B0*YDS + A1C*YDS**2/2. + A2C*YDS**3/3.
C
50  DX = .003
40  XA = 0.
      II = 0
C
      DO 80 I = 1,20
55
C   DETERMINE RBUB FOR THIS XA
      XA = XA+DX
      CALL ARFL (XA, XB, YB, DYB, DDYB, 2)
      YO = (DE + XB)/DYB + YB
      YD = YO-YSO-YS-VI(NNO,2)
60
C   LET Y2 = V(2,NNO-4)
C   J=3
C   Y1 = V(2,NNO-J)-YS-YSO-VI(NNO,2)
C   Y2 = V(2,NNO-J-1)-YS-YSO-VI(NNO,2)
65  CALL A1SUB(Y1,Y2,U(2,NNO),U(2,NNO-J),U(2,NNO-J-1),A1U)
      CALL A2SUB(Y1,Y2,U(2,NNO),U(2,NNO-J),U(2,NNO-J-1),A2U)
      CALL A1SUB(Y1,Y2,V(2,NNO),V(2,NNO-J),V(2,NNO-J-1),A1V)
      CALL A2SUB(Y1,Y2,V(2,NNO),V(2,NNO-J),V(2,NNO-J-1),A2V)

```

```

70      B1 = U(2,NNO-J)*R(2,NNO-J)
      B2 = U(2,NNO-J-1)*R(2,NNO-J-1)
      CALL A1SUB(Y1,Y2,B0,B1,B2,A1C)
      CALL A2SUB(Y1,Y2,B0,B1,B2,A2C)
54     UO = D(U(2,NNO),A1U,A2U,YD)
75     VO = D(V(2,NNO),A1V,A2V,YD)
      RO = ((C-UO*UO-VO*VO)/(C-1.))**.5
      CT = 1./SQRT(1. + DVB**2)
      ST = DVB*CT
      DB = (DE + XB)/ST
      VS = UO*CT + VO*ST
80     CL = B0*YJ + A1C*YD**2/2. + A2C*YD**3/3. + CLA - CLB
      RBUB = 6.*CL/DB-VS*RO-4.*VS*RO*CYD

C      IF(RBUB.LT.0.0) GO TO 50
85     C      UBS = 0.1
      RBURP = RBUB**0.4*(C-1.)
C      USING NEWTON RAPHSONG METHOD ITERATE ON UB UNTIL RUP = RBURP
C      UB=0.1
90     DO 60 K=1,50
      RUP = C*UB**0.4-UB**2.4
      IF(ABS(RUP-RBURP).LT..000001) GO TO 70
      DRUPDU = 0.4*C/UB**0.6-2.4*UB**1.4
95     UB = UB+(RBURP-RUP)/DRUPDU
      IF(UB.LT.0.) UBS=UBS+.05
      IF(UB.LT.0.) UB=UBS
      IF(UBS.GT.1.) GO TO 50
60     CONTINUE
100    C      IF(I.GT.4.OR.DX.LT.0.0004) GO TO 90
      DX = .0003
      GO TO 40
C      70 RB = ((C - UB**2)/(C - 1.))**.5
105    PB = RB**1.4
C      CALCULATE RMB FOR THIS UB
C      RMB = UB/SQRT(1.4*CK*PB/PB)
110    C      II = II+1
      ARMB(II) = RMB
      AXB(II) = XB
C      50 CONTINUE
115    C      90 RETURN
      END

```

```

      SUBROUTINE IOLWRIN(ICRIT,L)
C
C THIS SUBROUTINE PRINTS THE INPUT PARAMETERS AND THE CALCULATED
C OUTPUT FROM SUBROUTINE LWRINIT
5
C
      COMMON/AINPUT/      AIN(24),NN1(7),HI(6)
      COMMON/YUVSAV/      NNINIT,NNSPR,NNDWN,YUV(156)
      COMMON/OUTCOM/
10      AXA(160),ARMO(160),ADU(160),II,II2
      COMMON/COMPRS/XX(160,2),PP(160,2),NP(2)
      COMMON/RBUBCM/RBUB,UBINIT,IRBUB
      DIMENSION ISTAR(5),ITITLE(4)
      DATA (ISTAR(I),I=1,5)/5*10H*****/
15      DATA (ITITLE(I),I=1,4)/10H* AIRFOIL,10HSOLUTION*,10H LOWER S,
      1 10HURFACE /
      J=2
      WRITE(6,200) (ISTAR(I),I=1,5),(ITITLE(I),I=1,2),(ISTAR(I),I=1,5),
      1 (ITITLE(I),I=3,4)
      WRITE(6,210) NN1(4),AIN(5),AIN(6),AIN(13),HI(3),HI(4)
20      M = (1.0-AIN(13))/HI(4)+(AIN(13)-AIN(5))/HI(3)
      NN1(7) = 0
      IF(M.LT.470.OR.ICRIT.EQ.2.OR.NNINIT.GE.NN1(4)) GO TO 4
      IF(ICRIT.NE.2) WRITE(6,360)
      IF(M.GT.470) WRITE(6,370)
25      IF(NNINIT.LT.NN1(4)) WRITE(6,380)
      RETURN
4      CALL LWRINIT(ICRIT)
      IF(IRBUB.EQ.0) WRITE(6,330) RBUB,UBINIT
      IF(IRBUB.EQ.1) WRITE(6,350) RBUB
30      IF(IRBUB.EQ.2) WRITE(6,340) RBUB
      IF(II.EQ.0) RETURN
      IHALF = II/2
      K = MOD(II,2)
      IHALF1 = IHALF
35      IF(K.EQ.1) IHALF1 = IHALF+1
      WRITE(6,400)
      IF(II.EQ.1) GO TO 15
      DO 10 I=1,IHALF
10      WRITE(6,300) AXA(I),ARMO(I),PP(I,J),ADU(I),AXA(I+IHALF1),
      1 ARMO(I+IHALF1),PP(I+IHALF1,J),ADU(I+IHALF1)
      IF(K.NE.1) GO TO 18
15      WRITE(6,300) AXA(IHALF1),ARMO(IHALF1),PP(IHALF1,J),ADU(IHALF1)
18      IF(NN1(7).EQ.0) GO TO 28
      CALL INVELOCL(J)
      CALL SUBCRT2(J)
45      NN17P1 = NN1(7)+1
      II3 = II-NN1(7)
      IF(II3.LE.0) GO TO 28
      IHALF = II3/2
50      IMIDL = IHALF+NN1(7)
      K = MOD(II3,2)
      IHALF1 = IHALF
      IF(K.EQ.1) IHALF1 = IHALF+1
      WRITE(6,400)
55      IF(II3.EQ.1) GO TO 25
      DO 20 I=NN17P1,IMIDL
20      WRITE(6,300) AXA(I),ARMO(I),PP(I,J),ADU(I),AXA(I+IHALF1),
      1 ARMO(I+IHALF1),PP(I+IHALF1,J),ADU(I+IHALF1)
      IF(K.NE.1) GO TO 28
60      25      WRITE(6,300) AXA(IMIDL+1),ARMO(IMIDL+1),PP(IMIDL+1,J),ADU(IMIDL+1)
      28      IF(II3.EQ.1) WRITE(6,260)
      RETURN
200      FORMAT(4(I/),7X,12A10/57X,2A13)
210      FORMAT(//20X,4HNB =,I2//20X,4HXA =,F8.4,9H, CYD =
65      1 F8.4, 8H, CX =F8.4, 9H, HSO =,F8.4, 8H, HO =F8.4)
260      FORMAT(/20X,39H*****INTEGRATION WAS NOT COMPLETED )
300      FORMAT(10X,2(10X,4F10.4))
310      FORMAT(20X,+A10,10X,4F10.4)
320      FORMAT(20X,+F10.4,10X,4A10)

```



```

70      330 FORMAT(/ 47X,6HRBUB =,F10.6,10X,4HUB =,F10.6)
      340 FORMAT(/ 39X,6HRBUB =,F10.6,40H*****FLOW CONDITIONS CANNOT BE MAT
          1CHED )
      350 FORMAT(/ 59X,6HRBUB =,F10.6)
75      360 FORMAT(/ 20X,62H*****SUPERCRITICAL FLOW IS NOT PERMITTED ON L
          1OWER SURFACE )
      370 FORMAT(/ 20X,29H*****STEP SIZE TOO SMALL )
      380 FORMAT(/ 20X,49H*****INSUFFICIENT NUMBER OF STRIPS AVAILABLE)
      400 FORMAT(/ 10X,2(17X,2HXB,8X,2HMB,8X,2HPB,7X,4HODUX))
          END

```

SUBROUTINE LWRINIT(ICRIT)

THIS SUBROUTINE CALCULATES THE INITIAL CONDITIONS USED IN THE LOWER SURFACE

C
C
C
C

```
COMMON C ,CK ,RS ,FM ,ALPHA
COMMON/ACOM/X ,XA ,VN ,VS ,H ,DY
1 ,YO ,PO ,RO ,UO ,VO ,RMO ,DUO
2 ,V(2,10),P(2,10),R(2,10),U(2,10),V(2,10),RM(2,10),DU(2,10)
COMMON/CCOM/XB ,YB ,DYB ,DDYB ,DUB ,PB
1 ,UB ,RMB ,OB ,HS ,CPA ,Q1 ,DQ1 ,RK
COMMON/DCOM/CS ,CZ ,DV1 ,Q1 ,DQ1 ,RK
1 ,V00 ,ISKIP
COMMON/AINPUT/ DV00I ,XAS ,BDUM(2),XAI ,CVD
1 ,CDUM(6),CXI ,DDUM(6),DE ,YSO ,YS ,EDUM(2)
2 ,NN1(3) ,NNLWR ,NN2(3) ,H1(2) ,HSO ,H2(3)
COMMON/YUVSAV/ NNO,NNSPR,NNDOWN
1 ,VI(10,2),UI(10,2),VI(10,2),YUV(96)
COMMON/COMNN/NN
COMMON/RBUBCM/RBUB ,UBINIT ,IRBUR
COMMON/OUTCOM/ADUM(480),II ,II2
D(A0, A1, A2, Z) = A0 + A1*Z + A2*Z*Z
```

C
C

INITIALIZE INPUT

```
DCX = .004
II2=0
II = 0
NN1(7) = 0
IF((XAI-CXI + 3.*DCX).GT.0.0) RETURN
NN =>NNLWR
XA = XAI
X = -DE
HS = HSO
DO 45 N = 1, NNO
V(2,N) = VI(N,2)+YSO+YS
U(2,N) = UI(N,2)
V(2,N) = VI(N,2)
YSO = U(2,N) *U(2,N) +V(2,N)*V(2,N)
R(2,N) = ((C-VSQ)/(C-1.))**2.5
P(2,N) = R(2,N)**1.4
45 RM(2,N) = SQRT(VSQ*R(2,N)/(1.4*CK*P(2,N)))
```

C
C

CALCULATE FACTORS USED IN DETERMINING RBUB

```
Y1 = V(2,NNO-1)-YS-YSO-YI(NNO,2)
Y2 = V(2,NNO-2)-YS-YSO-YI(NNO,2)
CALL A1SUB(Y1,Y2,U(2,NNO),U(2,NNO-1),U(2,NNO-2),A1U)
CALL A2SUB(Y1,Y2,U(2,NNO),U(2,NNO-1),U(2,NNO-2),A2U)
CALL A1SUB(Y1,Y2,V(2,NNO),V(2,NNO-1),V(2,NNO-2),A1V)
CALL A2SUB(Y1,Y2,V(2,NNO),V(2,NNO-1),V(2,NNO-2),A2V)
B0 = U(2,NNO)*R(2,NNO)
B1 = U(2,NNO-1)*R(2,NNO-1)
B2 = U(2,NNO-2)*R(2,NNO-2)
CALL A1SUB(Y1,Y2,B0,B1,B2,A1C)
CALL A2SUB(Y1,Y2,B0,B1,B2,A2C)
CALL ARFL (XAS, XBS, YS, DYBS, DDYBS,2)
DBS = (DE + XBS)*SQRT(1. + DDYBS**2)/DYBS
YDS = (DE+XBS)/DYBS-YSO-YI(NNO,2)
UO = D(U(2,NNO),A1U,A2U,YDS)
VO = D(V(2,NNO),A1V,A2V,YDS)
RO = ((C - UO**2 - VO**2)/(C - 1.))**2.5
VS = (UO +VO*DYBS)/SQRT(1. +DDYBS**2)
CLA= DBS *RO*VS/2.
CLR = 90*YDS + A1C*YDS**2/2. + A2C*YDS**3/3.
CALL ARFL (XA, XB, YB, DYB, DDYB,2)
YO = (DE + XB)/DYB + YB
YD = YO-YSO-YS-YI(NNO,2)
```

C
C

FIND A VALUE FOR Y2 SUCH THAT YO IS LESS THAN Y2
J=0

```

70      48 J = J+1
        Y1 = Y(2,NNO-J)-YS-YSO-YI(NNO,2)
        Y2 = Y(2,NNO-J-1)-YS-YSO-YI(NNO,2)
        IF(YD-Y2) 52,48,48

75      C
        C CALCULATE RBUB
        52 IF(J.EQ.1) GO TO 54
            CALL A1SUB(Y1,Y2,U(2,NNO),U(2,NNO-J),U(2,NNO-J-1),A1U)
            CALL A2SUB(Y1,Y2,U(2,NNO),U(2,NNO-J),U(2,NNO-J-1),A2U)
            CALL A1SUB(Y1,Y2,V(2,NNO),V(2,NNO-J),V(2,NNO-J-1),A1V)
80      CALL A2SUB(Y1,Y2,V(2,NNO),V(2,NNO-J),V(2,NNO-J-1),A2V)
            B1 = U(2,NNO-J)*R(2,NNO-J)
            B2 = U(2,NNO-J-1)*R(2,NNO-J-1)
            CALL A1SUB(Y1,Y2,B0,B1,B2,A1C)
            CALL A2SUB(Y1,Y2,B0,B1,B2,A2C)

85      C
        C CALCULATE RBUB
        54 UD = D(U(2,NNO),A1U,A2U,YD)
            VO = D(V(2,NNO),A1V,A2V,YD)
            RO = ((C - UD**2 - VO**2)/(C - 1.))**2.5
90      CT = 1./SQRT(1. + DY**2)
            ST = DYB*CT
            RAB = ABS(1./((CT**3*DDYB)))
            DB = (DE + XB)/ST
            VS = UD*CT + VO*CT
95      VN = -UD*ST + VO*CT
            CALL ARFL(XA+HS*CT,XBT, YBT, DYBT, DDYBT,2)
            DRT = DB + ((1. + DB/(RAB+DB))*VN/VS*HS
            H = XBT - DRT*DYBT/SQRT(1. + DYBT**2) - X
            CL = 90*YD + A1C*YD**2/2. + A2C*YD**3/3. + CLA - CLB
100     RBUB = 6.*CL/DB - VS*RO - 4.*VS*RO*CYD

        C
            IRBUB=0
            IF(RBUB) 55,55,58
105     55 IRBUB = 1
            RETURN
        58 UBS = 0.1
            RBUBP = RBUB**0.4*(C-1.)

        C
        C USING NEWTON RAPHSONG METHOD ITERATE ON UB UNTIL RUP = RBUBP
110     UB = 0.1
            DO 60 K=1,50
                RUP = C*UB**0.4-UB**2.4
                IF(ABS(RUP-RBUBP).LT..000001) GO TO 70
                DRUPDU = 0.4*C/UB**0.6-2.4*UB**1.4
115     UB = UB + (RBUBP-RUP)/DRUPDU
                IF(UB.LT.0) UBS = UBS+.05
                IF(UB.LT.0.) UB = UBS
                IF(UBS.GT.1.) RETURN
60     CONTINUE

120     C
            IRRUR = 2
65     RETURN

        C
70     RB = ((C-UB*UB)/(C-1.))**2.5
125     UBINIT = UR
            PB = R9**1.4

        C
        C CALCULATE RMB FOR THIS UB
            RMB = UB/SQRT(1.4*CK*PB/RB)
130     IF (Y0/Y(2,NN).GE.0.3) NN = NN - 1
            PO = R0**1.4

        C
            RMO = SQRT((UD**2 + VO**2)/(1.4*CK*PO/RO))

        C
135     CALL SUBCOT(1(2))
            RETURN
            END

```

```

      SUBROUTINE SUBCRT(J)
C
C   THIS SUBROUTINE CALCULATES SUBCRITICAL FLOW FOR THE INITIAL PORTION
C   OF THE AIRFOIL SURFACE
9
C
      COMMON      C      ,CK      ,RS      ,FM      ,ALPHA
      COMMON/ACOM/X      ,XA      ,VN      ,VS      ,H      ,DY
1      ,VO      ,PO      ,RO      ,UO      ,VO      ,RMO      ,DUO
2      ,Y(2,10),P(2,10),R(2,10),U(2,10),V(2,10),RM(2,10),DU(2,10)
10     COMMON/CCOM/XB      ,YB      ,DYB      ,DDYB      ,DUB      ,PB
1      ,UB      ,RMB      ,NB      ,HS      ,CRA
      COMMON/DCOM/CS      ,CZ      ,DV1      ,Q1      ,DQ1      ,RK
1      ,VOO      ,ISKIP
      COMMON/AINPUT/      DUM(12),CXI      ,RUM(11),NN1(7) ,H1(6)
15     COMMON/OUTCOM/
1      XB0(160) ,RMB0(160),DUB0(160),II      ,II2
      COMMON/COMNN/NN
      COMMON/COMPRS/XX(160,2),PP(160,2),NP(2)
      DIMENSION BX(4),BU(4,10),BV(4,10),BY(4,10)
20
C
C   INITIALIZE INPUT
      DCX = 0.004
      CX = CXI -3.*DCX
      CRA = 1.0
25     II2=0
      I=0
      N1 = NN - 1
100 DO 106 K=1,30
C
C   PERFORM FLOW INTEGRATION STEP
30     CALL OUNS(1,J)
      DO 104 N = 3, N1
104    CALL INAS(1,J,N,1)
      CALL INBO(NN,J)
35
C
      II = II+1
      XB0(II) = XB
      RMB0(II) = RMB
      XX(II,J) = XB
40     PP(II,J) = PB
      DUB0(II) = DUB
C
      IF (RMO .GE. 1.0 .OR. DUB .LE. 0.0) RETURN
C
45     IF (XB .GE. CX ) GO TO 120
C
106 CONTINUE
C
      RETURN
50
C
C   SAVE FLOW PROPERTIES AT THIS STATION
120 I=I+1
      BX(I) = X
      DO 124 N = 2, NN
55     BU(I,N) = U(J,N)
      BV(I,N) = V(J,N)
124    BY(I,N) = Y(J,N)
C
      IF (I - 4) 126, 200, 200
60     126 CX = CX + DCX
      GO TO 100
C
C   CALCULATE FLOW PROPERTIES AT XB AS INPUT TO NEXT STEP
65     200 UO = UR/SQRT(1.+DYB*DYB)
      VO = UO*DYB
      VSQ = UR*UB
      RO = ((C-VSQ)/(C-1.))**2.5
      PO = RO**1.4
      RMO = SQRT(VSQ*RO/(1.4*CK*PO))

```

```

70      DO 220 N = 2, NN
          CALL LGRNGN(BY(1,N),BY(2,N),BY(3,N),BY(4,N),
1BX(1),BX(2),BX(3),BX(4),XB,Y(J,N))
          CALL LGRNGN(BU(1,N),BU(2,N),BU(3,N),BU(4,N),
1BX(1),BX(2),BX(3),BX(4),XB,U(J,N))
75      220 CALL LGRNGN(BV(1,N),BV(2,N),BV(3,N),BV(4,N),
1BX(1),BX(2),BX(3),BX(4),XB,V(J,N))
      C
          II = II+1
          XX(II,J) = XB
80      PP(II,J) = PB
          XBO(II) = XB
          RMBO(II) = RM3
          DUBO(II) = DUB
          NN1(7) = II
85      C
          RETURN
          END

```

```

      SUBROUTINE SUBCRT2(J)
C
C   THIS SUBROUTINE CALCULATES SUBCRITICAL FLOW FOR THE BULK OF THE
C   INTEGRATION PROCESS
5
C
      COMMON      C      ,CK      ,RS      ,FM      ,ALPHA
      COMMON/ACOM/X      ,XA      ,VN      ,VS      ,H      ,DY
1      ,VO      ,PO      ,RO      ,UO      ,VO      ,RMO      ,DOO
2      ,Y(2,10),P(2,10),R(2,10),U(2,10),V(2,10),RM(2,10),DU(2,10)
10     COMMON/DCOM/CS      ,CZ      ,DV1      ,Q1      ,DQ1      ,RK
1      ,VOO      ,ISKIP
      COMMON/AINPUT/      DUM(24),NN1(7) ,H1(3) ,HO      ,H2(2)
      COMMON/OUTCOM/
15     1      AXA(160) ,ARMO(160),ADU(160) ,II      ,II2
      COMMON/COMPRS/XX(160,2),PP(160,2),NP(2)
      COMMON/YUUSAV/      NNINIT, NNSPR,NNDWN
1      ,YUV(90),YU(10),UU(10),VU(10),YL(10),UL(10),VL(10)
2      ,YOU,YOL,UOU,UOL,VOU,VOL
20     COMMON/COMMON/NN
      D(AO, A1, A2, Z) = AO + A1*Z + A2*Z*Z
C
C   INITIALIZE INPUT
      NTERM = 3
      CX = 0.5
25     ISKIP = 2
      CS = 1.0
      CZ = C
      H = HO
      CALL ARFL (XA, X, YO, DY,DOY,2)
30     N=NN
      VSO = U(J,NN)*U(J,NN)+V(J,NN)*V(J,NN)
      R(J,NN) = ((C-VSO)/(C-1.))**2.5
      P(J,NN) = R(J,NN)**1.4
      RM(J,NN) = SQRT(VSO*R(J,NN)/(1.4*CK*P(J,NN)))
35
C
250  M = ABS((1.-X)/H)
      DO 268 K = 1, M
      DO 266 KK=1,NTERM
C
C   PERFORM FLOW INTEGRATION STEP
40     CALL OUNS(1,J)
      X = X*H
      DO 265 N=3,NN
265  CALL INAS(1,J,N,NN)
45
C
      IF (X.GE.CX.OR.X.LT.0.0.OR.RMO.LE.0.1.OR.RMO.GE.1.0.OR.
1      ABS(ADU(II)).GT.2.0) GO TO 267
C
266  CONTINUE
50
C
267  II = II+1
      AXA(II) = XA
      ARMO(II) = RMO
      ADU(II) = DU(J,NN)
55     XX(II,J) = X
      PP(II,J) = PO
C
      IF (X .GE. CX ) GO TO 270
C
60     IF (X .LT. 0. .OR. RMO .LE. 0.4.OR.RMO.GE.1.0) RETURN
C
      IF (ABS(ADU(II)).GT.2.0) NN = NN-1
268  CONTINUE
270  CONTINUE
65     IF (CX.GT.9.999) GO TO 380
C
C   ADD ANOTHER STRIP TO THE INTEGRATION
      Y1 = Y(J,NN-1)-Y(J,NN)
      Y2 = Y(J,NN-2)-Y(J,NN)

```

```

70      CALL A1SUB(Y1,Y2,U(J,NN),U(J,NN-1),U(J,NN-2),A1U)
      CALL A2SUB(Y1,Y2,U(J,NN),U(J,NN-1),U(J,NN-2),A2U)
      CALL A1SUB(Y1,Y2,V(J,NN),V(J,NN-1),V(J,NN-2),A1V)
      CALL A2SUB(Y1,Y2,V(J,NN),V(J,NN-1),V(J,NN-2),A2V)
      NN = NN+1
75      Y(J,NN) = Y(J,NN-1)/2.
      U(J,NN) = D(U(J,NN-1),A1U,A2U,Y(J,NN)-Y(J,NN-1))
      V(J,NN) = D(V(J,NN-1),A1V,A2V,Y(J,NN)-Y(J,NN-1))
      VSQ = U(J,NN)*U(J,NN)+V(J,NN)*V(J,NN)
      R(J,NN) = ((C-VSQ)/(C-1.))**2.5
80      P(J,NN) = R(J,NN)**1.4
      RH(J,NN) = SQRT(VSQ*R(J,NN)/(1.4*CK*P(J,NN)))
      CX = 1.0
      GO TO 250

C
C  SAVE FINAL FLOW PROPERTIES OF THIS SUBROUTINE AS INPUT TO NEXT STEP
85      380 II2=1
      NP(J) = II
      IF(J.EQ.2) GO TO 410
      DO 400 N=1,NN
90      YU(N) = Y(J,N)
      UU(N) = U(J,N)
      400 VU(N) = V(J,N)
      YUO = YO
      UO = UO
      VUO = VO
95      RETURN
      410 DO 420 N=1,NN
      YL(N) = Y(J,N)
      UL(N) = U(J,N)
100      420 VL(N) = V(J,N)
      YOL = YO
      UOL = UO
      VOL = VO
      RETURN
105      END

```

```

      SUBROUTINE IOUPRCY
C
C THIS SUBROUTINE PRINTS THE INPUT PARAMETERS AND THE CALCULATED
C OUPUT FOR SUBROUTINE UPRCRIT
5
C
      COMMON/AINPUT/      AIN(24),NN1(7),HI(6)
      COMMON/YUUSAW/      NNINIT,NNSPR,NNOWN,YUV(156)
      COMMON/OUTCOM/
10
      1  AXB(160),ARMB(160),DUM(160),II,II2
      DIMENSION ISTAR(5),ITITLE(4)
      DATA (ISTAR(I),I=1,5)/5*10H*****/
      DATA (ITITLE(I),I=1,4)/10HTEST OF CR,10HITICALITY*,10H  UPPER S,
15
      1  10HURFACE /
      WRITE(6,200) (ISTAR(I),I=1,5),(ITITLE(I),I=1,2),(ISTAR(I),I=1,5),
      1  (ITITLE(I),I=3,4)
      WRITE(6,220) NNINIT,AIN(20)
      WRITE(6,230) AIN(22),AIN(21)
      CALL UPRCRIT
      IF(II.EQ.0) RETURN
20
      IHALF = II/2
      J = MOD(II,2)
      IHALF1 = IHALF
      IF(J.EQ.1) IHALF1=IHALF+1
      WRITE(6,400)
25
      IF(II.EQ.1) GO TO 25
      DO 28 I=1,IHALF
      20 WRITE(6,300) AXB(I),ARMB(I),AXB(I+IHALF1),ARMB(I+IHALF1)
      IF(J.NE.1) GO TO 28
      25 WRITE(6,300) AXB(IHALF1),ARMB(IHALF1)
30
      28 RETURN
      200 FORMAT(1H1,4(/),7X,12A10/57X,2A10/)
      220 FORMAT(/20X,34HFROM THE UPSTREAM SOLUTION,  NN =,I2,8H,  DE =,
      1  F10.6)
      230 FORMAT(/20X,36HFROM THE STAGNATION SOLUTION,  YS =,F10.6,
35
      1  9H,  YSO = ,F10.6)
      300 FORMAT(30X,2(10X,2F10.4))
      400 FORMAT(/29X,2(18X,2HXB,8X,2HMB))
      END

```



```

      SUBROUTINE UPRCRIT
C
C THIS SUBROUTINE CALCULATES MACH NUMBER FOR A SELECTED NUMBER OF
C POINTS ON THE INITIAL PORTION OF THE UPPER SURFACE
5
C      COMMON      C      ,CK      ,RS      ,FM      ,ALPHA
      COMMON/ACOM/X      ,XA      ,VN      ,VS      ,H      ,DY
1      ,Y0      ,P0      ,R0      ,U0      ,V0      ,RMO      ,DUO
10     ,V(2,10),P(2,10),R(2,10),U(2,10),V(2,10),RM(2,10),DU(2,10)
      COMMON/YUVSAV/      NNO,NNSPR,NNDWN
1      ,YI(10,2),UI(10,2),VI(10,2),YUV(96)
      COMMON/AINPUT/DUM(19),DE      ,YSO      ,YS      ,DDUM(2),NDUM(7)
1      ,HDUM(6)
      COMMON/OUTCOM/
15     1      AXB(160) ,ARMB(160),ADUM(160),II      ,II2
      D(A0, A1, A2, Z) = A0 + A1*Z + A2*Z*7
C
C INITIALIZE INPUT
      ND = NNO - 2
20     DO 50 N = ND, NNO
      Y(1,N) = YI(N,1) - YSO - YS
      U(1,N) = UI(N,1)
      V(1,N) = VI(N,1)
25     50 R(1,N) = ((C-U(1,N)*U(1,N)-V(1,N)*V(1,N))/(C-1.))**.5
C
      Y1 = Y(1,NNO-1) + YS + YSO - YI(NNO,1)
      Y2 = Y(1,NNO-2) + YS + YSO - YI(NNO,1)
      CALL A1SUB(Y1,Y2,U(1,NNO),U(1,NNO-1),U(1,NNO-2),A1U)
      CALL A2SUB(Y1,Y2,U(1,NNO),U(1,NNO-1),U(1,NNO-2),A2U)
30     CALL A1SUB(Y1,Y2,V(1,NNO),V(1,NNO-1),V(1,NNO-2),A1V)
      CALL A2SUB(Y1,Y2,V(1,NNO),V(1,NNO-1),V(1,NNO-2),A2V)
      B0 = U(1,NNO)*R(1,NNO)
      B1 = U(1,NNO-1)*R(1,NNO-1)
      B2 = U(1,NNO-2)*R(1,NNO-2)
35     CALL A1SUB(Y1,Y2,B0,B1,B2,A1C)
      CALL A2SUB(Y1,Y2,B0,B1,B2,A2C)
C
      DX = .003
C
40     56 XA = 0.
      II = 0
C
      DO 100 I=1,20
      XA = XA+DX
45
C DETERMINE RBUB FOR THIS XA
      CALL ARFL (XA, XB, YB, DYB, DDYB,1)
      Y0 = (DE + XB)/DYB + YB
      YD = Y0 + YSO + YS - YI(NNO,1)
50     U0 = D(U(1,NNO),A1U,A2U,YD)
      V0 = D(V(1,NNO),A1V,A2V,YD)
      VSO = U0*U0 + V0*V0
      IF((C-VSO).GT.0.) GO TO 57
      IF(I.GT.3.OR.DX.LT.0.0006) RETURN
55     DX = .0005
      GO TO 56
57     RO = ((C-VSO)/(C-1.))**.5
      CT = 1./SQRT(1. + DYB**2)
      ST = DYB*CT
      DP = (DE + XB)/ST
      VS = U0*CT + V0*ST
      CL = B0*YD + A1C*YD**2/2. + A2C*YD**3/3.
      RBUB = 2.*CL/DP - VS*RO
C
65     IREUB = 0
      IF(RBUB.LT.0.) GO TO 100
59     URS = 0.1
      PRUPP = RBUB**.4*(C-1.)
C

```

```

70      C   USING NEWTON-RAPHSONG METHOD, ITERATE ON UB UNTIL RBUBP = RUP
        UB=0.1
        DO 60 K=1,50
          RUP = C*UB**0.4-UB**2.4
          IF(ABS(RUP-RBUBP).LT..000001) GO TO 70
75      DRUPDU = 0.4*C/UB**0.6-2.4*UB**1.4
          UB = UB+(RBUBP-RUP)/DRUPDU
          IF(UB.LT.0.) UBS=UBS+.05
          IF(UB.LT.0.) UB=UBS
          IF(UBS.GT.1.) GO TO 100
80      60 CONTINUE
        C
          IF(I.GT.3.OR.DX.LT.0.0006) RETURN
          DX = .0005
          GO TO 56
85      70 RB = ((C-UB**2)/(C-1.))**2.5
          PB = RB**1.4
        C
        C   CALCULATE RMB FOR THIS UB
        RMB = UB/SQRT(1.4*CK*PB/RB)
90      C
          II = II+1
          ARMB(II) = RMB
          AXB(II) = XB
        C
95      100 CONTINUE
        C
          RETURN
          END

```

SUBROUTINE IOUPRIN(ICRIT)

THIS SUBROUTINE PRINTS THE INPUT PARAMETERS AND THE CALCULATED
OUTPUT FOR SUBROUTINE UPRINIT

```

C
C
C
5      COMMON/AINPUT/      AIN(24),NN1(7),HI(6)
      COMMON/YUVSAV/      NNINIT,NNSPR,NNOWN,YUV(155)
      COMMON/OUTCOM/
10     1 XBO(160),RMBO(160),DUBO(160),II      ,II2
      COMMON/COMPRS/XX(160,2),PP(160,2),NP(2)
      COMMON/RBUBCN/RBUB      ,UBINIT      ,IRBUB
      DIMENSION ISTAR(5),ITITLE(4)
      DATA (ISTAR(I),I=1,5)/5*10H*****/
15     DATA (ITITLE(I),I=1,4)/10H* INITIAL ,10HSOLUTION *,10H  UPPER S,
      1 10HURFACE      /
      J=1
      WRITE(6,200) (ISTAR(I),I=1,5),(ITITLE(I),I=1,2),(ISTAR(I),I=1,5),
20     1 (ITITLE(I), I=3,4)
      WRITE(6,210) NN1(3),AIN(3),AIN(4),AIN(14),HI(2)
      NN1(7) = 0
      IF(HI(2).GT.0.0001.OR.NNINIT.GE.NN1(3)) GO TO 4
      IF(HI(2).LT.0.0001) WRITE(6,360)
      IF(NNINIT.LT.NN1(3)) WRITE(6,370)
      RETURN
25     4 CALL UPRINIT(ICRIT)
      IF(IRBUB.EQ.0) WRITE(6,330) RBUB,UBINIT
      IF(IRBUB.EQ.1) WRITE(6,350) RBUB
      IF(IRBUB.EQ.2) WRITE(6,340) RBUB
      IF(II.EQ.0) RETURN
30     IF(II2.EQ.0) NN1(7) = II+1
      IF(II2.EQ.0) II=II+1
      IICX = NN1(7)
      IHALF = II/2
      K = MOD(II,2)
35     IHALF1 = IHALF
      IF(K.EQ.1) IHALF1 = IHALF+1
      WRITE(6,400)
      IF(II.EQ.1) GO TO 15
      DO 10 I=1,IHALF
40     IF(I.NE.IICX.AND.(I+IHALF1).NE.IICX) GO TO 5
      IF(I.EQ.IICX) WRITE(6,310) (ISTAR(L),L=1,4),XBO(I+IHALF1),
      1 RMBO(I+IHALF1),PP(I+IHALF1,J),DUBO(I+IHALF1)
      IF((I+IHALF1).EQ.IICX) WRITE(6,320) XBO(I),RMBO(I),PP(I,J),DUBO(I)
45     1 ,(ISTAR(L),L=1,4)
      GO TO 10
      5 WRITE(6,300) XBO(I),RMBO(I),PP(I,J),DUBO(I),XBO(I+IHALF1),
      1 RMBO(I+IHALF1),PP(I+IHALF1,J),DUBO(I+IHALF1)
10     CONTINUE
      IF(K.NE.1) GO TO 18
      IF(IICX.EQ.IHALF1) WRITE(6,310) (ISTAR(L),L=1,4)
      IF(IICX.EQ.IHALF1) GO TO 18
50     15 WRITE(6,300) XBO(IHALF1),RMBO(IHALF1),PP(IHALF1,J),DUBO(IHALF1)
      19 IF(II2.LE.0) WRITE(6,260)
      RETURN
55     200 FORMAT(4(/),      7X,12A10/57X,2A10)
      210 FORMAT(      //20X,4HNN =I2,9H,      XAO =,F10.6,3H,      CYD =F12.8,
      1 9H,      RMC =,F10.6,8H,      HS =,F10.6)
      250 FORMAT(/20X,39H*****INTEGRATION WAS NOT COMPLETED )
      300 FORMAT(10X,2(10X,4F10.4))
60     310 FORMAT(20X,4A10,10X,4F10.4)
      320 FORMAT(20X,4F10.4,10X,4A10)
      330 FORMAT( /47X,6HREUB =,F10.6,10X,4HUB =,F10.6)
      340 FORMAT(/ 39X,6HREUB =,F10.6,40H*****FLOW CONDITIONS CANNOT BE MAT
      1CHED      )
65     350 FORMAT(/ 59X,6HREUB =,F10.6)
      360 FORMAT(/20X,29H*****STEP SIZE TOO SMALL)
      370 FORMAT(/20X,49H*****INSUFFICIENT NUMBER OF STRIPS AVAILABLE)
      400 FORMAT(/10X,2(17X,2HX3,3X,2HMB,8X,2HPB,7X,4HDDX))
      END

```

```

SUBROUTINE UPRINIT(ICRIT)
C
C THIS SUBROUTINE CALCULATES THE INITIAL CONDITIONS ON THE UPPER
C SURFACE
5
COMMON C ,CK ,RS ,FH ,ALPHA
COMMON/ACOM/X ,XA ,VN ,VS ,H ,DY
1 ,VO ,PO ,RO ,UO ,VO ,RMO ,DUO
2 ,V(2,10),P(2,10),R(2,10),U(2,10),V(2,10),RM(2,10),DU(2,10)
10 COMMON/CCOM/XR ,YB ,OYB ,DOYB ,DU9 ,PB
1 ,UB ,RMB ,DB ,HS ,CRA
COMMON/AINPUT/ ADUM(2),XAO ,CYD ,DUM(15),DE
1 ,YSO ,VS ,DDUM(2),NDUM(2),NNUPR ,MDUM(4),H1
2 ,HSI ,H2(4)
15 COMMON/YUVSAV/ NNO,NNSPR,NNDWN
1 ,VI(10,2),UI(10,2),VI(10,2),YUV(96)
COMMON/COMNN/NN
COMMON/OUTCOM/EDUM(450),II ,II2
20 COMMON/RBUBCM/RBUB ,UBINIT ,IR9UB
D(AC, A1, A2, Z) = AO + A1*Z + A2*Z*Z
C
C INITIALIZE INPUT
II2=0
II = 0
25 HS = HSI
NN = NNUPR
X = -DE
XA = XAO
DO 52 N = 1, NNO
30 Y(1,N) = YI(N,1) -YSO-YS
U(1,N) = UI(N,1)
V(1,N) = VI(N,1)
YSO = U(1,N)*U(1,N)+V(1,N)*V(1,N)
R(1,N) = ((C-VS2)/(C-1.))**2.5
35 P(1,N) = R(1,N)**1.4
52 RM(1,N) = SQRT(VSO*R(1,N)/(1.4*CK*P(1,N)))
C
C CALCULATE RBUB
Y1 = Y(1,NNO-1)+YS+YSO-YI(NNO,1)
40 Y2 = Y(1,NNO-2)+YS+YSO-YI(NNO,1)
CALL A1SUB(Y1,Y2,U(1,NNO),U(1,NNO-1),U(1,NNO-2),A1U)
CALL A2SUB(Y1,Y2,U(1,NNO),U(1,NNO-1),U(1,NNO-2),A2U)
CALL A1SUB(Y1,Y2,V(1,NNO),V(1,NNO-1),V(1,NNO-2),A1V)
45 CALL A2SUB(Y1,Y2,V(1,NNO),V(1,NNO-1),V(1,NNO-2),A2V)
RO = U(1,NNO)*R(1,NNO)
R1 = U(1,NNO-1)*R(1,NNO-1)
R2 = U(1,NNO-2)*R(1,NNO-2)
CALL A1SUB(Y1,Y2,R0,R1,R2,A1C)
CALL A2SUB(Y1,Y2,R0,R1,R2,A2C)
50 CALL ARFL(XA, XB, Y9, OY9, DOY9,1)
YO = (DE + X9)/OY9 + Y9
YD = YO+YSO+VS-YI(NNO,1)
UO = D(U(1,NNO),A1U,A2U,YD)
VO = D(V(1,NNO),A1V,A2V,YD)
55 RO = ((C - UO**2 - VO**2)/(C - 1.))**2.5
PO = RO**1.4
RMO = SQRT((UO**2 + VO**2)/(1.4*CK*PO/RO))
CT = 1./SQRT(1. + OYB**2)
ST = OYB*CT
60 RAP = ABS(1./((CT**3*DOYB))
DB = (DE + X9)/ST
VS = UO*CT + VO*ST
VN = -UO*ST + VO*CT
CL = B0*YD + A1C*YD**2/2. + A2C*YD**3/3.
65 RBUP = 6.*CL/DB - VS*RO - 4.*VS*RO*CYD
C
II = 0
IR9UB=0
IF(R9UB) 55,55,58

```

```

70      C      55 IRBUB = 1
          RETURN
      C
      58 URS = 0.1
75      R9UBP = R9UB**0.4*(C-1.)
      C
      C      USING NEWTON-RAPHSONG METHOD, ITERATE ON UP UNTIL R9UBP = RUP
      C      UB = 0.1
          DO 60 K=1,50
80          RUP = C*UB**0.4-UR**2.4
          IF(ABS(RUP-R9UBP).LT..000001) GO TO 70
          DRUPDU = 0.4*C/UR**0.6-2.4*UB**1.4
          UB = UB + (R9UBP-RUP)/DRUPDU
          IF(UB.LT.0.) UBS = UBS+.05
85          IF(UR.LT.0.) UB = UBS
          IF(UBS.GT.1.) RETURN
          60 CONTINUE
      C
          IRBUB = 2
90      65 RETURN
      C
          70 IF(C-UB*UR) 65,65,71
          71 RB = ((C-UB*UR)/(C-1.))**2.5
          UBINIT = UR
95          RB = RB**1.4
      C
      C      CALCULATE RMB FOR THIS UB
          RMB = UB/SQRT(1.4*CK**RB/RB)
      C
100      CALL ARFL(XA+HS*CT, XBT, YBT, DYBT, DDYBT,1)
          DBT = DB + (1. + DB/(RAB*DB))*VN/VS*HC
          H = XBT - DBT*DYBT/SQRT(1. + DYBT**2) - X
      C
105      IF(ICRIT.EQ.1) CALL SPRORT1(1)
          IF(ICRIT.EQ.2) CALL SUBORT1(1)
      C
          RETURN
          END

```

```

      SUBROUTINE SPRCRT1(J)
C
C   THIS SUBROUTINE CALCULATES THE INITIAL FLOW CONDITIONS ON THE UPPER
C   SURFACE
5
C
      COMMON      C      ,CK      ,RS      ,FM      ,ALPHA
      COMMON/ACOM/X      ,XA      ,VN      ,VS      ,H      ,DY
1      ,YO      ,PO      ,RO      ,UO      ,VO      ,RMO      ,DUO
10     2      ,Y(2,10),P(2,10),R(2,10),U(2,10),V(2,10),RM(2,10),DU(2,10)
      COMMON/CCOM/XB      ,YB      ,OYB      ,DDYB      ,DUB      ,PB
1      ,UB      ,RMB      ,OB      ,HS      ,CRA
      COMMON/DCOM/CS,CZ,AJDUM(5),ISKIP
      COMMON/AINPUT/      DUM(13),RMC      ,BDUM(4),XASPR      ,CDUM(5)
1      ,NN1(7),H1(6)
15     COMMON/YUVSAV/      NNINIT,NNSPR,NNQWN
1      ,YUV1(60),YSPR(10),USPR(10),VSPR(10),YUV2(66)
      COMMON/OUTCOM/
1      ,XB0(160),RMB0(160),DUB0(160),II      ,II2
      COMMON/COMPRS/XX(160,2),PP(160,2),NP(2)
20     COMMON/COMNN/NN
      DIMENSION BVS(6),BYN(6),BDR(6)
      DIMENSION BX(4),BXA(4),BUB(4),BMB(4), BU(4,10),BY(4,10),BY(4,10)
C
C   INITIALIZE INPUT
25     II2 = 0
      CRA = 0.
      CSO = 0.9
      DCSO = .02
      DCS1 = .03
30     NTERM = 3
      I = 0
      N1 = NN - 1
      DO 110 K = 1, 100
      DO 108 KK=1,NTERM
35
C
C   PERFORM FLOW INTEGRATION STEP IN THE SUBSONIC REGION
      CALL OUNS(1,J)
      DO 104 N = 3, N1
40     104 CALL INAS(1,J,N,1)
      CALL INBO(NN,J)
C
      IF(RMB.GE.CSO.OR.DUB.LE.5.0) GO TO 109
105 CONTINUE
C
45     109 II = II+1
      XB0(II) = XB
      RMB0(II) = RMB
      DUB0(II) = DUB
      XX(II,J) = X
50     PP(II,J) = PB
C
      IF(RMB.GE.1..OR.DUB.LE.5.) RETURN
C
      IF(RMB.GE.CSO) GO TO 120
55
C
110 CONTINUE
C
      RETURN
C
60
C   IF THIS IS THE FIRST TIME THROUGH DECREASE THE STEP SIZE BY HALF
120 IF(I.GT.0) GO TO 122
      HS = HS/2.
      H = H/2.
C
65
C   SAVE FLOW PROPERTIES AT THIS STATION FOR FUTURE USE
122 I=I+1
      BX(I) = X
      BXA(I) = XA
      BUP(I) = UB

```

```

70      BMB(I) = RMB
      BDB(I) = DB
      BVS(I) = VS
      BVN(I) = VN
75      DO 124 N = 2, NN
      BU(I,N) = U(J,N)
      BV(I,N) = V(J,N)
124    BY(I,N) = Y(J,N)
C
      IF (I - 4) 126, 150, 150
126    CSO = CSO + DBSO
      GO TO 100
C
150    H = H*2.
      HS = HS*2.
85      HX = HS/SQRT(1. + DYB**2)
C
C      FIND THE X STATION FOR WHICH RMB IS GREATER THAN 1.03 USING A
C      LAGRANGIAN FUNCTION
      DO 160 N = 1, 100
90      XA = XA + HX
      CALL LGRNGN(BMB(1),BMB(2),BMB(3),BMB(4),
      1BXA(1),BXA(2),BXA(3),BXA(4),XA,DBB)
      IF (RMB .GE. 1.03) GO TO 200
160    CONTINUE
95      RETURN
C
C      CALCULATE FLOW PROPERTIES AT THIS X STATION
200    II = -1
      II = II+1
100      NN1(7) = II
      CALL LGRNGN(BDB(1),BDB(2),BDB(3),BDB(4),
      1BXA(1),BXA(2),BXA(3),BXA(4),XA,DBB)
      CALL LGRNGN(BVS(1),BVS(2),BVS(3),BVS(4),
      1BXA(1),BXA(2),BXA(3),BXA(4),XA,VS)
105      CALL LGRNGN(BVN(1),BVN(2),BVN(3),BVN(4),
      1BXA(1),BXA(2),BXA(3),BXA(4),XA,VN)
      CALL ARFL(XA, XB, YB, DYB, DBYP,1)
      CT = 1./SQRT(1. + DYB**2)
      ST = CT*DYB
110      YD = YB + DB*CT
      X = XB - DB*ST
      UD = VS*CT - VN*ST
      VD = VS*ST + VN*CT
      RO = ((C - UD*UD - VD*VD)/(C - 1.))**2.5
      PO = RO**1.4
115      RMO = SQRT((UD*UD + VD*VD)*RO/(1.4*CK*PO))
      CALL LGRNGN(BUB(1),BUB(2),BUB(3),BUB(4),
      1BXA(1),BXA(2),BXA(3),BXA(4),XA,UB)
      RB = ((C - UB*UB)/(C - 1.))**2.5
      PB = RB**1.4
120      RMB = UB/SQRT(1.4*CK*PB/RB)
      DO 220 N = 2, NN
      CALL LGRNGN(BU(1,N),BU(2,N),BU(3,N),BU(4,N),
      1BX(1),BX(2),BX(3),BX(4),X,U(J,N))
      CALL LGRNGN(BV(1,N),BV(2,N),BV(3,N),BV(4,N),
125      1 BX(1),BX(2),BX(3),BX(4),X,V(J,N))
      CALL LGRNGN(BY(1,N),BY(2,N),BY(3,N),BY(4,N),
      1 BX(1),BX(2),BX(3),BX(4),X,Y(J,N))
      VSC = U(J,N)*U(J,N)+V(J,N)*V(J,N)
      R(J,N) = ((C-VSQ)/(C-1.))**2.5
      P(J,N) = P(J,N)**1.4
130      RM(J,N) = SQRT(VSQ*R(J,N)/(1.4*CK*P(J,N)))
C
      CS1 = RMB
      I=0
135
C
      DO 290 K = 1, 50
      DO 290 KK=1,NTERM
C

```

```

140      C   PERFORM FLOW INTEGRATION STEP IN SUPERSONIC REGION
          CALL OUNS(1,J)
          N1 = NN - 1
          DO 275 N = 3, N1
145      275 CALL INAS(1,J,N,1)
          CALL INBO(NN,J)
      C
          IF(RMB.GE.CS1.OR.RMB.LT.1.0.OR.RM(J,NN).GE.RMC) GO TO 285
      C
280      CONTINUE
150      C
          285 II = II+1
          XBO(II) = XB
          RMB0(II) = RMB
          OUBO(II) = OUB
155      XX(II,J) = XB
          PP(II,J) = PB
      C
          IF(RMB.LT.1.0.OR.RMB.GT.2.0) RETURN
      C
          IF (RMB .GE. CS1) GO TO 320
      C
          IF (RM(J,NN).GE.RMC) NN=NN-1
          290 CONTINUE
      C
165      C   SAVE FLOW PROPERTIES AT THIS STATION
          320 I = I+1
          BX(I) = X
          DO 324 N = 2, NN
          BU(I,N) = U(J,N)
170      BV(I,N) = V(J,N)
          324 BY(I,N) = Y(J,N)
      C
          IF (I - 4) 326, 350, 350
      C
175      326 CS1 = CS1 + DCS1
          GO TO 250
      C
      C   CALCULATE FLOW PROPERTIES AT XB FOR INPUT TO NEXT STEP
180      350 YSPR(1) = Y(J,1)
          USPR(1) = U(J,1)
          VSPR(1) = V(J,1)
          DO 360 N = 2, NN
          CALL LGRNGN(BY(1,N),BY(2,N),BY(3,N),BY(4,N),
185      1 BX(1),BX(2),BX(3),BX(4),XB,YSPR(N))
          CALL LGRNGN(BU(1,N),BU(2,N),BU(3,N),BU(4,N),
          1 BX(1),BX(2),BX(3),BX(4),XB,USPR(N))
          360 CALL LGRNGN(BV(1,N),BV(2,N),BV(3,N),BV(4,N),
          1 BX(1),BX(2),BX(3),BX(4),XB,VSPR(N))
          NN = NN+1
          YSP(NN) = YB
          USPR(NN) = UB/SQRT(1.+DYB*DYB)
          VSPR(NN) = USPR(NN)*DYB
          NNSPR = NN
          XASPR = XA
195      II2=1
      C
          RETURN
          END

```



```

      SUBROUTINE IOSPCT2(J,L)
C
C THIS SUBROUTINE PRINTS THE INPUT PARAMETERS AND THE CALCULATED
C OUTPUT FOR SUBROUTINE SPCRT2
5
      COMMON/AINPUT/      AIN(24),NN1(7),HI(6)
      COMMON/YUVSAV/      NNINIT,NNSPR,NNOWN,YUV(156)
      COMMON/OUTCOM/
10      AXA(160),ADU(160),DDQO(160),II,II2
      COMMON/CONSPR/ARMO(160)
      COMMON/COMPRS/XX(160,2),PP(160,2),NP(2)
      DIMENSION ISTAR(5),ITITLE(4)
      DATA (ISTAR(I),I=1,5)/5*10H*****/
      DATA (ITITLE(I),I=1,4)/10H* AIRFOIL ,10HSOLUTION *,10H  UPPER S,
15      1 10HURFACE /
      WRITE(6,200) (ISTAR(I),I=1,5),(ITITLE(I),I=1,2),(ISTAR(I),I=1,5),
      1 (ITITLE(I),I=3,4)
      WRITE(6,210) NN1(5),AIN(7),(AIN(I),I=15,17),HI(5)
      IF((NNSPR.EQ.0).OR.(NNSPR.GT.9)) GO TO 20
20      WRITE(6,220) NNSPR,AIN(19)
      M = (1.0-AIN(7))/0.01+(AIN(7)-0.1)/0.005+(0.1-AIN(3))/HI(5)
      IF(M.LT.470.OR.NNSPR.GE.NN1(5)) GO TO 4
      IF(NNSPR.LT.NN1(5)) WRITE(6,330)
      IF(M.GT.470) WRITE(6,320)
25      IF(NN1(5).LT.NNSPR) WRITE(6,330)
      RETURN
4      DO 5 I=1,160
5      DDQO(I) = 0.
      CALL INVELOC(L,J)
      CALL SPCRT2(J,L)
30      IF(II.EQ.0) RETURN
      IHALF = II/2
      K = MOD(II,2)
      IHALF1 = IHALF
35      IF(K.EQ.1) IHALF1 = IHALF+1
      WRITE(6,400)
      IF(II.EQ.1) GO TO 15
      DO 10 I=1,IHALF
10      WRITE(6,310) AXA(I),ARMO(I),PP(I,J),ADU(I),DDQO(I),AXA(I+IHAF1),
40      1 ARMO(I+IHAF1),PP(I+IHAF1,J),ADU(I+IHAF1),DDQO(I+IHAF1)
      IF(K.NE.1) GO TO 18
15      WRITE(6,310) AXA(IHALF1),ARMO(IHALF1),PP(IHALF1,J),ADU(IHALF1),
40      1 DDQO(IHALF1)
18      IF(II2.EQ.0) WRITE(6,260)
      RETURN
45      20 WRITE(6,250)
      RETURN
200 FORMAT(4(/),7X,12A10/57X,2A10)
210 FORMAT( //20X,4HNC =,I2//20X,12HSHOCK LOC. =F10.6,
50      1 10H, BETA = ,F10.6,10H, DELS =,F10.6,10H, CDDQ =,F10.6,
      2 8H, HO =,F10.6)
220 FORMAT(/20X,31HFROM INITIAL CONDITIONS, NN =,I2,13H, X(INIT) =
      1 ,F10.6)
250 FORMAT(/20X,45H*****PREVIOUS STEP HAS NOT BEEN COMPUTED)
55      250 FORMAT(/20X,39H*****INTEGRATION WAS NOT COMPLETED )
310 FORMAT(2(10X,5F10.4))
320 FORMAT(/20X,29H*****STEP SIZE TOO SMALL)
330 FORMAT(/20X,49H*****INSUFFICIENT NUMBER OF STRIPS AVAILABLE)
400 FORMAT(/2(17X,1HX,9X,2HMO,8X,2HPO,7X,4HDOJX,6X,3HDDQ,1X))
60      END

```

```

SUBROUTINE SPRCRT2(J,L)
C
C THIS SUBROUTINE PERFORMS FLOW INTEGRATION FOR THE BULK OF THE
C AIRFOIL SURFACE
5
C
COMMON C ,CK ,RS ,FM ,ALPHA
COMMON/ACOM/X ,XA ,VN ,VS ,H ,DY
1 ,VO ,PO ,RO ,UO ,VO ,RMO ,DUO
2 ,Y(2,10),P(2,10),R(2,10),U(2,10),V(2,10),RM(2,10),DU(2,10)
10 COMMON/DCOM/CS ,CZ ,DV1 ,Q1 ,DQ1 ,RK
1 ,VOO ,ISKIP
COMMON/AINPUT/ ADUM(6),SL ,BDUM(7),BETAU ,DELS
1 ,CDDQ ,RKI ,XASPR ,CDUM(3),CSI ,CZI ,NN1(4)
2 ,NNSPR ,NN2(2),H1(4) ,HO ,HOWN
15 COMMON/YUVSAV/ NNINIT,NNO,NNOWN
1 ,YUV(60),YSPR(10),USPR(10),VSPR(10),YU(10),UU(10),VU(10)
2 ,VL(10),UL(10),VL(10),YOU,VOL,UOU,UOL,WOU,VOL
COMMON/OUTCOM/
20 1 AXA(160),ADU(160),DDQO(160),II ,II2
COMMON/COMPRS/XX(160,2),PP(160,2),NP(2)
COMMON/COMSPR/ARMO(160)
D(AO, A1, A2, Z) = AO + A1*Z + A2*Z*Z
C
C INITIALIZE INPUT
25
C
NN = NNSPR
II = 0
II2=0
NTERM = 3
ISKIP = 3
30 PS = RS**1.4
CS = 1.0
CZ = C
H = HO
XA = XASPR
35 CALL ARFL(XA,X,YO,DY,DUM,J)
BETA = BETAU/57.2957795
YO = YSPR(NNO)
UO = USPR(NNO)
VO = VSPR(NNO)
40 QO = SQRT(UO*UO+VO*VO)
RO = ((C - QO**2)/(C - 1.))**2.5
PO = RO**1.4
RMO = QO/SQRT(1.4*CK*PO/RO)
DO 102 N = 1, NN
45 Y(J,N) = YSPR(N)
U(J,N) = USPR(N)
V(J,N) = VSPR(N)
VSQ = U(J,N)*U(J,N)+V(J,N)*V(J,N)
R(J,N) = ((C-VSQ)/(C-1.))**2.5
50 P(J,N) = R(J,N)**1.4
102 RM(J,N) = SQRT(VSQ*R(J,N)/(1.4*CK*P(J,N)))
C
M = ABS((.99-X)/H)
DQ1 = 0.0
55 DO 295 K=1,M
DO 280 KK=1,NTERM
DQO = DQ1
C
C PERFORM FLOW INTEGRATION STEP IN SUPERSONIC REGION
60
C
CALL OUNSI(1,J)
X = X+H
DO 270 N = 3, NN
270 CALL INAS(1,J,N,NN)
C
65
C
IF (ABS(DUO).GE.100.0.OR.X.LT.0.0.OR.X.GE.SL.OR.RMO.LT.1.)GOTO 285
C
IF (X.GE. 0.1) H = 0.005
C

```

```

70      200 CONTINUE
      C
      205 DDQ = (DQ1 - DQ0)/H
        II = II+1
        AXA(II) = XA
75      ADU(II) = DU(J,NN)
        ARMO(II) = RMO
        DDQO(II) = DDQ
        XX(II,J) = X
        PP(II,J) = P0
80
      IF(DDQ.GE.CDDQ) NN = NN-1
      C
      IF(ABS(DUO).GE.100..OR.X.LT.0.0) RETURN
      C
85      IF (RMO .LT. 1.0) RETURN
      C
      IF (X .GE. 0.1) H = 0.005
      C
      IF(X.GE.SL) GO TO 300
90      C
      295 CONTINUE
      RETURN
      C
      C  APPLY RANKINE HUGONIOT RELATIONS THROUGH SHOCK WAVE
95      300 Q0 = SQRT(U0*U0 + V0*V0)
        U01 = Q0*SIN(BETA)
        V01 = Q0*COS(BETA)
        RMO = RMO*SIN(BETA)
        R2R1 = 2.4*RMO**2/(0.4*RMO**2 + 2.)
        P2P1 = 1. + 7./6.*(RMO**2 - 1.)
100      U02 = U01/R2R1
        V02 = V01
        Q0 = SQRT(U02**2 + V02**2)
        U0 = Q0/SQRT(1. + DY*DY)
        V0 = U0*DY
105      R0 = R0*R2R1
        P0 = P0*P2P1
      C
      IF (DELS .LE. 0.0) GO TO 306
110      PS2 = PS*(2.4*RMO**2/(0.4*RMO**2 + 2.))**3.5/P2P1**2.5
        RS2 = R0*(PS2/P0)**(1./1.4)
        CZ = (C - 1.)*PS2/RS2
        CS = P0/R0**1.4
      C
115      306 H = 0.01
        RMO = SQRT((U0*U0 + V0*V0)/(1.4*CK*P0/R0))
        IF(L.EQ.2) CALL LGRNGN(V0,V(J,NN-1),V(J,NN-2),V(J,NN-3),0.0,
1      V(J,NN-1)-Y0,V(J,NN-2)-Y0,V(J,NN-3)-Y0,V(J,NN)-Y0,V(J,NN))
      C
120      M = (1.0-X)/H
        DO 320 K = 1, M
        DO 308 KK=1,NTERM
      C
      C  PERFORM FLOW INTEGRATION STEP IN SUBSONIC REGION
125      CALL OUNS(1,J)
        X = X+H
        DO 307 N = 3, NN
        307 CALL INAS(1,J,N,NN)
      C
130      IF(RMO.GT.1.0.OR.X.GE.1.0.OR.ABS(DUO).GE.50.0.OR.X.LT.0.) GO TO 310
        303 CONTINUE
      C
135      310 II = II+1
        AXA(II) = XA
        ADU(II) = DU(J,NN)
        ARMO(II) = RMO
        XX(II,J) = X
        PP(II,J) = P0
      C

```

```

140      IF (ABS(DUO) .GE. 50.0 .OR. X .LT. 0.0 .OR. RMO.GT.1.0) RETURN
      C
      IF(X.GE.1.0) GO TO 360
      C
      320 CONTINUE
145      C
      C   SAVE FLOW PROPERTIES CALCULATED AT FINAL STATION AS INPUT TO NEXT
      C   STEP
      360 II2=1
      NP(J) = II
150      NNOWN = NN
      DO 400 N=1,NN
      VU(N) = V(J,N)
      UU(N) = U(J,N)
      400 VU(N) = V(J,N)
155      YOU = VO
      UOU = UO
      VOU = VO
      CSI = CS
      CZI = CZ
160      RETURN
      END

```

```

      SUBROUTINE IODNSTM(J)
C
C   THIS SUBROUTINE PRINTS THE INPUT PARAMETERS AND THE CALCULATED
C   OUTPUT FOR SUBROUTINE DWNSTRM
5
C
      COMMON/AINPUT/      AIN(24),NN1(7) ,HI(6)
      COMMON/OUTCOM/
1      AX(160) ,APO(160) ,AP1(160) ,II      ,II1
      COMMON/COMDOWN/ARMO(160)
10     COMMON/VUUSAV/NNINIT ,NNSPR ,NNDWN ,YUV(156)
      DIMENSION ISTAR(5),ITITLE(2)
      DATA (ISTAR(I),I=1,5)/5*10H*****/
      DATA (ITITLE(I),I=1,2)/10HDOWNSTREAM,10H SOLUTION*/
15     WRITE(6,200) (ISTAR(I),I=1,5),(ITITLE(I),I=1,2),(ISTAR(I),I=1,5)
      WRITE(6,210) NN1(6),HI(6),AIN(18)
      WRITE(6,220) AIN(7),AIN(15),AIN(23),AIN(24)
      M = 9.0/HI(6)
      IF(M.LT.470.OR.NNDWN.GE.NN1(6)) GO TO 4
      IF(M.GT.470) WRITE(6,310)
20     IF(NNDWN.LT.NN1(6)) WRITE(6,320)
      RETURN
4     CALL DWNSTRM(J)
      IF(II.EQ.0) RETURN
      IHALF = II/2
25     K = MOD(II,2)
      IHALF1 = IHALF
      IF(K.EQ.1) IHALF1 = IHALF+1
      WRITE(6,400)
      IF(II.EQ.1) GO TO 15
30     DO 10 I=1,IHALF
      WRITE(6,300) AX(I),ARMO(I),APO(I),AP1(I),AX(I+IHALF1),ARMO(I+IHALF
      1 1),APO(I+IHALF1),AP1(I+IHALF1)
10    CONTINUE
      IF(K.NE.1) GO TO 18
35     WRITE(6,300) AX(IHALF1),ARMO(IHALF1),APO(IHALF1),AP1(IHALF1)
18    CONTINUE
      IF(II1.EQ.0) WRITE(6,250)
      RETURN
200  FORMAT(1H1,4(/),7X,12A10)
40    210  FORMAT(//20X,4HNN =,I2,7H, H =,F10.6,8H, RK =F10.6)
      220  FORMAT(/20X,45HFROM UPPER SURFACE INTEGRATION, SHOCK LOC. =
      1 F8.4 ,10H, BETA = F8.4 ,3H, CS = F8.4 ,8H, CZ = F8.4 )
250  FORMAT(/20X,39H*****INTEGRATION WAS NOT COMPLETED )
300  FORMAT(10X,2(10X,4F10.4))
45    310  FORMAT(/20X,29H*****STEP SIZE TOO SMALL)
      320  FORMAT(/20X,49H*****INSUFFICIENT NUMBER OF STRIPS AVAILABLE)
400  FORMAT(/8X,2(19X,1HX,9X,2HMO,8X,2HPO,8X,2HP1))
      END

```

```

SUBROUTINE DWNSTRM(J)
COMMON C ,CK ,RS ,FM ,ALPHA
COMMON/ACOM/X ,XA ,VN ,VS ,H ,DY
1 ,VO ,PO ,RO ,UO ,VO ,RMO ,DUO
5 2 ,Y(2,10),P(2,10),R(2,10),U(2,10),V(2,10),RM(2,10),DU(2,10)
COMMON/DCOM/CS ,CZ ,DV1 ,Q1 ,DQ1 ,RK
1 ,VOO ,ISKIP
COMMON/AINPUT/ AIN(17),RKI ,DDUM(4),CSI ,CZI
1 ,NN1(5) ,NN ,NN2 ,HT(5) ,HI
10 COMMON/YUVSAV/ NNINIT,NNSPR,NNOWN
1 ,YUV(60),YSPR(10),USPR(10),VSPR(10),YU(10),UU(10),VU(10)
2 ,VL(10),UL(10),VL(10),YOU,YOL,UOU,UOL,VOU,VOL
COMMON/OUTCOM/
15 1 AX(160) ,APO(160) ,AP1(160) ,II ,II1
COMMON/COMDWN/ARMO(160)

C
C INITIALIZE INPUT
NTERM = 4
CS = CSI
20 CZ = CZI
H = HI
RK = RKI
II = 0
II1=0
25 ISKIP = 1
IF(J.EQ.1) GO TO 4
DO 3 N=1,NN
YU(N) = YL(N)
30 UU(N) = UL(N)
3 VU(N) = VL(N)
4 DO 5 N=1,NN
Y(1,N) = YU(N)
U(1,N) = UU(N)
5 V(1,N) = VU(N)
35 X = 1.
DO 14 N = 1, NN
VSQ = UU(N)*UU(N)+VU(N)*VU(N)
R(1,N) = ((C-VSQ)/(C-1.))**2.5
P(1,N) = R(1,N)**1.4
40 RM(1,N) = SQRT(VSQ/(1.4*CK*P(1,N)/R(1,N)))
14 DU(1,N) = 0.
VSQ = UOU*UOU+VOU*VOU
IF(J.EQ.2) VSQ = UOL*UOL+VOL*VOL
45 RO = ((CZ - VSQ)/(CS*(C-1.))**2.5
PO = RO **1.4*CS
RMO =SQRT(VSQ/(1.4*CK*PO/RO))
DUO = 0.
YO = (YOU-YOL)/2.
QOU = SQRT(VSQ)
50 TU = ATAN(VOU/UOU)

C
C DETERMINE T AND VOO- INITIAL VALUES
TL =-ATAN(VOL/UOL)
T = (TU + TL)/2.
55 UO = QOU*COS(T)
VO = QOU*SIN(T)
VOO = VO
M = ABS(10./H/NTERM)
DO 40 K = 1, M
60 DO 35 KK=1,NTERM

C
C PERFORM FLOW INTEGRATION STEP
CALL OUNS(1,1)
CALL INAS(1,1,NN,NN)
65 C
IF(RM(1,NN).GT.0.95) GO TO 36
IF (X .GE.10..OR. X .LT .0.0 .OR. RMO .GE. 0.97) GO TO 36
X = X + H
35 CONTINUE

```

```

70      36 II = II+1
        AX(II) = X
        ARMO(II) = RMO
        APO(II) = PO
        AP1(II) = P(1,NN)
75      IF(X,GE.10.) GO TO 50
        IF(RM(1,NN).GT.0.95.OR.X.LT.0.0.OR.RMO.GE.0.97) RETURN
        40 CONTINUE
        50 II1=1
        RETURN
80      END

```

SUBROUTINE AKUTTA

```

C
C THIS SUBROUTINE PRINTS THE CALCULATED PRESSURE DISTRIBUTION ON THE
C UPPER AND LOWER SURFACES
5
C
COMMON/COMPRS/XX(160,2),PP(160,2),NN1,NN2
DIMENSION ISTAR(4),ITITLE(4)
DATA (ISTAR(I),I=1,4)/4*10H*****/
DATA (ITITLE(I),I=1,4)/10H**** PARTI,10HAL PRESSUR,10HE DISTRIBU,
10 110HTION *****/
WRITE(6,200) (ISTAR(I),I=1,4),(ITITLE(I),I=1,4),(ISTAR(I),I=1,4)
IF(NN1.EQ.0.OR.NN2.EQ.0) RETURN
WRITE(6,400)
N1 = NN1
N2 = NN2
15 N1HALF = N1/2
N2HALF = N2/2
J1 = MOD(N1,2)
J2 = MOD(N2,2)
20 IHALF = N1HALF
IF(N1.GT.N2) IHALF = N2HALF
IF(J1.EQ.1) N1HALF = N1HALF+1
IF(J2.EQ.1) N2HALF = N2HALF+1
DO 10 I=1,IHALF
25 10 WRITE(6,300) XX(I,1),PP(I,1),XX(I+N1HALF,1),PP(I+N1HALF,1),
1 XX(I,2),PP(I,2),XX(I+N2HALF,2),PP(I+N2HALF,2)
IF(N1.GT.N2) GO TO 30
IF(J1.NE.1) GO TO 18
WRITE(6,310) XX(N1HALF,1),PP(N1HALF,1),XX(N1HALF,2),PP(N1HALF,2),
30 1 XX(N1HALF+N2HALF,2),PP(N1HALF+N2HALF,2)
18 N2STOP = N2HALF
IF(J2.EQ.1) N2STOP = N2HALF-1
NSTART = N1HALF+1
DO 19 I=NSTART,N2STOP
35 19 WRITE(6,320) XX(I,2),PP(I,2),XX(I+N2HALF,2),PP(I+N2HALF,2)
IF(J2.NE.1) GO TO 50
WRITE(6,320) XX(N2HALF,2),PP(N2HALF,2)
GO TO 50
40 30 WRITE(6,340) XX(N2HALF,1),PP(N2HALF,1),XX(N1HALF+N2HALF,1),
1 PP(N1HALF+N2HALF,1),XX(N2HALF,2),PP(N2HALF,2)
38 N1STOP = N1HALF
IF(J1.EQ.1) N1STOP = N1HALF-1
NSTART = N2HALF+1
DO 39 I=NSTART,N1STOP
45 39 WRITE(6,340) XX(I,1),PP(I,1),XX(I+N1HALF,1),PP(I+N1HALF,1)
IF(J1.NE.1) GO TO 50
WRITE(6,340) XX(N1HALF,1),PP(N1HALF,1)
50 CONTINUE
RETURN
50 200 FORMAT(1H1,4(/)7X,12A10)
300 FORMAT(12X,2(10X,4F10.6))
310 FORMAT(22X,2F10.6,30X,4F10.6)
320 FORMAT(72X,4F10.6)
340 FORMAT(22X,4F10.6,10X,2F10.6)
55 400 FORMAT(/35X,13HUPPER SURFACE,37X,13HLOWER SURFACE//10X,
1 2(10X,2(8X,1HX,9X,2HPO)))
END

```



```

SUBROUTINE INVELOC(L,J)
COMMON/COMMON/NN
COMMON/ACOM/X,XA,VN,VS,H,DY,YO,PO,RO,UO,VO,RMO,DUO,
1 Y(2,10),P(2,10),R(2,10),U(2,10),V(2,10),RM(2,10),DU(2,10)
COMMON/YUVSAV/ NNINIT,NNO,NNDWN
1 ,YUV1(60),YSPR(10),USPR(10),VSPR(10),YUV2(66)
D(A0,A1,A2,Z) = A0+A1*Z+A2*Z*Z
IF(J.EQ.2) GO TO 2
NN = NNO-1
10 DO 1 K=1,NN
V(J,K) = YSPR(K)
U(J,K) = USPR(K)
1 V(J,K) = VSPR(K)
YO = YSPR(NNO)
15 UO = USPR(NNO)
VO = VSPR(NNO)
2 IF(L.EQ.1) GO TO 4
IF(L.GE.3) GO TO 3
WRITE(6,310)
20 CALL LGRNGN(VO,V(J,NN-1),V(J,NN-2),V(J,NN-3),0.0,Y(J,NN-1)-YO,
1 Y(J,NN-2)-YO,Y(J,NN-3)-YO,Y(J,NN)-YO,V(J,NN))
GO TO 5
3 WRITE(6,320)
Y1 = V(J,NN-2)-Y(J,NN-1)
25 Y2 = V(J,NN-3)-Y(J,NN-1)
CALL A1SUB(Y1,Y2,V(J,NN-1),V(J,NN-2),V(J,NN-3),A1V)
CALL A2SUB(Y1,Y2,V(J,NN-1),V(J,NN-2),V(J,NN-3),A2V)
V(J,NN) = D(V(J,NN-1),A1V,A2V,Y(J,NN)-Y(J,NN-1))
GO TO 5
30 4 WRITE(6,300)
5 WRITE(6,400)
NNP1 = NN+1
IHALF = NNP1/2
K = MOD(NNP1,2)
IHALF1 = IHALF
35 IF(K.EQ.1) IHALF1=IHALF+1
DO 10 I=1,IHALF
IF((I+IHALF1).EQ.NNP1) GO TO 7
6 WRITE(6,410) V(J,I),U(J,I),V(J,I),Y(J,I+IHALF1),U(J,I+IHALF1),
40 1 V(J,I+IHALF1)
GO TO 10
7 WRITE(6,410) V(J,I),U(J,I),V(J,I),YO,UO,VO
10 CONTINUE
IF(K.EQ.0) GO TO 12
45 WRITE(6,410) V(IHALF1,J),U(IHALF1,J),V(IHALF1,J)
12 IF(J.EQ.1) VSPR(NN) = V(J,NN)
RETURN
300 FORMAT(/47X,40H***INTERMEDIATE VELOCITY DISTRIBUTION***)
50 310 FORMAT(/34X,66H***INTERMEDIATE VELOCITY DISTRIBUTION USING LAGRAN
1GIAN FUNCTION***)
320 FORMAT(/34X,65H***INTERMEDIATE VELOCITY DISTRIBUTION USING PARABO
1LIC FUNCTION***)
400 FORMAT(/17X,2(19X,1HY,9X,1HU,9X,1HV))
55 410 FORMAT(20X,2(10X,3F10.6))
END

```

```

      SUBROUTINE ARFL(XA,XB,YB,DYB,DDYB,J)
C
C   THIS SUBROUTINE DETERMINES THE Y COORDINATE AND ITS FIRST AND
C   SECOND DERIVATIVES AT A POINT ON THE AIRFOIL
5
C   COMMON/PTARFL/XX(40,2) ,YY(40,2) ,AM(40,2) ,CA      ,SA
      IF(XA.GE.1.0) GO TO 60
      DO 10 I=1,40
      IF(XA-XX(I,J)) 20,20,10
10  CONTINUE
      XA = 10000.
      RETURN
20  IF(I.GT.1) GO TO 30
      XA = 0.001
      YA=0.001
15  DYB = AM(I,J)
      DDYA = (-4.*AM(1,J)-2.*AM(2,J)+6.*(YY(2,J)-YY(1,J)) /
1      (XX(2,J)-XX(1,J)))/(XX(2,J)-XX(1,J))
      GO TO 40
20  H = XX(I,J)-XX(I-1,J)
      X2MXA = XX(I,J)-XA
      XAMX1 = XA-XX(I-1,J)
      YA = AM(I-1,J)*X2MXA**2*XAMX1/H**2
      YA = YA-AM(I,J)*XAMX1**2*X2MXA/H**2
25  YA = YA+YY(I-1,J)*X2MXA**2*(2.*XAMX1+H)/H**3
      YA = YA+YY(I,J)*XAMX1**2*(2.*X2MXA+H)/H**3
      DYA = AM(I-1,J)*X2MXA*(X2MXA-2.*XAMX1)/H**2
      DYA = DYA-AM(I,J)*XAMX1*(2.*X2MXA-XAMX1)/H**2
      DYA = DYA+6.*(YY(I,J)-YY(I-1,J))*X2MXA*XAMX1/H**3
30  DDYA = -2.*AM(I-1,J)*(2.*X2MXA-XAMX1)/H**2
      DDYA = DDYA+2.*AM(I,J)*(2.*XAMX1-X2MXA)/H**2
      DDYA = DDYA+6.*(YY(I,J)-YY(I-1,J))*(X2MXA-XAMX1)/H**3
40  IF(J.EQ.2) GO TO 50
      XB = XA*CA+YA*SA
      YB = YA*CA-XA*SA
35  DYB = (DYA*CA-SA)/(CA+DYA*SA)
      DDYB = DDYA*(CA-DYB*SA)**3
      RETURN
50  XB = XA*CA-YA*SA
      YB = YA*CA+XA*SA
40  DYB = (DYA*CA+SA)/(CA-DYA*SA)
      DDYB = DDYA/(CA-SA*DYA)**3
      RETURN
60  XB = 1.0
45  YB = SA/CA
      DYB = YB
      DDYB = 0.
      RETURN
      END

```

```

SUBROUTINE LGRNGN(A1,A2,A3,A4,X1,X2,X3,X4,X,ANS)
F1 = X-X1
F2 = X-X2
F3 = X-X3
5 F4 = X-X4
F12 = X1-X2
F13 = X1-X3
F14 = X1-X4
F21 = X2-X1
10 F23 = X2-X3
F24 = X2-X4
F31 = X3-X1
F32 = X3-X2
F34 = X3-X4
15 F41 = X4-X1
F42 = X4-X2
F43 = X4-X3
D1 = F12*F13*F14
D2 = F21*F23*F24
20 D3 = F31*F32*F34
D4 = F41*F42*F43
U1 = F2*F3*F4
U2 = F1*F3*F4
U3 = F1*F2*F4
25 U4 = F1*F2*F3
ANS1 = A1*U1/D1+A2*U2/D2
ANS2 = A3*U3/D3+A4*U4/D4
ANS = ANS1+ANS2
RETURN
30 END

```

```

SUBROUTINE A1SUB(Y1,Y2,U0,U1,U2,ANS)
F1 = Y2*Y2*U1
F2 = Y1*Y1*U2
F3 = Y2*Y2-Y1*Y1
5 F4 = Y2-Y1
F5 = Y1*Y2
ANS1 = F1-F2-F3*U0
ANS2 = F4*F5
ANS = ANS1/ANS2
10 RETURN
END

```

```

SUBROUTINE A2SUB(Y1,Y2,U0,U1,U2,ANS)
F1 = -Y2*U1
F2 = Y1*U2
F3 = Y2-Y1
5 F4 = Y1*Y2
ANS1 = F1+F2+F3*U0
ANS2 = F3*F4
ANS = ANS1/ANS2
RETURN
10 END

```

```

SUBROUTINE DIST(M,I,N,DV1,DVS,DV1)
C
C THIS SUBROUTINE PERFORMS A FLOW INTEGRATION STEP ON THE STAGNATION
C STREAMLINE IN THE UPSTREAM SOLUTION
5 C THIS SUBROUTINE INCLUDES THE EFFECTS OF THE CROSS VELOCITY GRADIENT
C ,DV00, IN DETERMINING THE FLOW CONDITIONS FAR UPSTREAM FROM THE AIRFOIL
C
COMMON C ,CK ,RS ,FM ,ALPHA
COMMON/ACOM/X ,XA ,VN ,VS ,H ,DY
10 1 ,Y0 ,PO ,RO ,UO ,VO ,RMO ,DUO
2 ,Y(2,10),P(2,10),R(2,10),U(2,10),V(2,10),RM(2,10),DU(2,10)
COMMON/BCOM/ XO ,DV00 ,L
COMMON/DCOM/ DRHU(2),DPRU(2),DRUV(2)
15 DIMENSION ZVS(5),ZV1(5),ZY1(5)
DATA ZV1,ZVS,ZY1/ 15*0.0 /
J=2
IF(I.EQ.2) J=1
DO 700 K=2,5
RN = (K-1)/2
20 RNH = RN/2.*H
AY1 = Y0*H+ZY1(K-1)*RNH
AVS = VS+ZVS(K-1)*RNH
AV1 = V0*H
IF (AVS - AV1) 200, 100, 100
25 100 IF (C - AVS**2) 200, 300, 300
200 X = -1.
RETURN
300 AR1 = ((C - AVS**2)/(C - 1.))**2.5
AP1 = AR1**1.4
30 AU1 = SQRT(AVS**2 - AV1**2)
AX = X + RNH
Y10 = AY1+Y(I,N)
Y20 = Y(J,N)+Y(I,N)
Y21 = Y(J,N)-AY1
35 Y10SQ = Y10*Y10
Y20SQ = Y20*Y20
Y10QU = Y10SQ*Y10SQ
Y20QU = Y20SQ*Y20SQ
DY = -V(I,N)/U(I,N)
40 DY1 = AV1/AU1
DY2 = V(J,N)/U(J,N)
D = Y10*Y20*Y21
DD = -Y21*(Y20+Y10)*DY + Y20*(Y21-Y10)*DY1 +Y10*(Y21+Y20)*DY2
45 EY2 = Y20SQ-Y10SQ
ALOC = R(I,N)*U(I,N)
ALOY = -ALOC*V(I,N)
AL1C = AR1*AU1 - ALOC
AL1Y = AR1*AU1*AV1 - ALOY
AL2C = R(J,N)*U(J,N) -ALJC
50 AL2Y = R(J,N)*U(J,N)*V(J,N) -ALOY
A1C = (AL1C*Y20SQ-AL2C*Y10SQ)/D
A1Y = (AL1Y*Y20SQ-AL2Y*Y10SQ)/D
A2C = (AL2C*Y10 - AL1C*Y20)/D
A2Y = (AL2Y*Y10 - AL1Y*Y20)/D
55 F1 = Y10*(D-EY2*Y10/2.+Y10SQ*Y21/3.)
F2 = Y10SQ*Y20*(Y20/2.-Y10/3.)
FC1 = AL1C+2.*AL2C
FC2 = Y20 -Y10/3.
FC3 = AL1Y+2.*AL2Y
60 FC4 = Y10/2.-Y20/3.
FC5 = AL1C-AL2C
FC6 = Y10-Y2/3.
FC7 = A1C/2.+Y20*A2C/3.
FC8 = AL1Y-AL2Y
65 FC9 = A1Y/2.+Y20*A2Y/3.
F3C = -Y10QU*DRHU(J)/6.
F3C = F3C +(-AL1C*D+Y10SQ*(Y10*FC1/3.-Y20*AL1C))*DY
F3C = F3C -2.*AL2C*Y10SQ*Y10/3.*DY1
F3C = F3C +AL1C*Y10SQ*FC2*DY2
70 F3C = F3C -Y10SQ*(A1C/2.+Y10*A2C/3.)*DD

```

```

F3C = F3C + (AR1*AV1+R(I,N)*V(I,N))*D
F3Y = -Y10QU*DRUV(J)/6.
F3Y = F3Y + (-AL1Y*D + Y10SQ*(Y10*FC3/3. - Y20*AL1Y))*DY
75 F3Y = F3Y - 2.*AL2Y*Y10SQ*Y10/3.*DY1
F3Y = F3Y + AL1Y*Y10SQ*FC2*DY2
F3Y = F3Y - Y10SQ*(A1Y/2. + Y10*A2Y/3.)*DD
F3Y = F3Y + (CK*AP1+AR1*AV1*AV1-CK*P(I,N)-R(I,N)*V(I,N)*V(I,N))*D
F4 = Y20*(D + Y20*(-EY2/2. + Y20*Y21/3.))
F5 = Y20QU/6.
80 F6C = -Y10*Y20SQ*FC4*DRHU(J)
F6C = F6C + (-AL2C*D + Y20SQ*(AL2C*Y10-AL1C*Y20+Y20*FC5/3.))*DY
F6C = F6C - Y20SQ*(AL2C*FC6*DY1-2.*Y20*AL1C/3.*DY2+FC7*DD)
F6C = F6C + (R(J,N)*V(J,N)+R(I,N)*V(I,N))*D
85 F6Y = -Y10*Y20SQ*FC4*DRUV(J)
F6Y = F6Y + (-AL2Y*D + Y20SQ*(AL2Y*Y10-AL1Y*Y20+Y20*FC8/3.))*DY
F6Y = F6Y - Y20SQ*(AL2Y*FC6*DY1 - 2.*Y20*AL1Y/3.*DY2+FC9*DD)
F6Y = F6Y + (CK*(P(J,N)-P(I,N)) + R(J,N)*V(J,N)*V(J,N) - R(I,N)*
1 V(I,N)*V(I,N))*D
DEL = F1*F5 - F2*F4
90 E2 = F4*F3C - F1*F6C
E6 = F4*F3Y - F1*F6Y
ZVS(K) = DV00*(AX/X0)**L/(AVS**2*AR1/(1.4*CK*AP1)-1.)
ZV1(K) = (E6 - AV1*E2)/(AR1*AU1*DEL)
700 ZY1(K) = DY1
95 OVS = (ZVS(2) + 2.*(ZVS(3) + ZVS(4)) + ZVS(5))/6.
DV1 = (ZV1(2) + 2.*(ZV1(3) + ZV1(4)) + ZV1(5))/6.
DY1 = (ZY1(2) + 2.*(ZY1(3) + ZY1(4)) + ZY1(5))/6.
RETURN
END

```

```

SUBROUTINE STMN(N,T,DY,DVS)
C
C THIS SUBROUTINE PERFORMS AFLOW INTEGRATION STEP ON THE STAGNATION
C STREAMLINE IN THE UPSTREAM SOLUTION
5 C THIS SUBROUTINE NEGLECTS THE EFFECTS OF CHANGES IN THE VERTICAL
C COMPONENT OF THE STAGNATION STREAMLINE IN THE FLOW INTEGRATION
C
COMMON C ,CK ,RS ,FM ,ALPHA
COMMON/ACOM/X ,XA ,VN ,VS ,H ,DY1
10 1 ,YO ,PO ,RO ,UO ,VO ,RMO ,DUO
2 ,Y(2,10),P(2,10),R(2,10),U(2,10),V(2,10),RM(2,10),DU(2,10)
COMMON/OCOM/ DRHU(2),DPRU(2),DRUV(2)
DIMENSION ZY(5),ZVS(5),ZT(5)
DATA ZY,ZVS,ZT/15*0.0/
15 DO 700 K=2,5
RN = (K-1)/2
RNH = RN/2.*H
AVS = VS+ZVS(K-1)*RNH
AY = YO+ZY(K-1)*RNH
20 AT = T + ZT(K-1)*RNH
IF (C - AVS**2) 100, 300, 300
100 X = -1.
RETURN
300 AR = ((C - AVS**2) / (C - 1.))**2.5
25 AP = AR**1.4
Y10 = AY+Y(2,N)
Y20 = Y(1,N)+Y(2,N)
ST = SIN(AT)
CT = COS(AT)
30 DY = ST/CT
VNO = -U(2,N)*ST -V(2,N)*CT
VN2 = -U(1,N)*ST +V(1,N)*CT
VSO = U(2,N)*CT -V(2,N)*ST
VS2 = U(1,N)*CT +V(1,N)*ST
35 CALL A1SU9(Y10,Y20, R(2,N)*VSO*VNO,0.0,R(1,N)*VS2*VN2,A1RUV)
CALL A2SU9(Y10,Y20, R(2,N)*VSO*VNO,0.0,R(1,N)*VS2*VN2,A2RUV)
DVDY = (A1RUV + 2.*A2RUV*Y10) / (AR*AVS)
CALL A1SU3(Y10,Y20,P(2,N),AP,P(1,N),A1P)
CALL A2SU3(Y10,Y20,P(2,N),AP,P(1,N),A2P)
40 DDPY = A1P + 2.*A2P*Y10
ZVS(K) = DVDY/ (AVS*AVS*AR/(1.4*CK*AP)-1.)
ZT(K) = CK/(AR*AVS**2)*(DY*(-AR*AVS/CK)*ZVS(K)-(1.+DY**2)*DDPY)
700 ZY(K) = DY
45 DVS = (ZVS(2) + 2.*(ZVS(3) + ZVS(4)) + ZVS(5))/6.
DY = (ZY(2) + 2.*(ZY(3) + ZY(4)) + ZY(5))/6.
DT = (ZT(2) + 2.*(ZT(3) + ZT(4)) + ZT(5))/6.
X = X + H
VS = VS + H*DVS
YO = YO+H*DY
50 T = T + H*DT
UO = VS*COS(T)
VO = VS*SIN(T)
RO = ((C-VS**2)/(C-1.))**2.5
PO = RO**1.4
55 RMO = VS/SQRT(1.4*CK*PO/RO)
RETURN
END

```

```

      SUBROUTINE LUMR(M,I,N,DY1,OVS,DV1)
C
C   THIS SUBROUTINE PERFORMS A FLOW INTEGRATION STEP ON THE STAGNATION
C   STREAMLINE IN THE UPSTREAM SOLUTION
5
C   COMMON      C      ,CK      ,RS      ,FM      ,ALPHA
COMMON/ACOM/X      ,XA      ,VN      ,VS      ,H      ,DY
1   ,YO      ,PO      ,RO      ,UO      ,VO      ,RMO      ,DUO
2   ,Y(2,10),P(2,10),R(2,10),U(2,10),V(2,10),RM(2,10),DU(2,10)
10  COMMON/OCOM/      DRHU(2),DPRU(2),DRUV(2)
      DIMENSION ZVS(5),ZV1(5),ZY1(5)
      DATA ZY1,ZVS,ZV1/15*0.0/
      J=2
      IF(I.EQ.2) J=1
15  DO 700 K=2,5
      RN = (K-1)/2
      RNH = RN/2.*H
      AY1 = YO*H+ZY1(K-1)*RNH
      AVS = VS +ZVS(K-1)*RNH
20  AV1 = VO*H
      IF (AVS - AV1) 200, 100, 100
100 IF      (C - AVS**2) 200, 300, 300
200 X = -1.
      RETURN
25 300 AR1 = ((C - AVS**2      )/(C - 1.))**2.5
      AP1 = AR1**1.4
      AU1 = SQRT(AVS**2 - AV1**2)
      Y10 = AY1+Y(I,N)
      Y20 = Y(J,N)+Y(I,N)
30  Y21 = Y(J,N)-AY1
      Y10SQ = Y10*Y10
      Y20SQ = Y20*Y20
      Y10OU = Y10SQ*Y10SQ
      Y20OU = Y20SQ*Y20SQ
35  DY = -V(I,N)/U(I,N)
      DY1 = AV1/AU1
      DY2 = V(J,N)/U(J,N)
      CT = 1.0/SQRT(1. + DY1**2)
      ST = DY1/SQRT(1. + DY1**2)
40  VNO = -U(I,N)*ST-V(I,N)*CT
      VN2 = -U(J,N)*ST+V(J,N)*CT
      VSO = U(I,N)*CT-V(I,N)*ST
      VS2 = U(J,N)*CT+V(J,N)*ST
      CALL A1SUB(Y10,Y20, R(I,N)*VSO*VNO,0.0,R(J,N)*VS2*VN2,A1RUV)
45  CALL A2SUB(Y10,Y20, R(I,N)*VSO*VNO,0.0,R(J,N)*VS2*VN2,A2RUV)
      DVDY = (A1RUV + 2.*A2RUV*Y10) / (AR1*AVS)
      D = Y10*Y20*Y21
      DD = -Y21*(Y20+Y10)*DY + Y20*(Y21-Y10)*DY1 +Y10*(Y21+Y20)*DY2
50  EY2 = Y20SQ-Y10SQ
      ALOC = R(I,N)*U(I,N)
      ALOY = -ALOC*V(I,N)
      AL1C = AR1*AU1 - ALOC
      AL1Y = AR1*AU1*AV1 - ALOY
      AL2C = R(J,N)*U(J,N) -ALOC
55  AL2Y = R(J,N)*U(J,N)*V(J,N) -ALOY
      A1C = (AL1C*Y20SQ-AL2C*Y10SQ)/D
      A1Y = (AL1Y*Y20SQ-AL2Y*Y10SQ)/D
      A2C = (AL2C*Y10 - AL1C*Y20)/D
      A2Y = (AL2Y*Y10 - AL1Y*Y20)/D
60  F1 = Y10*(D-EY2*Y10/2.+Y10SQ*Y21/3.)
      F2 = Y10SQ*Y20*(Y20/2.-Y10/3.)
      FC1 = AL1C+2.*AL2C
      FC2 = Y20 -Y10/3.
      FC3 = AL1Y+2.*AL2Y
65  FC4 = Y10/2.-Y20/3.
      FC5 = AL1C-AL2C
      FC6 = Y10-Y20/3.
      FC7 = A1C/2.+Y20*A2C/3.
      FC8 = AL1Y-AL2Y
70  FC9 = A1Y/2.+Y20*A2Y/3.

```

```

F3C = -Y10QU*DRHU(J)/6.
F3C = F3C +(-AL1C*D+Y10SQ*(Y10*FC1/3.-Y20*AL1C))*DY
F3C = F3C -2.*AL2C*Y10SQ*Y10/3.*DY1
F3C = F3C +AL1C*Y10SQ*FC2*DY2
75 F3C = F3C -Y10SQ*(A1C/2.+Y10*A2C/3.)*DD
F3C = F3C +(AR1*AV1+R(I,N)*V(I,N))*D
F3Y = -Y10QU*DRUV(J)/6.
F3Y = F3Y +(-AL1Y*D +Y10SQ*(Y10*FC3/3.-Y20*AL1Y))*DY
F3Y = F3Y -2.*AL2Y*Y10SQ*Y10/3.*DY1
80 F3Y = F3Y +AL1Y*Y10SQ*FC2*DY2
F3Y = F3Y -Y10SQ*(A1Y/2.+Y10*A2Y/3.)*DD
F3Y = F3Y +(CK*AP1+AR1*AV1*AV1-CK*P(I,N)-R(I,N)*V(I,N)*V(I,N))*D
F4 = Y20*ID + Y20*(-EY2/2. + Y20*Y21/3.))
F5 = Y20QU/6.
85 F6C = -Y10*Y20SQ*FC4*DRHU(J)
F6C = F6C +(-AL2C*D+Y20SQ*(AL2C*Y10-AL1C*Y20+Y20*FC5/3.))*DY
F6C = F6C -Y20SQ*(AL2C*FC6*DY1-2.*Y20*AL1C/3.*DY2+FC7*DD)
F6C = F6C +(R(J,N)*V(J,N)+R(I,N)*V(I,N))*D
F6Y = -Y10*Y20SQ*FC4*DRUV(J)
90 F6Y = F6Y +(-AL2Y*D +Y20SQ*(AL2Y*Y10-AL1Y*Y20+Y20*FC8/3.))*DY
F6Y = F6Y -Y20SQ*(AL2Y*FC6*DY1 -2.*Y20*AL1Y/3.*DY2+FC9*DD)
F6Y = F6Y +(CK*(P(J,N)-P(I,N)) +R(J,N)*V(J,N)*V(J,N) -R(I,N)*
1 V(I,N)*V(I,N))*D
DEL = F1*F5 - F2*F4
95 E2 = F4*F3C - F1*F6C
400 E6 = F4*F3Y - F1*F6Y
ZVS(K) = DVDY/(AVS**2*AR1/(1.4*CK*AP1)-1.)
ZV1(K) = (E6-AV1*E2)/(AR1*AU1*DEL)
700 ZY1(K) = DY1
100 DVS = (ZVS(2) + 2.*(ZVS(3) + ZVS(4)) + ZVS(5))/6.
DV1 = (ZV1(2) + 2.*(ZV1(3) + ZV1(4)) + ZV1(5))/6.
DY1 = (ZY1(2) + 2.*(ZY1(3) + ZY1(4)) + ZY1(5))/6.
RETURN
END

```



```

      SUBROUTINE OUNS(M,I)
C
C      THIS SUBROUTINE PERFORMS A FLOW INTEGRATION STEP ON THE NEXT TO THE
C      OUTERMOST STREAMLINE
5
C      COMMON      C      ,CK      ,RS      ,FM      ,ALPHA
COMMON/ACOM/X      ,XA      ,VN      ,VS      ,H      ,DY
1      ,YO      ,PO      ,RO      ,UO      ,VO      ,RMO      ,DUO
2      ,V(2,10),P(2,10),R(2,10),U(2,10),V(2,10),RM(2,10),DU(2,10)
10     COMMON/OCOM/      DRHU(2),DPRU(2),DRUV(2)
      DIMENSION      ZU1(5),ZV1(5),ZY1(5), ZRHU(5),ZPRU(5),ZRUV(5)
      DATA ZU1,ZV1,ZY1/ 15*0.0 /
      Y20 = Y(I,1) -Y0*M
      Y20SQ = Y20*Y20
15     Y20QU = Y20SQ*Y20SQ
      DY = M*VO/UO
      ALOC = RO* UO
      ALOX = CK* PO + ALOC* UO
      ALOY = M*ALOC*VO
20     AL2C = 1. - ALOC
      AL2X = CK + 1. - ALOX
      AL2Y = - ALOY
      DO 700 K=2,5
      RN =(K-1)/2
25     RNH = RN/2.*H
      AY1 = Y(I,2)+ZY1(K-1)*RNH
      AU1 = U(I,2)+ZU1(K-1)*RNH
      AV1 = V(I,2)+ZV1(K-1)*RNH
      IF (C - AU1*AU1 - AV1*AV1) 100, 300, 300
30     100 X = -1.
      RETURN
300     AR1 = ((C - AU1*AU1 - AV1*AV1)/(C - 1.))*2.5
      AP1 = AR1**1.4
      Y10 = AY1 -Y0*M
35     Y21 = Y(I,1)-AY1
      Y10SQ = Y10*Y10
      DY1 = AV1/AU1
      D = Y10*Y20*Y21
      UD = -Y21*(Y20+Y10)*DY + Y20*(Y21-Y10)*DY1
40     EY2 = Y20SQ-Y10SQ
      AL1C = AR1*AU1 - ALOC
      AL1X = CK*AP1 + AR1*AU1*AU1 - ALOX
      AL1Y = AR1*AU1*AV1 - ALOY
45     A1C = (AL1C*Y20SQ-AL2C*Y10SQ)/D
      A1X = (AL1X*Y20SQ-AL2X*Y10SQ)/D
      A1Y = (AL1Y*Y20SQ-AL2Y*Y10SQ)/D
      A2C = (AL2C*Y10 - AL1C*Y20)/D
      A2X = (AL2X*Y10 - AL1X*Y20)/D
      A2Y = (AL2Y*Y10 - AL1Y*Y20)/D
50     F1 = Y10*(D-EY2*Y10/2.+Y10SQ*Y21/3.)
      F2 = Y10SQ*Y20*(Y20/2.-Y10/3.)
      FC1 = AL1C+2.*AL2C
      FC3 = AL1Y+2.*AL2Y
      FC5 = AL1C-AL2C
55     FC6 = Y10-Y20/3.
      FC7 = A1C/2.+Y20*A2C/3.
      FC8 = AL1Y-AL2Y
      FC9 = A1Y/2.+Y20*A2Y/3.
      FCA = AL1X+2.*AL2X
60     FCU = A1X/2.+Y10*A2X/3.
      FCC = AL1X-AL2X
      FCD = A1X/2.+Y20*A2X/3.
      F3C = (-AL1C*D+Y10SQ*(Y10*FC1/3.-Y20*AL1C))*DY
      F3C = F3C -2.*AL2C*Y10SQ*Y10/3.*DY1
65     F3C = F3C -Y10SQ*(A1C/2.+Y10*A2C/3.)*DD
      F3C = F3C +(A1*AV1-R0*VO*M)*D
      F3X = (-AL1X*D+Y10SQ*(Y10*FCA/3.-Y20*AL1X))*DY
      F3X = F3X -2.*AL2X*Y10SQ*Y10/3.*DY1
      F3X = F3X -Y10SQ*FC3*DD+AL1Y*D
70     F3Y = (-AL1Y*D+Y10SQ*(Y10*FC3/3.-Y20*AL1Y))*DY

```

```

F3Y = F3Y - 2.*AL2Y*Y10SQ*Y10/3.*DY1
F3Y = F3Y - Y10SQ*(A1Y/2.*Y10*A2Y/3.)*DD
F3Y = F3Y + (CK*AP1+AR1*AV1*AV1-CK*PO-RQ*VO*VO)*D
75 F4 = Y20*(D + Y20*(-EV2/2. + Y20*Y21/3.))
F5 = Y20QU/6.
F6C = (-AL2C*D+Y20SQ*(AL2C*Y10-AL1C*Y20+Y20*FC5/3.))*DY
F6C = F6C - Y20SQ*(AL2C*FC6*DY1+FC7*DD)
F6C = F6C - RQ*VO*M*D
80 F6X = (-AL2X*D+Y20SQ*(AL2X*Y10-AL1X*Y20+Y20*FC6/3.))*DY
F6X = F6X - Y20SQ*(AL2X*FC6*DY1+FC8*DD)+AL2Y*D
F6Y = (-AL2Y*D+Y20SQ*(AL2Y*Y10-AL1Y*Y20+Y20*FC8/3.))*DY
F6Y = F6Y - Y20SQ*(AL2Y*FC6*DY1+FC9*DD)
F6Y = F6Y + (CK*(1.-PO) - RQ*VO*VO)*D
85 DEL = F1*F5 - F2*F4
E2 = F4*F3C - F1*F6C
E4 = F4*F3X - F1*F6X
E6 = F4*F3Y - F1*F6Y
CD1 = DEL*(1.4*CK*AP1/AR1 - AU1*AU1)
90 ZU1(K) = ((CK*1.4*AP1/AR1 + AU1*AU1)*E2 - AU1*E4)/(AR1*CD1)
ZV1(K) = (E6 - AV1*E2)/(AR1*AU1*DEL)
ZRHU(K) = E2/DEL
ZPRU(K) = E4/DEL
ZRUU(K) = E6/DEL
700 ZY1(K) = DY1
95 DV1 = (ZV1(2) + 2.*(ZV1(3) + ZV1(4)) + ZV1(5))/6.
DY1 = (ZY1(2) + 2.*(ZY1(3) + ZY1(4)) + ZY1(5))/6.
JU(I,2) = (ZU1(2)+2.*(ZU1(3)+ZU1(4))+ZU1(5))/6.
DRHU(I) = (ZRHU(2)+2.*(ZRHU(3)+ZRHU(4))+ZRHU(5))/6.
100 DPRU(I) = (ZPRU(2)+2.*(ZPRU(3)+ZPRU(4))+ZPRU(5))/6.
DRUV(I) = (ZRUU(2)+2.*(ZRUU(3)+ZRUU(4))+ZRUU(5))/6.
U(I,2) = U(I,2) + H*DU(I,2)
V(I,2) = V(I,2) + H*DV1
Y(I,2) = Y(I,2) + H*DY1
VSQ = U(I,2)*U(I,2)+V(I,2)*V(I,2)
105 R(I,2) = ((C-VSQ)/(C-1.))**2.5
P(I,2) = R(I,2)**1.4
RM(I,2) = SQRT(VSQ*R(I,2)/(1.4*CK*P(I,2)))
RETURN
END

```

```

      SUBROUTINE INAS(M,I,N,IJ)
C
C   THIS SUBROUTINE PERFORMS A FLOW INTEGRATION STEP ON THE NTH STRIP
C   IN SOME CASES THIS SUBROUTINE PERFORMS A FLOW INTEGRATION STEP ON
5   C   THE STAGNATION STREAMLINE
C
      COMMON      C      ,CK      ,RS      ,FM      ,ALPHA
      COMMON/ACOM/X      ,XA      ,VN      ,VS      ,H      ,DY
10     1      ,Y0      ,P0      ,R0      ,U0      ,V0      ,RMO      ,DU0
      2      ,Y(2,10),P(2,10),R(2,10),U(2,10),V(2,10),RM(2,10),DU(2,10)
      COMMON/DCOM/CS      ,CZ      ,DV1      ,Z1      ,DQ1      ,RK
15     1      ,V00      ,ISKIP
      COMMON/OCOM/      DRHU(2),DPRU(2),DRUV(2)
      DIMENSION      ZU1(5),ZV1(5),ZY1(5), ZRHU(5),ZPRU(5),ZRUU(5)
      DIMENSION ZUO(5),ZVO(5)
      DATA ZUO,E1,E3,E5/8*0.0/
      DATA ZU1,ZV1,ZY1/ 15*0.0 /
      Y20 = Y(I,N-1)-Y0*M
      Y20SQ = Y20*Y20
      Y20GU = Y20SQ*Y20SQ
20     DO 700 K=2,5
      RN = (K-1)/2
      RNH = RN/2.*H
      IF(N.EQ.IJ) GO TO 40
25     AUO = UO
      AVO = VO*M
      ARO = RO
      APO = PO
      GO TO 220
30     40 AUO = UO+ZUO(K-1)*RNH
      GO TO (50,60,80),ISKIP
      50 AVO = VOO*EXP((1.-X)*RK)
      GO TO 90
      60 AVO = AUO*DY
35     GO TO 90
      90 CONTINUE
      AVO = VO +ZVO(K-1)*RNH
      90 CONTINUE
      IF(C-AUO*AUO-AVO*AVO) 100,100,180
40     100 X = -1.
      RETURN
      180 ARO = ((CZ-AUO*AUO-AVO*AVO)/(CS*(C-1.)))**2.5
      APO = ARO**1.4*CS
45     220 AY1 = Y(I,N) +ZY1(K-1)*RNH
      AU1 = U(I,N)+ZU1(K-1)*RNH
      AV1 = V(I,N)+ZV1(K-1)*RNH
      IF (C - AU1*AU1 - AV1*AV1) 100, 300, 300
50     300 AR1 = ((C - AU1*AU1 - AV1*AV1)/(C - 1.))**2.5
      AP1 = AR1**1.4
      Y10 = AY1-Y0*M
      Y21 = Y(I,N-1)-AY1
      Y10SQ = Y10*Y10
      Y10QU = Y10SQ*Y10SQ
      DY = AVO/AUO
55     DY1 = AV1/AU1
      DY2 = V(I,N-1)/U(I,N-1)
      D = Y10*Y20*Y21
      DD = -Y21*(Y20+Y10)*DY + Y20*(Y21-Y10)*DY1 +Y10*(Y21+Y20)*DY2
      EY2 = Y20SQ-Y10SQ
60     ALOC =ARO*AUO
      ALOX =CK*APO+ALOC*AUO
      ALOY = ALOC*AVO
      AL1C = AR1*AU1 - ALOC
      AL1X = CK*AP1 + AR1*AU1*AU1 - ALOX
65     AL1Y = AR1*AU1*AV1 - ALOY
      AL2C= R(I,N-1)*U(I,N-1) -ALOC
      AL2X= CK*P(I,N-1) +R(I,N-1)*U(I,N-1)*U(I,N-1) -ALOX
      AL2Y= R(I,N-1)*U(I,N-1)*V(I,N-1) -ALOY
      A1C = (AL1C*Y20SQ-AL2C*Y10SQ)/D
70     A1X = (AL1X*Y20SQ-AL2X*Y10SQ)/D

```

```

A1Y = (AL1Y*Y20SQ-AL2Y*Y10SQ)/D
A2C = (AL2C*Y10 - AL1C*Y20)/D
A2X = (AL2X*Y10 - AL1X*Y20)/D
A2Y = (AL2Y*Y10 - AL1Y*Y20)/D
75 F1 = Y10*(D-EY2*Y10/2.+Y10SQ*Y21/3.)
F2 = Y10SQ*Y20*(Y20/2.-Y10/3.)
FC1 = AL1C+2.*AL2C
FC2 = Y20 -Y10/3.
FC3 = AL1Y+2.*AL2Y
80 FC4 = Y10/2.-Y20/3.
FC5 = AL1C-AL2C
FC6 = Y10-Y20/3.
FC7 = A1C/2.+Y20*A2C/3.
FC8 = AL1Y-AL2Y
85 FC9 = A1Y/2.+Y20*A2Y/3.
FCA = AL1X+2.*AL2X
FCB = A1X/2.+Y10*A2X/3.
FCC = AL1X-AL2X
FCD = A1X/2.+Y20*A2X/3.
90 F3C = -Y10QU*DRHU(I)/6.
F3C = F3C +(-AL1C*D+Y10SQ*(Y10*FC1/3.-Y20*AL1C))*DY
F3C = F3C -2.*AL2C*Y10SQ*Y10/3.*DY1
F3C = F3C +AL1C*Y10SQ*FC2*DY2
F3C = F3C -Y10SQ*(A1C/2.+Y10*A2C/3.)*DD
95 F3C = F3C+(AR1*AV1-ARO*AV0)*D
F3X = -Y10QU*DPRU(I)/6.
F3X = F3X +(-AL1X*D+Y10SQ*(Y10*FCA/3.-Y20*AL1X))*DY
F3X = F3X -2.*AL2X*Y10SQ*Y10/3.*DY1
F3X = F3X +AL1X*Y10SQ*FC2*DY2
100 F3X = F3X -Y10SQ*FCB*DD+AL1Y*D
F3Y = -Y10QU*DRUV(I)/6.
F3Y = F3Y +(-AL1Y*D +Y10SQ*(Y10*FC3/3.-Y20*AL1Y))*DY
F3Y = F3Y -2.*AL2Y*Y10SQ*Y10/3.*DY1
F3Y = F3Y +AL1Y*Y10SQ*FC2*DY2
105 F3Y = F3Y -Y10SQ*(A1Y/2.+Y10*A2Y/3.)*DD
F3Y = F3Y+(CK*AP1+AR1*AV1-CK*AP0-ARO*AV0*AV0)*D
F4 = Y20*(D + Y20*(-EY2/2. + Y20*Y21/3.))
F5 = Y20QU/6.
F6C = -Y10*Y20SQ*FC4*DRHU(I)
110 F6C = F6C +(-AL2C*D+Y20SQ*(AL2C*Y10-AL1C*Y20+Y20*FC5/3.))*DY
F6C = F6C -Y20SQ*(AL2C*FC6*DY1-2.*Y20*AL1C/3.*DY2+FC7*DD)
F6C = F6C+(R(I,N-1)*V(I,N-1)-ARO*AV0)*D
F6X = -Y10*Y20SQ*FC4*DPRU(I)
F6X = F6X +(-AL2X*D+Y20SQ*(AL2X*Y10-AL1X*Y20+Y20*FCC/3.))*DY
115 F6X = F6X -Y20SQ*(AL2X*FC6*DY1-2.*Y20*AL1X/3.*DY2+FCD*DD)+AL2Y*D
F6Y = -Y10*Y20SQ*FC4*DRUV(I)
F6Y = F6Y +(-AL2Y*D +Y20SQ*(AL2Y*Y10-AL1Y*Y20+Y20*FC8/3.))*DY
F6Y = F6Y -Y20SQ*(AL2Y*FC6*DY1 -2.*Y20*AL1Y/3.*DY2+FC9*DD)
F6Y =F6Y+(CK*(P(I,N-1)-AP0)+R(I,N-1)*V(I,N-1)*V(I,N-1)
120 1-ARO*AV0*AV0)*D
DEL = F1*F5 - F2*F4
IF(N.LT.IJ.OR.IJ.LE.1) GO TO 400
380 E1 = F2*F6C-F5*F3C
E3 = F2*F6X-F5*F3X
125 E5 = F2*F6Y-F5*F3Y
ZV0(K) = (E5-AV0*E1)/(ARO*AU0*DEL)
CDO = DEL*(1.4*CK*AP0/ARO-AU0*AU0)
ZU0(K) = ((CK*1.4*AP0/ARO+AU0*AU0)*E1-AU0*E3)/(ARO*CDO)
400 E2 = F4*F3C - F1*F6C
E4 = F4*F3X - F1*F6X
130 E6 = F4*F3Y - F1*F6Y
CD1 = DEL*(1.4*CK*AP1/AR1 - AU1*AU1)
ZRHU(K) = E2/DEL
ZPRU(K) = E4/DEL
135 ZRUV(K) = E6/DEL
ZU1(K) = ((CK*1.4*AP1/AR1 +AU1*AU1)*E2 -AU1*E4)/(AR1*CD1)
ZV1(K) = (E6-AV1*E2)/(AR1*AU1*DEL)
700 ZY1(K) = JY1
140 DV1 = (ZV1(2) + 2.*(ZV1(3) + ZV1(4)) + ZV1(5))/6.
DY1 = (ZY1(2) + 2.*(ZY1(3) + ZY1(4)) + ZY1(5))/6.

```

```

DU(I,N)      = (ZU1(2)+2.*(ZU1(3)+ZU1(4))+ZU1(5))/6.
IF(IJ.LE.1) GO TO 704
IF(ISKIP.EQ.1) GO TO 710
145 704 DRHU(I) = (ZRHU(2)+2.*(ZRHU(3)+ZRHU(4))+ZRHU(5))/6.
      DPRU(I) = (ZPRU(2)+2.*(ZPRU(3)+ZPRU(4))+ZPRJ(5))/6.
      DRUV(I) = (ZRUV(2)+2.*(ZRUV(3)+ZRUV(4))+ZRUV(5))/6.
      IF(N.LT.IJ.OR.IJ.LE.1) GO TO 720
      DO 705 K=1,25
      XA = XA+H*0.05
150      CALL ARFL(XA,XB,YO,DY,DUH,I)
      IF(XB.GT.X) GO TO 710
      705 CONTINUE
      710 DUO = (ZUO(2)+2.*(ZUO(3)+ZUO(4))+ZUO(5))/6.
      UO = UO+H*DUO
155      GO TO (714,715,716),ISKIP
      714 VO = VOO*EXP((1.-X)*RK)
      YO = YO+H*VO/UO
      GO TO 718
      715 VO = UO*DY
160      GO TO 718
      716 DVO = (ZVO(2)+2.*(ZVO(3)+ZVO(4))+ZVO(5))/6.
      VO = VO+H*DVO
      VSQ = UO*UO+VO*VO
      UO = SQRT(VSQ/(1.+DY*DY))
165      VO = UO*DY
      718 VSQ = UO*UO+VO*VO
      RO = ((CZ-VSQ)/(CS*(C-1.)))**2.5
      PO = CS*RO**1.4
      RMO = SQRT(RO*VSQ/(1.4*CK*PO))
170 720 U(I,N) = U(I,N)+H*DU(I,N)
      V(I,N) = V(I,N)+H*DV1
      Y(I,N) = Y(I,N)+H*DY1
      VSQ = U(I,N)*U(I,N)+V(I,N)*V(I,N)
      R(I,N) = ((C-VSQ)/(C-1.))**2.5
175      P(I,N) = R(I,N)**1.4
      RM(I,N) = SQRT(VSQ*R(I,N)/(1.4*CK*P(I,N)))
      Q1 = SQRT(VSQ)
      QQ1 = (U(I,N)*DU(I,N)+V(I,N)*DV1)/Q1
      RETURN
180      END

```

```

      SUBROUTINE INBO(N,I)
C
C   THIS SUBROUTINE PERFORMS A FLOW INTEGRATION STEP ALONG THE
C   STAGNATION STREAMLINE
5
C
      COMMON      C      ,CK      ,RS      ,FM      ,ALPHA
      COMMON/ACOM/X      ,XA      ,VN      ,VS      ,H      ,DY
1      ,YO      ,PO      ,QO      ,UO      ,VO      ,RMO      ,DUO
10     2      ,Y(2,10),P(2,10),R(2,10),U(2,10),V(2,10),RM(2,10),DU(2,10)
      COMMON/CCOM/XB      ,YB      ,DYB      ,DDYB      ,DUB      ,PB
1      ,UB      ,RMB      ,DB      ,HS      ,CRA
      COMMON/OCOM/      ORHU(2),OPRU(2),ORUV(2)
      DIMENSION ZU1(5), ZV1(5), ZY1(5), ZVS(5), ZVN(5), ZB (5), ZUB(5)
15     DATA ZU1,ZV1,ZVS,ZVN,ZUB,ZB,ZY1/35*0.0/
      CT = 1./SQRT(1. + DYB**2)
      ST = DYB*CT
      RABO = ABS(1./((CT**3*DDYB)))
      DO 700 K = 2, 5
      RN=1.0
20     IF(K.EQ.2) RN=0.0
      IF(K.EQ.5) RN=2.0
      RNH = RN/2.*H
      AY1 = Y(I,N)+ZY1(K-1)*RNH
      AU1 = U(I,N)+ZU1(K-1)*RNH
25     AV1 = V(I,N)+ZV1(K-1)*RNH
      IF ( C - AU1*AU1 - AV1*AV1) 100, 300, 300
100    RMB = 2.0
      RETURN
300    AR1 = ((C - AU1*AU1 - AV1*AV1)/(C - 1.))**2.5
      AP1 = AR1**1.4
      AVS = VS +ZVS(K-1)*RNH*HS/H
      AVN = VN +ZVN(K-1)*RNH*HS/H
      AUO = AVS*CT - AVN*ST
      AVO = AVS*ST + AVN*CT
35     IF (C - AUO**2 - AVO**2) 100, 400, 400
400    ARO = ((C - AUO*AUO - AVO*AVO)/(C - 1.))**2.5
      APO = ARO**1.4
      AUB = UB +ZUB(K-1)*RNH*HS/H
      IF (C - AUB**2) 100, 500, 500
40     500    ARB = ((C - AUB*AUB      )/(C - 1.))**2.5
      APB = ARB**1.4
      B = DB +ZB(K-1)*RNH*HS/H
      RAB = RABO+B*CRA
      AYO = YB +B*CT
45     Y10 = AY1 -AYO
      Y20 = Y(I,N-1)-AYO
      Y21 = Y(I,N-1)-AY1
      DY = AVO/AUO
      DY1 = AV1/AU1
50     DY2 = V(I,N-1)/U(I,N-1)
      D = Y10*Y20*Y21
      Y10SQ = Y10*Y10
      Y20SQ = Y20*Y20
      Y10QU = Y10SQ*Y10SQ
55     Y20QU = Y20SQ*Y20SQ
      DD = -Y21*(Y20+Y10)*DY + Y20*(Y21-Y10)*DY1 +Y10*(Y21+Y20)*DY2
      EY2 = Y20SQ-Y10SQ
      ALOC = ARO*AUO
      ALOX = CK*APO + ALOC*AUO
60     ALOY = ALOC*AVO
      AL1C = AR1*AU1 - ALOC
      AL1X = CK*AP1 + AR1*AU1*AU1 - ALOX
      AL1Y = AR1*AU1*AV1 - ALOY
      AL2C = R(I,N-1)*U(I,N-1) -ALOC
65     AL2X = CK*P(I,N-1) +R(I,N-1)*U(I,N-1)*U(I,N-1) -ALOX
      AL2Y = R(I,N-1)*U(I,N-1)*V(I,N-1) -ALOY
      A1C = (AL1C*Y20SQ-AL2C*Y10SQ)/D
      A1X = (AL1X*Y20SQ-AL2X*Y10SQ)/D
      A1Y = (AL1Y*Y20SQ-AL2Y*Y10SQ)/D
70     A2C = (AL2C*Y10 - AL1C*Y20)/D

```

```

A2X = (AL2X*Y10 - AL1X*Y20)/D
A2Y = (AL2Y*Y10 - AL1Y*Y20)/D
F1 = Y10*(D-EY2*Y10/2.+Y10SQ*Y21/3.)
F2 = Y10SQ*Y20*(Y20/2.-Y10/3.)
75 FC1 = AL1C+2.*AL2C
FC2 = Y20 -Y10/3.
FC3 = AL1Y+2.*AL2Y
FC4 = Y10/2.-Y20/3.
FC5 = AL1C-AL2C
80 FC6 = Y10-Y20/3.
FC7 = A1C/2.+Y20*A2C/3.
FC8 = AL1Y-AL2Y
FC9 = A1Y/2.+Y20*A2Y/3.
FCA = AL1X+2.*AL2X
85 FCB = A1X/2.+Y10*A2X/3.
FCC = AL1X-AL2X
FCD = A1X/2.+Y20*A2X/3.
F3C = -Y10QU*DRHU(I)/6.
F3C = F3C +(-AL1C*D+Y10SQ*(Y10*FC1/3.-Y20*AL1C))*DY
90 F3C = F3C -2.*AL2C*Y10SQ*Y10/3.*DY1
F3C = F3C +AL1C*Y10SQ*FC2*DY2
F3C = F3C -Y10SQ*(A1C/2.+Y10*A2C/3.)*DD
F3C = F3C +(AR1*AV1-ARO*AVO)*D
F3X = -Y10QU*DRU(I)/6.
95 F3X = F3X +(-AL1X*D+Y10SQ*(Y10*FCA/3.-Y20*AL1X))*DY
F3X = F3X -2.*AL2X*Y10SQ*Y10/3.*DY1
F3X = F3X +AL1X*Y10SQ*FC2*DY2
F3X = F3X -Y10SQ*FC3*DU+AL1Y*D
F3Y = -Y10QU*DRUV(I)/6.
100 F3Y = F3Y +(-AL1Y*D +Y10SQ*(Y10*FC3/3.-Y20*AL1Y))*DY
F3Y = F3Y -2.*AL2Y*Y10SQ*Y10/3.*DY1
F3Y = F3Y +AL1Y*Y10SQ*FC2*DY2
F3Y = F3Y -Y10SQ*(A1Y/2.+Y10*A2Y/3.)*DD
F3Y = F3Y +(CK*AP1+AR1*AV1*AV1-CK*APO-ARO*AVO*AVO)*D
105 F4 = Y20*(D + Y20*(-EY2/2. + Y20*Y21/3.))
F5 = Y20QU/6.
F6C = -Y10*Y20SQ*FC4*DRHU(I)
F6C = F6C +(-AL2C*D+Y20SQ*(AL2C*Y10-AL1C*Y20+Y20*FC5/3.))*DY
F6C = F6C -Y20SQ*(AL2C*FC6*DY1-2.*Y20*AL1C/3.*DY2+FC7*DU)
110 F6C = F6C +(R(I,N-1)*V(I,N-1)-ARO*AVO)*D
F6X = -Y10*Y20SQ*FC4*DRU(I)
F6X = F6X +(-AL2X*D+Y20SQ*(AL2X*Y10-AL1X*Y20+Y20*FCC/3.))*DY
F6X = F6X -Y20SQ*(AL2X*FC5*DY1-2.*Y20*AL1X/3.*DY2+FC8*DU)+AL2Y*D
F6Y = -Y10*Y20SQ*FC4*DRUV(I)
115 F6Y = F6Y +(-AL2Y*D +Y20SQ*(AL2Y*Y10-AL1Y*Y20+Y20*FC8/3.))*DY
F6Y = F6Y -Y20SQ*(AL2Y*FC6*DY1 -2.*Y20*AL1Y/3.*DY2+FC9*DU)
F6Y = F6Y+(CK*(P(I,N-1)-APO)+R(I,N-1)*V(I,N-1)*V(I,N-1)
1-ARO*AVO*AVO)*D
DEL = F1*F5 - F2*F4
120 E1 = F2*F6C - F5*F3C
E2 = F4*F3C - F1*F6C
E3 = F2*F6X - F5*F3X
E4 = F4*F3X - F1*F6X
E5 = F2*F6Y - F5*F3Y
125 E6 = F4*F3Y - F1*F6Y
CUO = DEL*(1.4*CK*APO/ARO - AUO*AUO)
CO1 = DEL*(1.4*CK*AP1/AR1 - AU1*AU1)
ZY1(K) = DY1
ZU1(K) = ((CK*1.4*AP1/AR1 +AU1*AU1)*E2 -AU1*E4)/(AR1*CO1)
130 ZV1(K) = (E6-AV1*E2)/(AR1*AU1*DEL)
RABPB = RAB*B
ZR(K) = (1.+B/ RABPB )*AVN/AVS
DUQ = ((CK*1.4*APO/ARO + AUO*AUO)*E1 - AUO*E3)/(ARO*CO1)
DVO = (E5 - AVO*E1)/(ARO*AUO*DEL)
135 ZVS(K) = (DUQ*CT+DVO*ST)*CT-AVN/RAB
OMS = 1. - AVS*2*ARO/(1.4*CK*APO)
FF = (2./B +1./RAB)*CK*APB
FF = FF +ARB*AU3*AUS/RAB
FF = FF -(2./B +1./ RABPB )*CK*APO
140 FF = FF +ARO*AVS*AVS/ RA9PB

```

```

FF = FF - 2.* (1./B + 1./RABPB) * ARO * AVN * AVN
FF = FF / ARO / AVS
ZVN(K) = AVN / B * ZB(K) - OMS * AVN / AVS * ZVS(K) + FF
ZVN(K) = ZVN(K) / (1. - AVN * AVS * ARO / (1.4 * CK * APO))
145 DRVS = ARO * (OMS * ZVS(K) - ARO * AVS * AVN / (1.4 * CK * APO) * ZVN(K))
ZUB(K) = (ARB * AUB + ARO * AVS) * ZB(K) / B + DRVS
ZUB(K) = ZUB(K) / (ARB * (AUB * AUB / (1.4 * CK * APB / ARB) - 1.))
700 CONTINUE
DY1 = (ZY1(2) + 2.* (ZY1(3) + ZY1(4)) + ZY1(5)) / 6.
150 DU(I,N) = (ZU1(2) + 2.* (ZU1(3) + ZU1(4)) + ZU1(5)) / 6.
DV1 = (ZV1(2) + 2.* (ZV1(3) + ZV1(4)) + ZV1(5)) / 6.
DVS = (ZVS(2) + 2.* (ZVS(3) + ZVS(4)) + ZVS(5)) / 6.
DVN = (ZVN(2) + 2.* (ZVN(3) + ZVN(4)) + ZVN(5)) / 6.
DUB = (ZUB(2) + 2.* (ZUB(3) + ZUB(4)) + ZUB(5)) / 6.
155 DOB = (ZB(2) + 2.* (ZB(3) + ZB(4)) + ZB(5)) / 6.
Y(I,N) = Y(I,N) + H * DY1
U(I,N) = U(I,N) + H * DU(I,N)
V(I,N) = V(I,N) + H * DV1
VSQ = U(I,N) * U(I,N) + V(I,N) * V(I,N)
160 R(I,N) = ((C - VSQ) / (C - 1.)) ** 2.5
P(I,N) = R(I,N) ** 1.4
RH(I,N) = SQRT(VSQ * R(I,N) / (1.4 * CK * P(I,N)))
DB = DB + DOB * HS
VS = VS + DVS * HS
165 VN = VN + DVN * HS
UB = UB + DUB * HS
RB = ((C - UB * UB) / (C - 1.)) ** 2.5
PB = RB ** 1.4
RMB = UB / SQRT(1.4 * CK * PB / RB)
XA = XA + HS * CT
170 CALL ARFL (XA, XB, Y9, DYB, DDYB, I)
CT = 1. / SQRT(1. + DYB ** 2)
ST = CT * DYB
H = XB - DD * ST - X
175 X = X + H
YO = YB + DB * CT
UO = VS * CT - VN * ST
VO = VS * ST + VN * CT
RO = ((C - UO * UO - VO * VO) / (C - 1.)) ** 2.5
180 PO = RO ** 1.4
RMO = SQRT((UO * UO + VO * VO) * RO / (1.4 * CK * PO))
RETURN
END

```


APPENDIX G IGS PROGRAM LISTING

	BLOCK DATA CGRAF	CGRAF	2
	COMMON/COMMONXY/NXY1(6) ,NXY2(6)	COMMONXY	2
	COMMON/INPUT/	INPUT	2
5	1 ,LRUPS(6) ,LRSTG(6) ,LRAFU2(6) ,LRAFL2(6) ,LRAFU3(6) ,LRX00Q(6)	INPUT	3
	2 ,LRDIEQ(6) ,LRXSEQ(6) ,LRXAUP(6) ,LRCYDU(6) ,LRXALW(6) ,LRCYDL(6)	INPUT	4
	3 ,LRSLEQ(6) ,LRMACH(6) ,LRALFA(6) ,LRYIU(6) ,LRYIL(6) ,LRSTRT(6)	INPUT	5
	4 ,LRNN1(6) ,LRNA2(6) ,LRNN3(6) ,LRNN4(6) ,LRNN5(6) ,LRNN6(6)	INPUT	6
	5 ,NLGRNG(6) ,NPARAB(6)	INPUT	7
	COMMON/NOU/ NAIRFL(6)	NOU	2
10	1 ,LRDEEQ(6) ,LRYSOQ(6) ,LRYSEQ(6) ,LRDOEQ(6) ,LRRUEQ(6) ,LRUBEQ(6)	NOU	3
	2 ,LRID(6) ,LRPOEQ(6) ,LRNOGO(6) ,LRSUB(6) ,LRSUPR(6) ,LRFLOW(6)	NOU	4
	COMMON/NAXES/ NALL(6)	NAXES	2
	1 ,NMXB(6) ,NUPB(6) ,NOUDXB(6) ,NAF3B(6) ,NDWNB(6) ,NKTAB(6)	NAXES	3
	2 ,NX1B(6) ,NX2B(6) ,NYB(6) ,NM9(6) ,NMO1B(6) ,NMO2B(6)	NAXES	4
15	3 ,NDU1B(6) ,NDU2B(6) ,NDOQB(6) ,NPOB(6) ,NP1B(6) ,NPKTAB(6)	NAXES	5
	COMMON/NCHARS/NNEQ	NCHARS	2
	1 ,NYSOEQ(2) ,NXAEQ(2) ,NCYDEQ(2) ,NSLEQ(2) ,NDEEQ(2) ,NYSEQ(2)	NCHARS	3
	2 ,NDVOEQ(2) ,NRUEQ(2) ,NUBEQ(2) ,NID(2) ,NMACHQ(2) ,NALPHA(2)	NCHARS	4
	3 ,NYIEUEQ(2) ,NYILEQ(2) ,NPOEQ(2) ,FMTI ,FMTF	NCHARS	5
20	COMMON/NPRCD/ NCUPS1(6) ,NCUPS2(6) ,NCAFU2(6) ,NCAFL2(6) ,NCAFU3(6)	NPRCD	2
	1 ,NCDWN1(6) ,NCDWN2(6) ,NPUPS1(6) ,NPUPS2(6) ,NPAFU1(6) ,NPAFU2(6)	NPRCD	3
	2 ,NPAFU3(6) ,NPAFL1(6) ,NPAFL2(6) ,NPDWN1(6) ,NPDWN2(6) ,NUPS(6)	NPRCD	4
	3 ,NAF1(6) ,NAF2(6)	NPRCD	5
	C CGRAF	CGRAF	9
25	C THESE DATA STATEMENTS CONTAIN CHARACTERS USED IN THE CREATION OF THE	CGRAF	10
	C LIGHT REGISTERS AND MANY TEXT ENTITIES	CGRAF	11
	DATA NNEQ,NAEQ/ 10HNN= ,10HNA= /	CGRAF	12
	DATA NDVIEQ,NXSEQ,NYSOEQ,NXAEQ,NCYDEQ,NSLEQ,NXOOEQ/	CGRAF	13
30	1 10HVV00(I)= ,10H ,10HXS= ,10H ,	CGRAF	14
	2 10HYSO= ,10H ,10HXA= ,10H ,	CGRAF	15
	3 10HCYD= ,10H ,10HSHOCK L= ,10H ,	CGRAF	16
	4 10HXOO= ,10H /	CGRAF	17
	DATA NMACHQ,NALPHA,NYIEUEQ,NYILEQ/	CGRAF	18
35	1 10HMACH NO.= ,10H ,10HALPHA= ,10H ,	CGRAF	19
	2 10HVI(UPR)= ,10H ,10HVI(LWR)= ,10H /	CGRAF	20
	DATA NDEEQ,NYSEQ,NDVOEQ,NRUEQ,NUBEQ,NID,NPOEQ/	CGRAF	21
	1 10HDE= ,10H ,10HYS= ,10H ,	CGRAF	22
	2 10HVV00(F)= ,10H ,10HRBUB= ,10H ,	CGRAF	23
	3 10HUB= ,10H ,10HFLWS NOT ,10HMATCHED ,	CGRAF	24
40	4 10HPO= ,10H /	CGRAF	25
	DATA FMTI,FMTF/ 4H(I1) ,7H(F10.8) /	CGRAF	26
	C CGRAF	CGRAF	27
	C THIS DATA STATEMENT CONTAINS THE SIX INTEGER ARRAYS IDENTIFYING THE	CGRAF	28
	C TEXT ENTITIES DISPLAYING SPECIFIED OUTPUT VALUES IN THE LOWER RIGHT	CGRAF	29
45	C HAND CORNER OF THE SCREEN	CGRAF	30
	DATA LRX00Q ,LRDIEQ ,LRXSEQ ,LRXAUP ,LRCYDU ,LRXALW ,	CGRAF	31
	1 LRCYDL ,LRSLEQ ,LRMACH ,LRALFA ,LRYIU ,LRYIL ,	CGRAF	32
	2 LRNN1 ,LRNA2 ,LRNN3 ,LRNN4 ,LRNN5 ,LRNN6 ,	CGRAF	33
	3 LRUPS ,LRSTG ,LRAFU2 ,LRAFL2 ,LRAFU3 ,LRSTRT /	CGRAF	34
50	5 1,1,4*99 ,2,2,4*99 ,3,2,4*99 ,4,3,4*99 ,5,3,4*99 ,6,4,4*99 ,	CGRAF	35
	6 7,4,4*99 ,8,5,4*99 ,11,6,4*99 ,12,6,4*99 ,13,6,4*99 ,14,6,4*99 ,	CGRAF	36
	7 21,1,4*99 ,22,1,4*99 ,23,3,4*99 ,24,4,4*99 ,25,5,4*99 ,26,5*99 ,	CGRAF	37
	8 0,1,4*0 ,0,2,4*0 ,0,3,4*0 ,0,4,4*0 ,0,5,4*0 ,0,6,4*0 /	CGRAF	38
	DATA LRDEEQ ,LRYSOQ ,LRYSEQ ,LRDOEQ ,LRRUEQ ,LRUBEQ ,	CGRAF	39
55	1 LRID ,LRPOEQ /	CGRAF	40
	2 20,5*20 ,20,5*21 ,20,5*22 ,20,5*23 ,20,5*24 ,20,5*25 ,	CGRAF	41
	3 20,5*26 ,20,5*27 /	CGRAF	42
	C CGRAF	CGRAF	43
	C THIS DATA STATEMENT CONTAINS THE SIX INTEGER ARRAYS IDENTIFYING THE	CGRAF	44
60	C TEXT ENTITIES DISPLAYING BLINKING ASTERISKS IN THE LOWER LEFT HAND	CGRAF	45
	C CORNER OF THE SCREEN	CGRAF	46
	DATA NCUPS1 ,NCUPS2 ,NCAFU2 ,NCAFL2 ,NCAFU3 ,NCDWN1 ,	CGRAF	47
	1 NCDWN2 /	CGRAF	48
	2 30,5*30 ,30,5*31 ,30,5*32 ,30,5*33 ,30,5*34 ,30,5*35 ,	CGRAF	49
65	3 30,5*36 /	CGRAF	50
	C CGRAF	CGRAF	51
	C THIS DATA STATEMENT CONTAINS THE SIX INTEGER ARRAYS IDENTIFYING THE	CGRAF	52
	C TEXT ENTITIES DISPLAYING NONBLINKING ASTERISKS IN THE LOWER LEFT	CGRAF	53
	C HAND CORNER OF THE SCREEN	CGRAF	54

70	DATA NPUPS1 ,NPUPS2 ,NPAFU1 ,NPAFU2 ,NPAFU3 ,NPAFL1	CGRAF	55
	1 ,NPAFL2 ,NPDWN1 ,NPDWN2 ,NUPS ,NAF1 ,NAF2 /	CGRAF	56
	2 31,32,37,34,37,31 ,31,32,33,37,35,34 ,32,32,33,34,35,33	CGRAF	57
	3 ,6*32 ,6*33 ,32,32,33,34,35,36	CGRAF	58
	4 ,6*34 ,6*35 ,6*36	CGRAF	59
75	5 ,31,32,4*0 ,0,32,33,3*0 ,0,32,0,34,2*0 /	CGRAF	60
	C	CGRAF	61
	C TEXT ENTITIES DISPLAYING CHARACTERS WHICH IDENTIFY THE ABSCISSA AND	CGRAF	62
	C ORDINATE AXES OF THE GRAPHICAL OUTPUT	CGRAF	63
	DATA NX1B ,NX2B ,NYB ,NMB ,NMO1B ,NMO2B ,	CGRAF	64
80	1 NOU1B ,NOU2B ,NDOQB ,NPOB ,NP1B ,NPKTAB /	CGRAF	65
	2 40,41,42,43,44,45 ,40,3*47,44,45 ,40,41,4*47 ,	CGRAF	66
	3 40,41,4*48 ,40,46,42,3*46 ,40,41,4*49 ,	CGRAF	67
	4 40,2*46,43,2*46 ,40,3*46,44,46 ,40,3*47,44,47 ,	CGRAF	68
	5 40,4*48,45 ,40,4*49,45 ,49,41,42,43,44,45 /	CGRAF	69
85	DATA NMXB ,NUPB ,NDUQB ,NAF3B ,NDWNB ,NKTAB /	CGRAF	70
	1 40,0,42,3*0 ,40,41,4*0 ,40,2*0,43,2*0 ,	CGRAF	71
	2 40,3*0,44,0 ,40,4*0,45 ,0,41,42,43,44,45 /	CGRAF	72
	C	CGRAF	73
	C THIS DATA STATEMENT CONTAINS A SIX INTEGER ARRAY IDENTIFYING A POLY-	CGRAF	74
90	C LINE ENTITY WHICH DISPLAYS THE AIRFOIL SHAPE IN THE LOWER LEFT HAND	CGRAF	75
	C CORNER OF THE SCREEN	CGRAF	76
	DATA NAIRFL/6*19 /	CGRAF	77
	DATA LRSUPR ,LRSUB ,LRFLOW /2*19,4*1 ,2*19,4*2 ,2*19,4*0 /	CGRAF	78
	DATA NLGRNG ,NPARB /5*39,37 ,5*39,38 /	CGRAF	79
95	DATA LRNOGC /6*39 /	CGRAF	80
	C	CGRAF	81
	C THIS DATA STATEMENT CONTAINS THE SIX INTEGER ARRAYS IDENTIFYING THE	CGRAF	82
	C POLYLINE ENTITIES FOR GRAPHICAL OUTPUT	CGRAF	83
	DATA NXY1 ,NXY2 /6*60 ,6*61 /	CGRAF	84
100	DATA NALL/6*0/	CGRAF	85
	END	CGRAF	86

	OVERLAY(OVFILE,0,0)	LIEN	2
	PROGRAM LIEN(INPUT,OUTPUT,TAPE5=INPUT,TAPE6=OUTPUT)	LIEN	3
	COMMON/ISSCAL/IDSCAL	ISSCAL	2
	COMMON/NCON/ICON	NCON	2
5	COMMON/OUTCOM/	OUTCOM	2
	1 X1(160),Y1(160),Y2(160),NN1,NN2	OUTCOM	3
	COMMON/COMNXY/NXY1(6),NXY2(6)	COMNXY	2
	COMMON/ICNTRL/J,ICRIT(2),LL(2),IGO(2)	ICNTRL	2
	COMMON/INPUT/	INPUT	2
10	1 LRUPS(6),LRSTG(6),LRAFU2(6),LRAFL2(6),LRAFU3(6),LRX00Q(6)	INPUT	3
	2 ,LRDIEQ(6),LRXSEQ(6),LRXAUP(6),LRCYDU(6),LRXALW(6),LRCYDL(6)	INPUT	4
	3 ,LRSLEQ(6),LRMACH(6),LRALFA(6),LRYIU(6),LRYIL(6),LRSTRT(6)	INPUT	5
	4 ,LRNN1(6),LRNA2(6),LRNN3(6),LRNN4(6),LRNN5(6),LRNN6(6)	INPUT	6
	5 ,NLGRNG(6),NPARAB(6)	INPUT	7
15	COMMON/NOU/NAIRFL(6)	NOU	2
	1 ,LRDEEQ(6),LRYSEQ(6),LRDDEQ(6),LRRUEQ(6),LRUBEQ(6)	NOU	3
	2 ,LRID(6),LRPOEQ(6),LRNOGO(6),LRSUB(6),LRSUPR(6),LRFLOW(6)	NOU	4
	COMMON/NPRCD/NCUPS1(6),NCUPS2(6),NCAFU2(6),NCAFL2(6),NCAFU3(6)	NPRCD	2
	1 ,NCDWN1(6),NCDWN2(6),NPUPS1(6),NPUPS2(6),NPAFU1(6),NPAFU2(6)	NPRCD	3
20	2 ,NPAFU3(6),NPAFL1(6),NPAFL2(6),NPDWN1(6),NPDWN2(6),NUPS(6)	NPRCD	4
	3 ,NAF1(6),NAF2(6)	NPRCD	5
	COMMON/NAXES/NALL(6)	NAXES	2
	1 ,NMXB(6),NUPB(6),NDUDX9(6),NAF3B(6),NDWNB(6),NKTAB(6)	NAXES	3
	2 ,NX1B(6),NX2B(6),NYB(6),NMB(6),NMO1B(6),NMO2B(6)	NAXES	4
25	3 ,NDU1B(6),NDU2B(6),NDDQ9(6),NPOB(6),NP1B(6),NPKTAB(6)	NAXES	5
	COMMON/NCHARS/NNEQ,NAEQ,NX00EQ(2),NDVIEQ(2),NXSEQ(2)	NCHARS	2
	1 ,NYSOEQ(2),NXAEQ(2),NCYDEQ(2),NSLEQ(2),NDEEQ(2),NYSEQ(2)	NCHARS	3
	2 ,NDVOEQ(2),NRUEQ(2),NUBEQ(2),NID(2),NMACHQ(2),NALPHA(2)	NCHARS	4
	3 ,NTIUEQ(2),NYILEQ(2),NPOEQ(2),FMTI,FMTF	NCHARS	5
30	COMMON C,CK,RS,FM,ALPHA	COMMON	2
	COMMON/BCOM/XO,DV00,L	BCOM	2
	COMMON/ECOM/ASTAG(26),XSTAG(11),YSTAG(11),XAF(50),YAF(50,2)	ECOM	2
	COMMON/AINPUT/AIN(24),NNI(7),HI(6)	AINPUT	2
	COMMON/YUUSAV/NNN(3),YUV(126)	YUUSAV	2
35	COMMON/PTARFL/XX(40,2),YY(40,2),AM(40,2),CA,SA	PTARFL	2
	COMMON/COMPRS/XP(160,2),PP(160,2),NP(2)	COMPRS	2
	COMMON/RBUBCM/RBUB,UBINIT,IRBUB	RBUBCM	2
C		LIEN	22
C	INITIATE PROGRAM EXECUTION	LIEN	23
40	CALL GPEXE(4LNPUT)	LIEN	24
	END	LIEN	25

```

OVERLAY(1,0)
PROGRAM NPUT

C
C THIS PROGRAM READS INPUT
5 C
COMMON/NCON/ ICON
COMMON/AINPUT/AIN(24) ,NNI(7) ,HI(6)
COMMON/YUVSAV/NNN(3) ,YUV(126)
10 COMMON/PTARFL/XX(40,2) ,YY(40,2) ,AM(40,2) ,CA ,SA
COMMON C ,CK ,RS ,FM ,ALPHA
DIMENSION LABEL(7),NP(2)

C
C READ THE CONSOLE NUMBER AND THE LABEL CARD
READ(5,90) ICON,(LABEL(I),I=1,7)

15 C
C READ IN FLOW CONDITIONS
READ(5,100) FM,TC,ALPHA

C
C READ IN FLOW SOLUTION PARAMETERS
20 READ(5,210) (AIN(I),I=1,7)
READ(5,100) (AIN(I),I=8,15)
READ(5,100) (AIN(I),I=16,18)

C
C READ IN THE NUMBER OF STRIPS AND THE INTEGRATION STEP SIZE
25 READ(5,110) (NNI(I),I=1,6),(HI(I),I=1,6)
WRITE(6,400)
WRITE(6,330) (LABEL(I),I=1,7)
READ(5,140) NP(1),NP(2)
DO 20 J=1,2
30 NN = NP(J)
20 READ(5,150) (XX(I,J),YY(I,J),AM(I,J),I=1,NN)
NN1 = NP(1)
IF(NP(2).LT.NP(1)) NN1 = NP(2)
WRITE(6,240)
35 DO 30 I=1,NN1
30 WRITE(6,250) XX(I,1),YY(I,1),AM(I,1),XX(I,2),YY(I,2),AM(I,2)
NN1 = NN1+1
J = 1
IF(NP(2).GT.NP(1)) J=2
IF(NP(2).EQ.NP(1)) GO TO 80
40 NN2 = NP(J)
GO TO (40,60),J
40 DO 50 I=NN1,NN2
50 WRITE(6,260) XX(I,1),YY(I,1),AM(I,1)
GO TO 80
45 DO 70 I=NN1,NN2
70 WRITE(6,270) XX(I,2),YY(I,2),AM(I,2)
80 CA = COS(ALPHA/57.2957795)
SA = SIN(ALPHA/57.2957795)
50 CALL AETSKC(4LSTUP)
90 FORMAT(I2,8X,7A10)
100 FORMAT(8F10.6)
110 FORMAT(6I1,4X,7F10.6)
140 FORMAT(2I2)
55 210 FORMAT(10X,7F10.6)
150 FORMAT(3F20.15)
240 FORMAT(17X,8HX(UPPER),12X,8HY(UPPER),9X,12HDY/DX(UPPER),11X,
1 8HX(LOWER),12X,8HY(LOWER),9X,12HDY/DX(LOWER))
250 FORMAT(7X,6F20.12)
60 260 FORMAT(7X,3F20.12)
270 FORMAT(67X,3F20.12)
330 FOPPAT(4(/)32X,7A10,4(/))
400 FORMAT(1H1,4(/)7X,12(10H*****))
END

```

```

NPUT      2
NPUT      3
NPUT      4
NPUT      5
NPUT      6
NCON      2
AINPUT    2
YUVSAV    2
PTARFL    2
COMMON    2
NPUT      12
NPUT      13
NPUT      14
NPUT      15
NPUT      16
NPUT      17
NPUT      18
NPUT      19
NPUT      20
NPUT      21
NPUT      22
NPUT      23
NPUT      24
NPUT      25
NPUT      26
NPUT      27
NPUT      28
NPUT      29
NPUT      30
NPUT      31
NPUT      32
NPUT      33
NPUT      34
NPUT      35
NPUT      36
NPUT      37
NPUT      38
NPUT      39
NPUT      40
NPUT      41
NPUT      42
NPUT      43
NPUT      44
NPUT      45
NPUT      46
NPUT      47
NPUT      48
NPUT      49
NPUT      50
NPUT      51
NPUT      52
NPUT      53
NPUT      54
NPUT      55
NPUT      56
NPUT      57
NPUT      58
NPUT      59
NPUT      60
NPUT      61
NPUT      62
NPUT      63
NPUT      64
NPUT      65

```

	OVERLAY(2,0)	STUP	2
	PROGRAM STUP	STUP	3
		STUP	4
		STUP	5
5	C THIS PROGRAM SETS UP THE LIGHT REGISTERS, THE LIGHT BUTTONS, AND	STUP	6
	C MANY TEXT ENTITIES	NCON	2
	COMMON/NCON/ ICON	ISSCAL	2
	COMMON/ISSCAL/IDSCAL	INPUT	2
	COMMON/INPUT/	INPUT	3
10	1 LRUPS(6), LRSTG(6), LRAFU2(6), LRAFL2(6), LRAFU3(6), LRX00Q(6)	INPUT	4
	2 ,LRDIEQ(6), LRXSEQ(6), LRXAUP(6), LRCYDU(6), LRXALW(6), LRCYDL(6)	INPUT	5
	3 ,LRSLEQ(6), LRMACH(6), LRALFA(6), LRVIU(6), LRYIL(6), LRSTRT(6)	INPUT	6
	4 ,LRNN1(6), LRNA2(6), LRNN3(6), LRNN4(6), LRNN5(6), LRNN6(6)	INPUT	7
	5 ,NLGRNG(6), NPARA8(6)	NOUT	2
	COMMON/NOUT/ NAIRFL(6)	NOUT	3
15	1 ,LRDEEQ(6), LRYSEQ(6), LRYSEQ(6), LRDOEQ(6), LRRUEQ(6), LRUBEQ(6)	NOUT	4
	2 ,LRID(6), LRPOEQ(6), LRNOGO(6), LRSUB(6), LRSUPR(6), LRFLOW(6)	NPRCD	2
	COMMON/NPRCD/ NCUPS1(6), NCUPS2(6), NCAFU2(6), NCAFL2(6), NCAFU3(6)	NPRCD	3
	1 ,NCDWN1(6), NCDWN2(6), NPUPS1(6), NPUPS2(6), NPAFU1(6), NPAFU2(6)	NPRCD	4
20	2 ,NPAFU3(6), NPAFL1(6), NPAFL2(6), NPDOWN1(6), NPDOWN2(6), NUPS(6)	NPRCD	5
	3 ,NAF1(6), NAF2(6)	NAXES	2
	COMMON/NAXES/ NALL(6)	NAXES	3
	1 ,NMXB(6), NUPB(6), NDU0XB(6), NAF3B(6), NDHNB(6), NKTA8(6)	NAXES	4
	2 ,NX1B(6), NX2B(6), NVB(6), NMB(6), NMO1B(6), NMO2B(6)	NAXES	5
	3 ,NDU1B(6), NDU2B(6), NDDQB(6), NPOB(6), NP13(6), NPKTAB(6)	NCHARS	2
25	COMMON/NCHARS/ NNEQ	NCHARS	3
	1 ,NYSOEQ(2), NXAEQ(2), NCYDEQ(2), NSLEQ(2), NJEEQ(2), NYSEQ(2)	NCHARS	4
	2 ,NDVOEQ(2), NRUEQ(2), NUBEQ(2), NID(2), NMACHQ(2), NALPHA(2)	NCHARS	5
	3 ,NVIEUQ(2), NVILEQ(2), NPOEQ(2), FMTI, FMTF	AINPUT	2
30	COMMON/AINPUT/ AIN(24), NNI(7), HI(6)	YUUSAV	2
	COMMON/YUUSAV/ NNN(3), YUV(126)	COMMON	2
	COMMON C ,CK, RS, FM, ALPHA	STUP	17
	DIMENSION IXLR(2), IYLR(4), XLR(2),	STUP	18
35	1 YLR(4), XPRCD(6), YPRCD(3), XGRID(2), YGRID(4), ALIM1(4),	STUP	19
	2 USER1(4), BASE(4), X(60), Y(60), NSNCPB(2), NOGOB(3),	STUP	20
	3 IVEL1(2), IVEL2(2)	STUP	21
	DATA NSNCPB, NOGOB, ICOMP, NSTOP, NSUB, NSUPR, LRSTAR, IPRCD, IVEL1, IVEL2/	STUP	22
	1 10HSONIC POIN, 10HT REACHED, 10HINTEGRATIO, 10HN INCOMPLE,	STUP	23
	2 2HTE, 7HCOMPUTE, 4HSTOP, 8HSUBSONIC,	STUP	24
40	3 10HSUPERSONIC, 1H*, 7HPROCEED, 10HLAGRANGIAN,	STUP	25
	4 10H FUNCTION, 10HPARABOLIC, 10HFUNCTION /	STUP	26
	DATA NX, NY, NM, NMO, NDU0X, NDDQ, NPO, NP1 /	STUP	27
	1 1HX, 1HY, 1HM, 2HMO, 4HDOUX, 3HDDQ, 2HPO, 2HP1 /	STUP	28
	DATA IXLR, IYLR, XLR, YLR, XPRCD, YPRCD /	STUP	29
45	1 11, 36, -53, -49, -45, -41,	STUP	30
	2 10., 35., -56., -52., -48., -44.,	STUP	31
	3 -56., -50., -39., -37., -27., -2., -56., -50., -43. /	STUP	32
	DATA XGRID, YGRID, ALIM1, USER1, BASE /	STUP	33
	1 -54., 1., -42., -16., 12., 36., 3*(-57., -57., 57., 57.) /	STUP	34
	DATA IXCM, IYCM/35, -56/	STUP	35
50	C INITIALIZE SUBSCREEN AREA IDENTIFIER	STUP	36
	C IDSCAL = 1	STUP	37
	C	STUP	38
	C CREATE POINTS ON AIRFOIL FOR THE POLYLINE ENTITY NAIRFL	STUP	39
55	X(1) = -12.	STUP	40
	CALL ARFL(1.0, A, YY, 3, C, 2)	STUP	41
	Y(1) = -50. - YY*25.	STUP	42
	XX = 0.95	STUP	43
	DO 5 I=2, 29	STUP	44
60	CALL ARFL(XX, A, YY, B, C, 2)	STUP	45
	X(I) = -37. + XX*25.	STUP	46
	Y(I) = -50. - YY*25.	STUP	47
	DX = -.05	STUP	48
	IF(I.GE.19) DX = -.01	STUP	49
65	IF(I.GE.28) DX = -.005	STUP	50
	5 XX = XX+DX	STUP	51
	X(30) = -37.	STUP	52
	Y(30) = -50.	STUP	53
	XX = .005	STUP	54

70	DO 6 I=31,58	STUP	55
	CALL ARFL(XX,A,VV,B,C,1)	STUP	56
	X(I) = -37.*XX*25.	STUP	57
	V(I) = -50.*VV*25.	STUP	58
	DX = .005	STUP	59
75	IF(I.GE.32) DX = .01	STUP	60
	IF(I.GE.41) DX = .05	STUP	61
6	XX = XX*DX	STUP	62
	X(59) = -12.	STUP	63
	V(59) = V(1)	STUP	64
80	C	STUP	65
	C INITIALIZE GRAPHIC PAC FACILITIES	STUP	66
	CALL INTGP(6,DATAFL,3,510,1)	STUP	67
	C	STUP	68
	C INITIALIZE THE GRAPHICS CONSOLE NUMBER ICON	STUP	69
85	CALL INCON(ICON)	STUP	70
	C	STUP	71
	C DEFINE SUBSCREEN AREA 1 TO DEFINE THE ENTIRE SCREEN AREA	STUP	72
	CALL SCORS(BASE)	STUP	73
	CALL SSCAL(1,ALIM1,USER1)	STUP	74
90	CALL PLYLN(NAIRFL,1,X(1),Y(1),58)	STUP	75
	CALL ASCAL(1)	STUP	76
	CALL GENDF(NAIRFL,0)	STUP	77
	C	STUP	78
	C CREATE POINT ENTITIES IN THE LOWER RIGHT HAND CORNER OF THE SCREEN	STUP	79
95	CALL POINT(XLR(1),YLR(1),PTLR11)	STUP	80
	CALL POINT(XLR(1),YLR(2),PTLR12)	STUP	81
	CALL POINT(XLR(1),YLR(3),PTLR13)	STUP	82
	CALL POINT(XLR(1),YLR(4),PTLR14)	STUP	83
	CALL POINT(XLR(2),YLR(1),PTLR21)	STUP	84
100	CALL POINT(XLR(2),YLR(2),PTLR22)	STUP	85
	CALL POINT(XLR(2),YLR(3),PTLR23)	STUP	86
	CALL POINT(XLR(2),YLR(4),PTLR24)	STUP	87
	C	STUP	88
	C CREATE POINT ENTITIES IN THE LOWER LEFT HAND CORNER OF THE SCREEN	STUP	89
105	CALL POINT(XPRCD(2),YPRCD(2),ISTR22)	STUP	90
	CALL POINT(XPRCD(3),YPRCD(2),ISTR32)	STUP	91
	CALL POINT(XPRCD(4),YPRCD(3),ISTR43)	STUP	92
	CALL POINT(XPRCD(5),YPRCD(3),ISTR53)	STUP	93
	CALL POINT(XPRCD(4),YPRCD(1),ISTR41)	STUP	94
110	CALL POINT(XPRCD(5),YPRCD(1),ISTR51)	STUP	95
	CALL POINT(XPRCD(5),YPRCD(2),ISTR52)	STUP	96
	CALL POINT(XPRCD(6),YPRCD(2),ISTR62)	STUP	97
	C	STUP	98
	C CREATE POINT ENTITIES IN THE UPPER AREA OF THE SCREEN	STUP	99
115	CALL POINT(XGRID(2),YGRID(1),PGRD21)	STUP	100
	CALL POINT(XGRID(1),YGRID(2),PGRD12)	STUP	101
	CALL POINT(XGRID(1),YGRID(3),PGRD13)	STUP	102
	CALL POINT(XGRID(2),YGRID(3),PGRD23)	STUP	103
	CALL POINT(XGRID(1),YGRID(4),PGRD14)	STUP	104
120	C	STUP	105
	C CREATE LIGHT REGISTERS FOR THE LOWER RIGHT HAND CORNER OF THE SCREEN	STUP	106
	C WHICH CAN BE USED TO CHANGE INPUT VARIABLES	STUP	107
	CALL LITRG(IXLR(2),IYLR(2),NNEQ,3,21,FMTI)	STUP	108
125	CALL LITRG(IXLR(2),IYLR(2),NAEQ,3,22,FMTI)	STUP	109
	CALL LITRG(IXLR(2),IYLR(2),NNEQ,3,23,FMTI)	STUP	110
	CALL LITRG(IXLR(2),IYLR(2),NNEQ,3,24,FMTI)	STUP	111
	CALL LITRG(IXLR(2),IYLR(2),NNEQ,3,25,FMTI)	STUP	112
	CALL LITRG(IXLR(2),IYLR(2),NNEQ,3,26,FMTI)	STUP	113
	CALL LITRG(IXLR(2),IYLR(4),NXOSEQ,4,1,FMTF)	STUP	114
130	CALL LITRG(IXLR(2),IYLR(4),NOVIEQ,8,2,FMTF)	STUP	115
	CALL LITRG(IXLR(2),IYLR(3),NXSEQ,3,3,FMTF)	STUP	116
	CALL LITRG(IXLR(2),IYLR(4),NXAEQ,3,4,FMTF)	STUP	117
	CALL LITRG(IXLR(2),IYLR(3),NCYDEQ,4,5,FMTF)	STUP	118
	CALL LITRG(IXLR(2),IYLR(4),NXAEQ,3,6,FMTF)	STUP	119
135	CALL LITRG(IXLR(2),IYLR(3),NCYDEQ,4,7,FMTF)	STUP	120
	CALL LITRG(IXLR(2),IYLR(4),NSLEQ,8,8,FMTF)	STUP	121
	CALL LITRG(IXLR(2),IYLR(4),NMACHQ,9,11,FMTF)	STUP	122
	CALL LITRG(IXLR(2),IYLR(3),NALPHA,6,12,FMTF)	STUP	123
	CALL LITRG(IXLR(2),IYLR(2),NYIUEQ,8,13,FMTF)	STUP	124

140	CALL LITRG(IXLR(2),IYLR(1),NYILEQ,8,14,FMTF)	STUP	125
C		STUP	126
C	CREATE TEXT ENTITIES FOR THE LOWER RIGHT HAND CORNER OF THE SCREEN	STUP	127
C	WHICH CAN BE USED IN CONJUNCTION WITH THE LIGHT REGISTERS TO CHANGE	STUP	128
C	INPUT VARIABLES	STUP	129
145	CALL ENSHFT(NNEQ,3,NNI(1),FMTI)	STUP	130
	CALL TEXT(LRNN1,0,PTLR22,NNEQ,4,0,3,4RCVLI)	STUP	131
	CALL ENSHFT(NAEQ,3,NNI(2),FMTI)	STUP	132
	CALL TEXT(LRNA2,0,PTLR23,NAEQ,4,0,3,4RCVLI)	STUP	133
	CALL ENSHFT(NNEQ,3,NNI(3),FMTI)	STUP	134
150	CALL TEXT(LRNN3,0,PTLR22,NNEQ,4,0,3,4RCVLI)	STUP	135
	CALL ENSHFT(NNEQ,3,NNI(4),FMTI)	STUP	136
	CALL TEXT(LRNN4,0,PTLR22,NNEQ,4,0,3,4RCVLI)	STUP	137
	CALL ENSHFT(NNEQ,3,NNI(5),FMTI)	STUP	138
	CALL TEXT(LRNN5,0,PTLR22,NNEQ,4,0,3,4RCVLI)	STUP	139
155	CALL ENSHFT(NNEQ,3,NNI(6),FMTI)	STUP	140
	CALL TEXT(LRNN6,0,PTLR22,NNEQ,4,0,3,4RCVLI)	STUP	141
	CALL ENSHFT(NDVIEQ,8,AIN(1),FMTF)	STUP	142
	CALL TEXT(LRDIEQ,0,PTLR24,NDVIEQ,18,0,3,4RCVLR)	STUP	143
	CALL ENSHFT(NXSEQ,3,AIN(2),FMTF)	STUP	144
160	CALL TEXT(LRXSEQ,0,PTLR23,NXSEQ,13,0,3,4RCVLR)	STUP	145
	CALL ENSHFT(NX00EQ,4,AIN(8),FMTF)	STUP	146
	CALL TEXT(LRX00Q,0,PTLR24,NX00EQ,14,0,3,4RCVLR)	STUP	147
	CALL ENSHFT(NXAEQ,3,AIN(3),FMTF)	STUP	148
	CALL TEXT(LRXAUP,0,PTLR24,NXAEQ,13,0,3,4RCVLR)	STUP	149
	CALL TEXT(LRCYDU,0,PTLR23,NCYDEQ,14,0,3,4RCVLR)	STUP	151
	CALL ENSHFT(NXAEQ,3,AIN(5),FMTF)	STUP	152
	CALL TEXT(LRXALW,0,PTLR24,NXAEQ,13,0,3,4RCVLR)	STUP	153
	CALL ENSHFT(NCYDEQ,4,AIN(6),FMTF)	STUP	154
170	CALL TEXT(LRCYDL,0,PTLR23,NCYDEQ,14,0,3,4RCVLR)	STUP	155
	CALL ENSHFT(NSLEQ,8,AIN(7),FMTF)	STUP	156
	CALL TEXT(LRSLEQ,0,PTLR24,NSLEQ,18,0,3,4RCVLR)	STUP	157
	CALL ENSHFT(NMACHQ,9,FH,FMTF)	STUP	158
	CALL TEXT(LRMACH,0,PTLR24,NMACHQ,19,0,3,4RCVLR)	STUP	159
175	CALL ENSHFT(NALPHA,6,ALPHA,FMTF)	STUP	160
	CALL TEXT(LRALFA,0,PTLR23,NALPHA,16,0,3,4RCVLR)	STUP	161
	CALL ENSHFT(NYIEUEQ,8,AIN(11),FMTF)	STUP	162
	CALL TEXT(LRYIU,0,PTLR22,NYIEUEQ,18,0,3,4RCVLR)	STUP	163
	CALL ENSHFT(NYILEQ,8,AIN(12),FMTF)	STUP	164
180	CALL TEXT(LRVIL,0,PTLR21,NYILEQ,18,0,3,4RCVLR)	STUP	165
C		STUP	166
C	CREATE TEXT ENTITIES FOR THE LOWER RIGHT HAND CORNER OF THE SCREEN	STUP	167
C	WHICH DISPLAY OUTPUT INFORMATION	STUP	168
185	CALL TEXT(LRDEEQ,1,PTLR14,NDDEEQ,13)	STUP	169
	CALL TEXT(LRYSOQ,1,PTLR13,NYSOEQ,14)	STUP	170
	CALL TEXT(LRYSEQ,1,PTLR14,NVSEQ,13)	STUP	171
	CALL TEXT(LRDOEQ,1,PTLR13,NDVOEQ,18)	STUP	172
	CALL TEXT(LRRUEQ,1,PTLR14,NRUEQ,16)	STUP	173
	CALL TEXT(LRUBEQ,1,PTLR13,NUBEQ,13)	STUP	174
190	CALL TEXT(LRID ,1,PTLR13,NID,20)	STUP	175
	CALL TEXT(LRPOEQ,1,PTLR12,NPOEQ,13)	STUP	176
C		STUP	177
C	CREATE TEXT ENTITIES IN THE UPPER AREA OF THE SCREENWHICHLABEL THE	STUP	178
C	GRAPHIC DISPLAY	STUP	179
195	CALL TEXT(NX1B,1,PGRD21,NX,1)	STUP	180
	CALL TEXT(NX2B,1,PGRD23,NX,1)	STUP	181
	CALL TEXT(NYB ,1,PGRD14,NY,1)	STUP	182
	CALL TEXT(NMB ,1,PGRD23,NM,1)	STUP	183
	CALL TEXT(NMO1B,1,PGRD13,NMO,2)	STUP	184
200	CALL TEXT(NMO2B,1,PGRD12,NMO,2)	STUP	185
	CALL TEXT(NDU1B,1,PGRD13,NDUOX,4)	STUP	186
	CALL TEXT(NDU2B,1,PGRD12,NDUOX,4)	STUP	187
	CALL TEXT(NDDQB,1,PGRD14,NDDQ,3)	STUP	188
	CALL TEXT(NPOB,1,PGRD12,NPO,2)	STUP	189
205	CALL TEXT(NPKTAB,1,PGRD13,NPO,2)	STUP	190
	CALL TEXT(NP1B,1,PGRD14,NP1,2)	STUP	191
C		STUP	192
C	CREATE TEXT ENTITIES IN THE LOWER LEFT HAND CORNER OF THE SCREEN	STUP	193
C	WHICH DISPLAY ASTERISKS INDICATING NEXT PROGRAM STEP	STUP	194

210	CALL TEXT (NPUPS1,0,ISTR22,LRSTAR,1,0,3,4RSTRT)	STUP	195
	CALL TEXT (NPUPS2,0,ISTR32,LRSTAR,1,0,3,4RPRP2)	STUP	196
	CALL TEXT (NPAFU1,0,ISTR43,LRSTAR,1,0,3,4RAFU1)	STUP	197
	CALL TEXT (NPAFU2,0,ISTR43,LRSTAR,1,0,3,4RPRP3)	STUP	198
	CALL TEXT (NPAFU3,0,ISTR53,LRSTAR,1,0,3,4RPRP5)	STUP	199
215	CALL TEXT (NPAFL1,0,ISTR41,LRSTAR,1,0,3,4RAFL1)	STUP	200
	CALL TEXT (NPAFL2,0,ISTR51,LRSTAR,1,0,3,4RPRP4)	STUP	201
	CALL TEXT (NPDOWN1,0,ISTR62,LRSTAR,1,0,3,4RPRP6)	STUP	202
	CALL TEXT (NPDOWN2,0,ISTR52,LRSTAR,1,0,3,4RDWN2)	STUP	203
	C	STUP	204
220	C CREATE TEXT ENTITIES IN THE LOWER LEFT HAND CORNER OF THE SCREEN	STUP	205
	C WHICH DISPLAY BLINKING ASTERISKS INDICATING THE CURRENT PROGRAM STEP	STUP	206
	CALL TEXT (NCUPS1,1,ISTR22,LRSTAR,1,1,3)	STUP	207
	CALL TEXT (NCUPS2,1,ISTR32,LRSTAR,1,1,3)	STUP	208
	CALL TEXT (NCAFU2,1,ISTR43,LRSTAR,1,1,3)	STUP	209
225	CALL TEXT (NCAFL2,1,ISTR51,LRSTAR,1,1,3)	STUP	210
	CALL TEXT (NCAFU3,1,ISTR53,LRSTAR,1,1,3)	STUP	211
	CALL TEXT (NCDWN1,1,ISTR62,LRSTAR,1,1,3)	STUP	212
	CALL TEXT (NCDWN2,1,ISTR52,LRSTAR,1,1,3)	STUP	213
	CALL POINT (10.,0.,PTGRF2)	STUP	214
230	CALL TEXT (LRN0G0,1,PTGRF2,N0G0B,22)	STUP	215
	CALL TEXT (LRSUB,0,PTLR24,NSU3,8,0,3,4RPRP4)	STUP	216
	CALL TEXT (LRSUPR,0,PTLR23,NSUPR,10,0,3,4RPRP3)	STUP	217
	CALL TEXT (NLGRNG,0,PTLR22,IVEL1,19,0,3,4RCHGV)	STUP	218
	CALL TEXT (NPARAB,0,PTLR22,IVEL2,18,0,3,4RCHGV)	STUP	219
235	CALL LITBN (IXLR(1),IYLR(1),IPRCD,7,1,4RPRP1)	STUP	220
	C	STUP	221
	C CREATE LIGHT BUTTONS FOR COMPUTATION OF THE CURRENT PROGRAM STEP	STUP	222
	CALL LITBN (IXCH,IYCH,ICOMP,7,2,4RUPS1)	STUP	223
	CALL LITBN (IXCH,IYCH,ICOMP,7,3,4RUPS2)	STUP	224
240	CALL LITBN (IXCH,IYCH,ICOMP,7,4,4RAFU2)	STUP	225
	CALL LITBN (IXCH,IYCH,ICOMP,7,5,4RAFL2)	STUP	226
	CALL LITBN (IXCH,IYCH,ICOMP,7,6,4RAFU3)	STUP	227
	CALL LITBN (IXCH,IYCH,ICOMP,7,7,4RDWN1)	STUP	228
	CALL LITBN (-56,-56,NSTOP,4,20,4RSTOP)	STUP	229
245	C	STUP	230
	C ENABLE ALL TEXT AND POLYLINE ENTITIES	STUP	231
	CALL ENGDS (1,NALL)	STUP	232
	CALL AETSKC (*LSTRT)	STUP	233
	END	STUP	234

	OVERLAY(3,8)	STRT	2
	PROGRAM STRT	STRT	3
		STRT	4
		STRT	5
5	C THIS PROGRAM DISPLAYS THE FLOW VARIABLES	STRT	6
	C	INPUT	2
	COMMON/INPUT/	INPUT	3
	1 ,LRUPS(6) ,LRSTG(6) ,LRAFU2(6) ,LRAFL2(6) ,LRAFU3(6) ,LRXOOQ(6)	INPUT	4
	2 ,LRDIEQ(6) ,LRXSEQ(6) ,LRXAUP(6) ,LRCYDU(6) ,LRXALW(6) ,LRCYDL(6)	INPUT	5
10	3 ,LRSLEQ(6) ,LRMACH(6) ,LRALFA(6) ,LRYIU(6) ,LRYIL(6) ,LRSTRT(6)	INPUT	6
	4 ,LRNN1(6) ,LRNA2(6) ,LRNN3(6) ,LRNN4(6) ,LRNN5(6) ,LRNN6(6)	INPUT	7
	5 ,NLGRNG(6) ,NPARAB(6)	NOUT	2
	COMMON/NOUT/ NAIRFL(6)	NOUT	3
	1 ,LRDEEQ(6) ,LRYSOQ(6) ,LRYSEQ(6) ,LRDOEQ(6) ,LRRUEQ(6) ,LRUBEQ(6)	NOUT	4
15	2 ,LRID(6) ,LRPOEQ(6) ,LRNOGO(6) ,LRSUB(6) ,LRSUPR(6) ,LRFLOW(6)	NPRCD	2
	COMMON/NPRCD/ NCUPS1(6) ,NCUPS2(6) ,NCAFU2(6) ,NCAFL2(6) ,NCAFU3(6)	NPRCD	3
	1 ,NCDWN1(6) ,NCDWN2(6) ,NPUPS1(6) ,NPUPS2(6) ,NPAFU1(6) ,NPAFU2(6)	NPRCD	4
	2 ,NPAFU3(6) ,NPAFL1(6) ,NPAFL2(6) ,NPDOWN1(6) ,NPDOWN2(6) ,NUPS(6)	NPRCD	5
	3 ,NAF1(6) ,NAF2(6)	NAXES	2
20	COMMON/NAXES/ NALL(6)	NAXES	3
	1 ,NMXB(6) ,NUPB(6) ,NDUOXB(6) ,NAF3B(6) ,NDWNB(6) ,NKTAB(6)	NAXES	4
	2 ,NX1B(6) ,NX2B(6) ,NYB(6) ,NMB(6) ,NMO1B(6) ,NMO2B(6)	NAXES	5
	3 ,NDU1B(6) ,NDU2B(6) ,NDDQB(6) ,NPQB(6) ,NP1B(6) ,NPKTAB(6)	COMMON	2
	COMMON C ,CK ,RS ,FM ,ALPHA	ISSCAL	2
25	COMMON/ISSCAL/IDSCAL	STRT	13
	DIMENSION LBID(2)	STRT	14
	DATA LBID/1,20/	STRT	15
	CALL ASCAL(1)	STRT	16
	CALL ERASE(NALL)	STRT	17
30	CALL ERASG(IDSCAL)	STRT	18
	CALL ERASG(IDSCAL-1)	STRT	19
	CALL GENDF(NAIRFL,0)	STRT	20
	CALL ENLB(2,LBID)	STRT	21
	CALL GENDF(LRSTRT,0)	STRT	22
35	C WAIT FOR AN ATTENTION SOURCE	STRT	23
	C CALL WAITE(DUM,0,DUM,DUM)	STRT	24
	END	STRT	25

	OVERLAY(4,0)		PRP1	2
	PROGRAM PRP1		PRP1	3
C			PRP1	4
C	THIS PROGRAM DISPLAYS ITEMS NEEDED FOR PROGRAM UPS1		PRP1	5
5			PRP1	6
	COMMON/INPUT/		INPUT	2
	1 ,LRUPS(6) ,LRSTG(6) ,LRAF2(6) ,LRAFL2(6) ,LRAF3(6) ,LRX00Q(6)		INPUT	3
	2 ,LRDIEQ(6) ,LRXSEQ(6) ,LRXAUP(6) ,LRCYDU(6) ,LRXALW(6) ,LRCYDL(6)		INPUT	4
	3 ,LRSLEQ(6) ,LRMACH(6) ,LRALFA(6) ,LRYIU(6) ,LRYIL(6) ,LRSTRT(6)		INPUT	5
10	4 ,LRNN1(6) ,LRNA2(6) ,LRNN3(6) ,LRNN4(6) ,LRNN5(6) ,LRNN6(6)		INPUT	6
	5 ,MLGRNG(6) ,NPARAB(6)		INPUT	7
	COMMON/NOU/ NAIRFL(6)		NOU	2
	1 ,LRDEEQ(6) ,LRYSEQ(6) ,LRDOEQ(6) ,LRRUEQ(6) ,LRUBEQ(6)		NOU	3
	2 ,LRID(6) ,LRPOEQ(6) ,LRNOGO(6) ,LRSUB(6) ,LRSUPR(6) ,LRFLOW(6)		NOU	4
15	COMMON/NPRCD/ NCUPS1(6) ,NCUPS2(6) ,NCAFU2(6) ,NCAFL2(6) ,NCAFU3(6)		NPRCD	2
	1 ,NCDWN1(6) ,NCDWN2(6) ,NPUPS1(6) ,NPUPS2(6) ,NPAFU1(6) ,NPAFU2(6)		NPRCD	3
	2 ,NPAFU3(6) ,NPAFL1(6) ,NPAFL2(6) ,NPDOWN1(6) ,NPDOWN2(6) ,NUPS(6)		NPRCD	4
	3 ,NAF1(6) ,NAF2(6)		NPRCD	5
	COMMON/NAXES/ NALL(6)		NAXES	2
20	1 ,NMXB(6) ,NUPB(6) ,NDOUXB(6) ,NAF3B(6) ,NDWNB(6) ,NKTAB(6)		NAXES	3
	2 ,NX1B(6) ,NX2B(6) ,NYB(6) ,NMB(6) ,NMO1B(6) ,NMO2B(6)		NAXES	4
	3 ,NDU1B(6) ,NDU2B(6) ,NDDQB(6) ,NPOB(6) ,NP1B(6) ,NPXTAB(6)		NAXES	5
	COMMON C ,CK ,RS ,FM ,ALPHA		COMMON	2
	COMMON/AINPUT/AIN(24) ,NNI(7) ,HI(6)		AINPUT	2
25	COMMON/YUUSAV/NNN(3) ,YUV(126)		YUUSAV	2
	COMMON/PTARFL/XX(40,2) ,YY(40,2) ,AM(40,2) ,CA ,SA		PTARFL	2
	DIMENSION LBID(2)		PRP1	15
	DATA LBID/2,20/		PRP1	16
	CALL ASCAL(1)		PRP1	17
30	CALL ENLB(2,LBID)		PRP1	18
	CALL ERASE(LRSTRT)		PRP1	19
	CALL GENDF(NCUPS1,0)		PRP1	20
	CALL GENDF(NPUPS2,0)		PRP1	21
	CALL GENDF(LRUPS,0)		PRP1	22
35	CALL GENDF(NUPB,0)		PRP1	23
	WRITE(6,100) FM,ALPHA		PRP1	24
100	FORMAT(1H1///20X,9HMACH NO.=,F10.6,16H ALPHA=,F10.6)		PRP1	25
	CALL WAITE(DUM,0,DUM,DUM)		PRP1	26
	END		PRP1	27

	OVERLAY(5,0)	UPS1	2
	PROGRAM UPS1	UPS1	3
C		UPS1	4
C	THIS PROGRAM DISPLAYS OUTPUT FROM SUBROUTINE UPSTRM	UPS1	5
5		UPS1	6
	COMMON/OUTCOM/	OUTCOM	2
	1 X1(160) ,Y1(160) ,Y2(160) ,NN1 ,NN2	OUTCOM	3
	COMMON/COMNXY/NXY1(6) ,NXY2(6)	COMNXY	2
	COMMON/INPUT/	INPUT	2
10	1 LRUPS(6) ,LRSTG(6) ,LRAFU2(6) ,LRAFL2(6) ,LRAFU3(6) ,LRX00Q(6)	INPUT	3
	2 ,LRDIEQ(6) ,LRXSEQ(6) ,LRXAUP(6) ,LRCYDU(6) ,LRXALW(6) ,LRCYDL(6)	INPUT	4
	3 ,LRSLEQ(6) ,LRMACH(6) ,LRALFA(6) ,LRYIU(6) ,LRYIL(6) ,LRSTRT(6)	INPUT	5
	4 ,LRNN1(6) ,LRNA2(6) ,LRNN3(6) ,LRNN4(6) ,LRNN5(6) ,LRNN6(6)	INPUT	6
	5 ,NLGRNG(6) ,NPARAB(6)	INPUT	7
15	COMMON/NOUT/ NAIRFL(6)	NOUT	2
	1 ,LRDEEQ(6) ,LRYSEQ(6) ,LRYSEQ(6) ,LRDOEQ(6) ,LRRUEQ(6) ,LRUBEQ(6)	NOUT	3
	2 ,LRID(6) ,LRPOEQ(6) ,LRNOGO(6) ,LRSUB(6) ,LRSUPR(6) ,LRFLOW(6)	NOUT	4
	COMMON/NCHARS/NNEQ ,NAEQ ,NX00EQ(2) ,NDVIEQ(2) ,NXSEQ(2)	NCHARS	2
	1 ,NYSOEQ(2) ,NXAEQ(2) ,NCYDEQ(2) ,NSLEQ(2) ,NDEEQ(2) ,NYSEQ(2)	NCHARS	3
20	2 ,NDVDEQ(2) ,NRUEQ(2) ,NUBEQ(2) ,NID(2) ,NMACHQ(2) ,NALPHA(2)	NCHARS	4
	3 ,NYIUEQ(2) ,NYILEQ(2) ,NPDEQ(2) ,FMTI ,FMTF	NCHARS	5
	COMMON C ,CK ,RS ,FM ,ALPHA	COMMON	2
	COMMON/BCOM/ XO ,DV00 ,L	BCOM	2
	COMMON/ECOM/ASTAG(26) ,XSTAG(11) ,YSTAG(11) ,XAF(50) ,YAF(50,2)	ECOM	2
25	COMMON/AINPUT/AIN(24) ,NNI(7) ,HI(6)	AINPUT	2
	COMMON/YUUSAV/NNN(3) ,YUV(156)	YUUSAV	2
	COMMON/PTARFL/XX(40,2) ,YY(40,2) ,AM(40,2) ,CA ,SA	PTARFL	2
	COMMON/ISSCAL/IDSCAL	ISSCAL	2
30	DIMENSION X2TEMP(10) ,Y2TEMP(10) ,X2(10)	UPS1	19
	C = 1.+5./FM**2	UPS1	20
	CK = 1./(1.4*FM*FM)	UPS1	21
	CA = COS(ALPHA/57.2957795)	UPS1	22
	SA = SIN(ALPHA/57.2957795)	UPS1	23
35	CALL ASCAL(1)	UPS1	24
	CALL ERASG(IDSCAL)	UPS1	25
	CALL ERASG(IDSCAL-1)	UPS1	26
	CALL IOUPSTM	UPS1	27
	CALL ERASE(LRDEEQ)	UPS1	28
40	CALL ERASE(LRYSEQ)	UPS1	29
C		UPS1	30
C	DISPLAY THE OUTPUT VARIABLES DE AND YSO	UPS1	31
	CALL ENSHFT(NDEEQ,3,AIN(20),FMTF)	UPS1	32
	CALL MODFY(LRDEEQ,1,2,NDEEQ)	UPS1	33
	CALL GENDF(LRDEEQ,0)	UPS1	34
45	CALL ENSHFT(NYSOEQ,4,AIN(21),FMTF)	UPS1	35
	CALL MODFY(LRYSEQ,1,2,NYSOEQ)	UPS1	36
	CALL GENDF(LRYSEQ,0)	UPS1	37
C		UPS1	38
C	GRAPHICALLY DISPLAY DATA POINTS IN ARRAY X1-Y1	UPS1	39
50	CALL PLOTT2(0.,1.0,0.0,0.8,0.0,1.0,1)	UPS1	40
	IF(NN2.GT.1) GO TO 10	UPS1	41
C		UPS1	42
C	GRAPHICALLY DISPLAY DATA POINTS IN ARRAY X2-Y2	UPS1	43
	NN2 = 4	UPS1	44
	Y2(2) = 1.	UPS1	46
	Y2(3) = 0.	UPS1	47
	Y2(4) = 1.	UPS1	48
	Y2(11) = 0.	UPS1	49
60	Y2(12) = 1.	UPS1	50
	Y2(13) = 1.	UPS1	51
	Y2(14) = 0.	UPS1	52
10	DO 15 I=1,NN2	UPS1	53
	X2TEMP(I) = Y2(I)	UPS1	54
65	15 Y2TEMP(I) = Y2(I+10)	UPS1	55
	NSWITCH = NN2-1	UPS1	56
	DO 18 I=1,NN2	UPS1	57
	X2(I) = X2TEMP(I+NSWITCH)	UPS1	58
	Y2(I) = Y2TEMP(I+NSWITCH)	UPS1	59

70	18 NSWITCH = NSWITCH-2	UPS1	60
	Y2MAX = Y2(1)	UPS1	61
	DO 25 I=2,NN2	UPS1	62
	IF(Y2(I)-Y2MAX) 25,25,22	UPS1	63
	22 Y2MAX = Y2(I)	UPS1	64
75	25 CONTINUE	UPS1	65
	X2MIN = 0.0	UPS1	66
	Y2MIN = 0.0	UPS1	67
	X2MAX = X2(NN2)	UPS1	68
	CALL AREA2(Y2MIN,Y2MAX,X2MIN,X2MAX,2)	UPS1	69
80	NXY2(5) = 0	UPS1	70
	CALL DLETE(NXY2)	UPS1	71
	NXY2(5) = 61	UPS1	72
	CALL PLYLN(NXY2,1,Y2(1),X2(1),NN2-1)	UPS1	73
	CALL GENOF(NXY2,0)	UPS1	74
85	C	UPS1	75
	C WAIT FOR AN ATTENTION SOURCE	UPS1	76
	CALL WAITE(DUM,0,DUM,DUM)	UPS1	77
	END	UPS1	78

	OVERLAY(6,0)	PRP2	2
	PROGRAM PRP2	PRP2	3
		PRP2	4
		PRP2	5
	THIS PROGRAM DISPLAYS ITEMS NEEDED FOR PROGRAM UPS2	COMNXY	2
5	COMMON/COMNXY/NXY1(6) ,NXY2(6)	INPUT	2
	COMMON/INPUT/	INPUT	3
	1 ,LRUPS(6) ,LRSTG(6) ,LRAFU2(6) ,LRAFL2(6) ,LRAFU3(6) ,LRX00Q(6)	INPUT	4
	2 ,LRDIEQ(6) ,LRXSEQ(6) ,LRXAUP(6) ,LRCYDU(6) ,LRXALW(6) ,LRCYDL(6)	INPUT	5
10	3 ,LRSLEQ(6) ,LRNACH(6) ,LRALFA(6) ,LRYIU(6) ,LRYIL(6) ,LRSTRT(6)	INPUT	6
	4 ,LRNN1(6) ,LRNA2(6) ,LRNN3(6) ,LRNN4(6) ,LRNN5(6) ,LRNN6(6)	INPUT	7
	5 ,NLGRNG(6) ,NPARAB(6)	NOUT	2
	COMMON/NOUT/ NAIRFL(6)	NOUT	3
	1 ,LRDEEQ(6) ,LRYSEQ(6) ,LRDOEQ(6) ,LRRUEQ(6) ,LRUBEQ(6)	NOUT	4
15	2 ,LRID(6) ,LRPOEQ(6) ,LRN0G0(6) ,LRSUB(6) ,LRSUPR(6) ,LRFLOW(6)	NAXES	2
	COMMON/NAXES/ NALL(6)	NAXES	3
	1 ,NMXB(6) ,NUPB(6) ,NDOUXB(6) ,NAF3B(6) ,NDWNB(6) ,NKTAB(6)	NAXES	4
	2 ,NX1B(6) ,NX2B(6) ,NYB(6) ,NMB(6) ,NMO1B(6) ,NMO2B(6)	NAXES	5
	3 ,NDU1B(6) ,NDU2B(6) ,NDDQB(6) ,NPOB(6) ,NP1B(6) ,NPKTAB(6)	NPRCO	2
20	COMMON/NPRCO/ NCUPS1(6) ,NCUPS2(6) ,NCAFU2(6) ,NCAFL2(6) ,NCAFU3(6)	NPRCO	3
	1 ,NCDWN1(6) ,NCDWN2(6) ,NPUPS1(6) ,NPUPS2(6) ,NPAFU1(6) ,NPAFU2(6)	NPRCO	4
	2 ,NPAFU3(6) ,NPAFL1(6) ,NPAFL2(6) ,NPDOWN1(6) ,NPDOWN2(6) ,NUPS(6)	NPRCO	5
	3 ,NAF1(6) ,NAF2(6)	ICNTRL	2
	COMMON/ICNTRL/J ,ICRIT(2) ,LL(2) ,IGO(2)	ISSCAL	2
25	COMMON/ISSCAL/IDSCAL	PRP2	13
	DIMENSION LBID(2)	PRP2	14
	DATA LBID/3,20/	PRP2	15
	IGO(1) = 0	PRP2	16
	IGO(2) = 0	PRP2	17
30	NXY1(5) = 0	PRP2	18
	NXY1(6) = 0	PRP2	19
	CALL DELETE(NXY1)	PRP2	20
	NXY1(6)=60	PRP2	21
	CALL ASCAL(1)	PRP2	22
35	CALL ERASG(IDSCAL)	PRP2	23
	CALL ERASG(IDSCAL-1)	PRP2	24
	CALL ERASE(NALL)	PRP2	25
	CALL ENLB(2,LBID)	PRP2	26
	CALL GENDF(NAIRFL,0)	PRP2	27
40	CALL GENDF(NCUPS2,0)	PRP2	28
	CALL GENDF(NAF2,0)	PRP2	29
	CALL GENDF(LRSTG,0)	PRP2	30
	CALL WAITE(DUM,0,DUM,DUM)	PRP2	31
	END		

	OVERLAY(7,0)	UPS2	2
	PROGRAM UPS2	UPS2	3
C		UPS2	4
C	THIS PROGRAM DISPLAYS OUTPUT FROM SUBROUTINE IOSTGNA	UPS2	5
5	COMMON/NOUT/ NAIRFL(6)	NOUT	2
	1 ,LRDEEQ(6),LRYSEQ(6),LRYSEQ(6),LRDOEQ(6),LRRUEQ(6),LRUBEQ(6)	NOUT	3
	2 ,LRID(6) ,LRPOEQ(6),LRNDO(6),LRSUB(6) ,LRSUPR(6),LRFLOW(6)	NOUT	4
	COMMON/NCHARS/ NNEQ ,NAEQ ,NXOSEQ(2),NDVIEQ(2),NXSEQ(2)	NCHARS	2
10	1 ,NYSOEQ(2),NXAEQ(2) ,NCYDEQ(2),NSLEQ(2) ,NDEEQ(2) ,NYSEQ(2)	NCHARS	3
	2 ,NDVOEQ(2),NRUEQ(2) ,NUBEQ(2) ,NID(2) ,NMACHQ(2),NALPHA(2)	NCHARS	4
	3 ,NYIEQ(2),NYILEQ(2),NPOEQ(2) ,FMTI ,FMTF	NCHARS	5
	COMMON/NPRCD/ NCUPS1(6),NCUPS2(6),NCAFU2(6),NCAFL2(6),NCAFU3(6)	NPRCD	2
	1 ,NCDWN1(6),NCDWN2(6),NPUPS1(6),NPUPS2(6),NPAFU1(6),NPAFU2(6)	NPRCD	3
	2 ,NPAFU3(6),NPAFL1(6),NPAFL2(6),NPDOWN1(6),NPDOWN2(6),NUPS(6)	NPRCD	4
15	3 ,NAF1(6) ,NAF2(6)	NPRCD	5
	COMMON C ,CK ,RS ,FM ,ALPHA	COMMON	2
	COMMON/BCOM/ XO ,DVOO ,L	BCOM	2
	COMMON/ECOM/ASTAG(26),XSTAG(11),YSTAG(11),XAF(50),YAF(50,2)	ECOM	2
20	COMMON/AINPUT/AIN(24) ,NNI(7) ,HI(6)	AINPUT	2
	COMMON/PTARFL/XX(40,2) ,YY(40,2) ,AM(40,2) ,CA ,SA	PTARFL	2
	DIMENSION XINF(2),YINF(2),XSTG(11),YSTG(11),XLOWER(50),YLOWER(50),	UPS2	14
	1XUPPER(50),YUPPER(50)	UPS2	15
	DIMENSION NXYUPR(6),NXYLWR(6),NXYSTG(6),NYOINF(6),NNNALL(6)	UPS2	16
	DATA NXYUPR,NXYLWR,NXYSTG,NYOINF,NNNALL/6*50,50,5*52,50,5*53,	UPS2	17
25	1 50,5*54,50,5*0/	UPS2	18
	CALL IOSTGNA	UPS2	19
	CALL ASCAL(1)	UPS2	20
	CALL DELETE(NNNALL)	UPS2	21
	CALL ERASE(LRDOEQ)	UPS2	22
30		UPS2	23
C	ERASE TEXT ENTITIES PREVIOUSLY DISPLAYED BY THIS PROGRAM	UPS2	24
C	CALL ERASE(LRYSEQ)	UPS2	25
	YSPYSO = -AIN(21)-AIN(22)	UPS2	26
	DE = AIN(20)	UPS2	27
35	YLWR = AMIN1(YAF(50,2),YSPYSO)	UPS2	28
C		UPS2	29
C	DETERMINE THE SCALING FACTORS FOR THE SCREEN DISPLAY	UPS2	30
	AMULTX = 114./((XAF(50) -XSTAG(1))	UPS2	31
	AMULTY = 100./((-YLWR)	UPS2	32
40	AMULT = AMULTX	UPS2	33
	IF(AMULTX.GT.AMULTY) AMULT = AMULTY	UPS2	34
	DE = AIN(20)	UPS2	35
C		UPS2	36
C	DETERMINE DATA POINTS FOR THE FIRST 3 PER CENT OF THE UPPER AND	UPS2	37
45	C LOWER SURFACES OF THE AIRFOIL	UPS2	38
	DO 10 I=1,50	UPS2	39
	YUPPER(I) = -40.+(YAF(I,1)-YLWR)*AMULT	UPS2	40
	IF(YUPPER(I).GT.57.) GO TO 15	UPS2	41
	XUPPER(I) = -57.+(XAF(I) +DE)*AMULT	UPS2	42
50	10 CONTINUE	UPS2	43
	I=51	UPS2	44
	15 CALL PLYLN(NXYUPR,1,XUPPER,YUPPER,I-2)	UPS2	45
	DO 20 I=1,50	UPS2	46
	XLOWER(I) = -57.+(XAF(I) +DE)*AMULT	UPS2	47
55	YLOWER(I) = -40.+(YAF(I,2)-YLWR)*AMULT	UPS2	48
	20 CONTINUE	UPS2	49
	CALL PLYLN(NXYLWR,1,XLOWER,YLOWER,49)	UPS2	50
C		UPS2	51
C	DISPLAY THE OUTPUT VARIABLES YS AND DVOOF	UPS2	52
60	CALL ENSHFT(NYSEQ,3,AIN(22),FMTF)	UPS2	53
	CALL MODFY(LRYSEQ,1,2,NYSEQ)	UPS2	54
	CALL GENDF(LRYSEQ,0)	UPS2	55
	CALL ENSHFT(NDVOEQ,8,ASTAG(4),FMTF)	UPS2	56
	CALL MODFY(LRDOEQ,1,2,NDVOEQ)	UPS2	57
65	CALL GENDF(LRDOEQ,0)	UPS2	58
C		UPS2	59
C	DETERMINE DATA POINTS FOR THE STAGNATION STREAMLINE	UPS2	60
	DO 25 I=1,11	UPS2	61
	XSTG(I) = -57.+(XSTAG(I)+DE)*AMULT	UPS2	62

70	YSTG(I) = -40.+(YSTAG(I)-YLWR)*AMULT	UPS2	63
25	CONTINUE	UPS2	64
	CALL PLYLN(NXYSTG,1,XSTG,YSTG,10)	UPS2	65
	XINF(1) = -57.	UPS2	66
	XINF(2) = XSTG(11)	UPS2	67
75	YINF(1) = -40.+(YSPYSO-YLWR)*AMULT	UPS2	68
	YINF(2) = YINF(1)	UPS2	69
	CALL PLYLN(NYOINF,1,XINF,YINF,1)	UPS2	70
	C	UPS2	71
	C DISPLAY AIRFOIL NOSE AND STAGNATION STREAMLINE	UPS2	72
80	CALL GENOF(NNNALL,0)	UPS2	73
	C	UPS2	74
	C WAIT FOR AN ATTENTION SOURCE	UPS2	75
	CALL WAITE(DUM,0,DUM,DUM)	UPS2	76
	END	UPS2	77

	OVERLAY(10,0)	AFU1	2
	PROGRAM AFU1	AFU1	3
C		AFU1	4
C	THIS PROGRAM DISPLAYS OUTPUT FROM SUBROUTINE IOUPRCT	AFU1	5
5		AFU1	6
	COMMON/ICNTRL/J ,ICRIT(2) ,LL(2) ,IGO(2)	ICNTRL	2
	COMMON/COMNXY/NXY1(6) ,NXY2(6)	COMNXY	2
	COMMON/INPUT/	INPUT	2
10	1 ,LRUPS(6) ,LRSTG(6) ,LRAFU2(6) ,LRAFL2(6) ,LRAFU3(6) ,LRX00Q(6)	INPUT	3
	2 ,LRDIEQ(6) ,LRXSEQ(6) ,LRXAUP(6) ,LRCYDU(6) ,LRXALW(6) ,LRCYDL(6)	INPUT	4
	3 ,LRSLEQ(6) ,LRMACH(6) ,LRALFA(6) ,LRYIU(6) ,LRYIL(6) ,LRSTRT(6)	INPUT	5
	4 ,LRNN1(6) ,LRNA2(6) ,LRNN3(6) ,LRNN4(6) ,LRNN5(6) ,LRNN6(6)	INPUT	6
	5 ,NLGRNG(6) ,NPARAB(6)	INPUT	7
	COMMON/NOU/ NAIRFL(6)	NOU	2
15	1 ,LRDEEQ(6) ,LRYSEQ(6) ,LRYSEQ(6) ,LRDOEQ(6) ,LRRUEQ(6) ,LRUBEQ(6)	NOU	3
	2 ,LRID(6) ,LRPOEQ(6) ,LRNOGO(6) ,LRSUB(6) ,LRSUPR(6) ,LRFLOW(6)	NOU	4
	COMMON/NAXES/ NALL(6)	NAXES	2
	1 ,NMXB(6) ,NUPB(6) ,NDUDXB(6) ,NAF3B(6) ,NDOWNB(6) ,NKTAB(6)	NAXES	3
	2 ,NX1B(6) ,NX2B(6) ,NYB(6) ,NMB(6) ,NMO1B(6) ,NMO2B(6)	NAXES	4
20	3 ,NDU1B(6) ,NDU2B(6) ,NDDQ9(6) ,NPOB(6) ,NP1B(6) ,NPKTAB(6)	NAXES	5
	COMMON C ,CK ,RS ,FM ,ALPHA	COMMON	2
	COMMON/AINPUT/AIN(24) ,NNI(7) ,HI(6)	AINPUT	2
	COMMON/YUVSAV/NNN(3) ,YUV(156)	YUVSAV	2
	COMMON/PTARFL/XX(40,2) ,YY(40,2) ,AM(40,2) ,CA ,SA	PTARFL	2
25	COMMON/NPRCD/ NCUPS1(6) ,NCUPS2(6) ,NCAFU2(6) ,NCAFL2(6) ,NCAFU3(6)	NPRCD	2
	1 ,NCDWN1(6) ,NCDWN2(6) ,NPUPS1(6) ,NPUPS2(6) ,NPAFU1(6) ,NPAFU2(6)	NPRCD	3
	2 ,NPAFU3(6) ,NPAFL1(6) ,NPAFL2(6) ,NPJWN1(6) ,NPJWN2(6) ,NUPS(6)	NPRCD	4
	3 ,NAF1(6) ,NAF2(6)	NPRCD	5
	COMMON/ISSCAL/IDSCAL	ISSCAL	2
30	NXY1(5) = 0	AFU1	18
	NXY1(6) = 0	AFU1	19
	CALL DELETE(NXY1)	AFU1	20
	NXY1(6) = 60	AFU1	21
	CALL ASCAL(1)	AFU1	22
35	CALL ERASG(IDSCAL)	AFU1	23
	CALL ERASG(IDSCAL-1)	AFU1	24
	CALL ERASE(NALL)	AFU1	25
	CALL ENLB(1,20)	AFU1	26
	CALL GENDF(NAIRFL,0)	AFU1	27
40	CALL GENDF(NUPS,0)	AFU1	28
	J=1	AFU1	29
	LL(J) = 1	AFU1	30
	CALL GENDF(NLGRNG,0)	AFU1	31
	CALL GENDF(LRFLOW,0)	AFU1	32
45	CALL GENDF(NMXB,0)	AFU1	33
	CALL IOUPRCT	AFU1	34
	CALL PLOTT1(J,0,0.06,0.0,1.0)	AFU1	35
C		AFU1	36
C	WAIT FOR AN ATTENTION SOURCE	AFU1	37
50	CALL WAITE(DUN,0,ID,DUM)	AFU1	38
	END	AFU1	39

	OVERLAY(11,0)	PRP3	2
	PROGRAM PRP3	PRP3	3
C		PRP3	4
C	THIS PROGRAM DISPLAYS ITEMS NEEDED FOR PROGRAM AFU2	PRP3	5
5		PRP3	6
	COMMON/COMNXY/NXY1(6) ,NXY2(6)	COMNXY	2
	COMMON/ICNTRL/J ,ICRIT(2) ,LL(2) ,IGO(2)	ICNTRL	2
	COMMON/INPUT/	INPUT	2
	1 LRUPS(6) ,LRSTG(6) ,LRAFU2(6) ,LRAFL2(6) ,LRAFU3(6) ,LRX00Q(6)	INPUT	3
10	2 ,LRDIEQ(6) ,LRXSEQ(6) ,LRXAUP(6) ,LRCYDU(6) ,LRXALW(6) ,LRCYDL(6)	INPUT	4
	3 ,LRSLEQ(6) ,LRMACH(6) ,LRALFA(6) ,LRYIU(6) ,LRYIL(6) ,LRSTRT(6)	INPUT	5
	4 ,LRNN1(6) ,LRNA2(6) ,LRNN3(6) ,LRNN4(6) ,LRNN5(6) ,LRNN6(6)	INPUT	6
	5 ,NLGRNS(6) ,NPARAB(6)	INPUT	7
	COMMON/NOUT/ NAIRFL(6)	NOUT	2
15	1 ,LRDEEQ(6) ,LRYSEQ(6) ,LRYSEQ(6) ,LRDDEQ(6) ,LRRUEQ(6) ,LRUBEQ(6)	NOUT	3
	2 ,LRID(6) ,LRPOEQ(6) ,LRN0GO(6) ,LRSUR(6) ,LRSUPR(6) ,LRFLOW(6)	NOUT	4
	COMMON/NAXES/ NALL(6)	NAXES	2
	1 ,NMXB(6) ,NUPB(6) ,NDUDXB(6) ,NAF3B(6) ,NDWNB(6) ,NKTAB(6)	NAXES	3
	2 ,NX1B(6) ,NX2B(6) ,NYB(6) ,NMB(6) ,NMO1B(6) ,NMO2B(6)	NAXES	4
20	3 ,NDU1B(6) ,NDU2B(6) ,NDDQ3(6) ,NPOB(6) ,NP1B(6) ,NPXTAB(6)	NAXES	5
	COMMON/NPRCD/ NCUPS1(6) ,NCUPS2(6) ,NCAFU2(6) ,NCAFL2(6) ,NCAFU3(6)	NPRCD	2
	1 ,NCDWN1(6) ,NCDWN2(6) ,NPUPS1(6) ,NPUPS2(6) ,NPAFU1(6) ,NPAFU2(6)	NPRCD	3
	2 ,NPAFU3(6) ,NPAFL1(6) ,NPAFL2(6) ,NPDWN1(6) ,NPDWN2(6) ,NUPS(6)	NPRCD	4
	3 ,NAF1(6) ,NAF2(6)	NPRCD	5
25	DIMENSION ID(6)	PRP3	13
	DIMENSION LBID(2)	PRP3	14
	DATA LBID/4,20/	PRP3	15
	CALL BPNFO(ITRN,ID)	PRP3	16
	J=1	PRP3	17
30	ICRIT(J) = ID(3)	PRP3	18
C		PRP3	19
C	A VALUE OF ICRIT(J)=1 IS ALLOWED FOR THIS VARIABLE, OTHERWISE THE	PRP3	20
C	PROGRAM AWAITS ANOTHER ATTENTION SOURCE	PRP3	21
	IF(ICRIT(J).EQ.2) CALL WAITE(DUM,0,DUM,DUM)	PRP3	22
35	CALL ASCAL(1)	PRP3	23
	CALL ERASE(NALL)	PRP3	24
	CALL ENLB(2,LBID)	PRP3	25
	CALL GENDF(NAIRFL,0)	PRP3	26
	CALL GENDF(NCAFU2,0)	PRP3	27
40	CALL GENDF(NUPS,0)	PRP3	28
	CALL GENDF(LRAFU2,0)	PRP3	29
	CALL GENDF(NDUDXB,0)	PRP3	30
	CALL WAITE(DUM,0,DUM,DUM)	PRP3	31
	END	PRP3	32

	OVERLAY(12,0)	AFU2	2
	PROGRAM AFU2	AFU2	3
		AFU2	4
		AFU2	5
5	C THIS SUBROUTINE DISPLAYS OUTPUT FROM SUBROUTINE IOUPRIN	OUTCOM	2
	COMMON/OUTCOM/	OUTCOM	3
	1 X1(160) ,Y1(160) ,Y2(160) ,NN1 ,NN2	ICNTRL	2
	COMMON/ICNTRL/J	NOUT	2
	COMMON/NOUT/ NAIRFL(6)	NOUT	3
	1 ,LRDEEQ(6),LRYSEQ(6),LRDOEQ(6),LRRUEQ(6),LRUBEQ(6)	NOUT	4
10	2 ,LRID(6) ,LRPOEQ(6),LRNOGO(6),LRSUB(6) ,LRSUPR(6),LRFLOW(6)	NCHARS	2
	COMMON/NCHARS/NNEQ ,NAEQ ,NXOOEQ(2),NDVIEQ(2),NXSEQ(2)	NCHARS	3
	1 ,NYSOEQ(2),NXAEQ(2) ,NCYDEQ(2),NSLEQ(2) ,NDEEQ(2) ,NYSEQ(2)	NCHARS	4
	2 ,NDVOEQ(2),NRUEQ(2) ,NUBEQ(2) ,NID(2) ,NMACHQ(2),NALPHA(2)	NCHARS	5
	3 ,NVIEQ(2),NYILEQ(2),NPOEQ(2) ,FMTI ,FMTF	NPRCD	2
15	COMMON/NPRCD/ NCUPS1(6),NCUPS2(6),NCAFU2(6),NCAFL2(6),NCAFU3(6)	NPRCD	3
	1 ,NCDWN1(6),NCDWN2(6),NPUPS1(6),NPUPS2(6),NPAFU1(6),NPAFU2(6)	NPRCD	4
	2 ,NPAFU3(6),NPAFL1(6),NPAFL2(6),NPJWN1(6),NPJWN2(6),NUPS(6)	NPRCD	5
	3 ,NAF1(6) ,NAF2(6)	COMMON	2
20	COMMON C ,CK ,RS ,FM ,ALPHA	AINPUT	2
	COMMON/AINPUT/AIN(24) ,NNI(7) ,HI(6)	YUVSAV	2
	COMMON/YUVSAV/NNN(3) ,YUV(156)	PTARFL	2
	COMMON/PTARFL/XX(40,2) ,YY(40,2) ,AM(40,2) ,CA ,SA	RUBUCH	2
	COMMON/RUBUCH/RBUB ,UBINIT ,IRBUB	ISSCAL	2
25	COMMON/ISSCAL/IDSCAL	AFU2	17
	CALL ASCAL(1)	AFU2	18
	CALL ERASG(IDSCAL)	AFU2	19
	CALL ERASG(IDSCAL-1)	AFU2	20
	C ERASE TEXT ENTITIES PREVIOUSLY DISPLAYED BY THIS PROGRAM	AFU2	21
30	CALL ERASE(LRNOGO)	AFU2	22
	CALL ERASE(LRRUEQ)	AFU2	23
	CALL ERASE(LRID)	AFU2	24
	CALL ERASE(LRUBEQ)	AFU2	25
	IICRIT = ICRIT(J)	AFU2	26
35	CALL IOUPRIN(IICRIT)	AFU2	27
	C DEPENDING ON THE VALUE OF NN2, DISPLAY TEXT ENTITIES RELATING THE	AFU2	28
	C STATUS OF THE INTEGRATION PROCESS	AFU2	29
	IF(NN2.NE.1) CALL GENOF(LRNOGO,0)	AFU2	30
	IF(NN2.EQ.1) CALL GENOF(NPAFU3,0)	AFU2	31
40	C DISPLAY THE OUTPUT VALUES OF RBUB AND UB	AFU2	32
	CALL ENSHFT(NRUEQ,5,RBUB,FMTF)	AFU2	33
	CALL MODFY(LRRUEQ,1,2,NRUEQ)	AFU2	34
	CALL GENOF(LRRUEQ,0)	AFU2	35
45	IF(IRBUB.EQ.0) GO TO 4	AFU2	36
	IF(IRBUB.EQ.2) CALL GENOF(LRID,0)	AFU2	37
	GO TO 6	AFU2	38
	4 CALL ENSHFT(NUBEQ,3,UBINIT,FMTF)	AFU2	39
	CALL MODFY(LRUBEQ,1,2,NUBEQ)	AFU2	40
50	CALL GENOF(LRUBEQ,0)	AFU2	41
	6 CONTINUE	AFU2	42
	DO 10 I=1,NN1	AFU2	43
	10 Y1(I) = Y2(I)	AFU2	44
55	CALL PLOTT(7.0,0.04,0.0,20.0)	AFU2	45
	C WAIT FOR AN ATTENTION SOURCE	AFU2	46
	CALL WAITE(DUM,0,DUM,DUM)	AFU2	47
	END	AFU2	48
		AFU2	49
		AFU2	50

	OVERLAY(13,0)	AFL1	2
	PROGRAM AFL1	AFL1	3
	COMMON/ICNTRL/J	ICNTRL	2
	COMMON/COMNXY/NXY1(6)	COMNXY	2
5	COMMON/INPUT/	INPUT	2
	1 ,LRUPS(6) ,LRSTG(6) ,LRAFU2(6) ,LRAFL2(6) ,LRAFU3(6) ,LRX00Q(6)	INPUT	3
	2 ,LRDIEQ(6) ,LRXSEQ(6) ,LRXAUP(6) ,LRCYDU(6) ,LRXALW(6) ,LRCYDL(6)	INPUT	4
	3 ,LRSLEQ(6) ,LRMACH(6) ,LRALFA(6) ,LRYIU(6) ,LRYIL(6) ,LRSTRT(6)	INPUT	5
	4 ,LRNN1(6) ,LRNA2(6) ,LRNN3(6) ,LRNN4(6) ,LRNN5(6) ,LRNN6(6)	INPUT	6
10	5 ,NLGRNG(6) ,NPARA9(6)	INPUT	7
	COMMON/NOU/ NAIRFL(6)	NOU	2
	1 ,LRDEEQ(6) ,LRYSEQ(6) ,LRDOEQ(6) ,LR RUEQ(6) ,LRUBEQ(6)	NOU	3
	2 ,LRID(6) ,LRPOEQ(6) ,LRNOGO(6) ,LRSUB(6) ,LRSUPR(6) ,LRFLOW(6)	NOU	4
	COMMON/NAXES/ NALL(6)	NAXES	2
15	1 ,NMXB(6) ,NUPB(6) ,NDUOXB(6) ,NAF3B(6) ,NDOWNB(6) ,NKTAB(6)	NAXES	3
	2 ,NX1B(6) ,NX2B(6) ,NYB(6) ,NMB(6) ,NMO1B(6) ,NMO2B(6)	NAXES	4
	3 ,NDU1B(6) ,NDU2B(6) ,NDDQB(6) ,NPQB(6) ,NP1B(6) ,NPKTAB(6)	NAXES	5
	COMMON/NPRCD/ NCUPS1(6) ,NCUPS2(6) ,NCAFU2(6) ,NCAFL2(6) ,NCAFU3(6)	NPRCD	2
20	1 ,NCDWN1(6) ,NCDWN2(6) ,NPUPS1(6) ,NPUPS2(6) ,NPAFU1(6) ,NPAFU2(6)	NPRCD	3
	2 ,NPAFU3(6) ,NPAFL1(6) ,NPAFL2(6) ,NPDWN1(6) ,NPDWN2(6) ,NUPS(6)	NPRCD	4
	3 ,NAF1(6) ,NAF2(6)	NPRCD	5
	COMMON C ,CK ,RS ,FM ,ALPHA	COMMON	2
	COMMON/AINPUT/AIN(24) ,NNI(7) ,HI(6)	AINPUT	2
	COMMON/YUVSAV/NNN(3) ,YUV(156)	YUVSAV	2
25	COMMON/PTARFL/XX(40,2) ,YY(40,2) ,AM(40,2) ,CA ,SA	PTARFL	2
	COMMON/ISSCAL/IDSCAL	ISSCAL	2
	NXY1(5) = 0	AFL1	15
	NXY1(6) = 0	AFL1	16
30	CALL DLETE(NXY1)	AFL1	17
	NXY1(6) = 60	AFL1	18
	CALL ASCAL(1)	AFL1	19
	CALL ERASG(IDSCAL)	AFL1	20
	CALL ERASG(IDSCAL-1)	AFL1	21
	CALL ERASE(NALL)	AFL1	22
35	CALL ENLB(1,20)	AFL1	23
	CALL GENDF(NAIRFL,0)	AFL1	24
	CALL GENDF(NUPS,0)	AFL1	25
	J=2	AFL1	26
	LL(J) = 1	AFL1	27
40	CALL GENDF(NLGRNG,0)	AFL1	28
	CALL GENDF(LRFLOW,0)	AFL1	29
	CALL GENDF(NMxB,0)	AFL1	30
	CALL IOLWRC	AFL1	31
	CALL PLOTT1(0.0,0.06,0.0,1.00)	AFL1	32
45	C	AFL1	33
	C WAIT FOR AN ATTENTION SOURCE	AFL1	34
	CALL WAITE(DUN,0,ID,DUM)	AFL1	35
	END	AFL1	36

	OVERLAY(14,0)	PRP4	2
	PROGRAM PRP4	PRP4	3
		PRP4	4
		PRP4	5
5	C THIS PROGRAM DISPLAYS ITEMS NEEDED FOR PROGRAM AFL2	PRP4	6
	C	COMMONXY	2
	COMMON/COMNXY/NXY1(6) ,NXY2(6)	ICNTRL	2
	COMMON/ICNTRL/J ,ICRIT(2) ,LL(2) ,IGO(2)	INPUT	2
	COMMON/INPUT/	INPUT	3
10	1 ,LRUPS(6) ,LRSTG(6) ,LRAFU2(6) ,LRAFL2(6) ,LRAFU3(6) ,LRX00Q(6)	INPUT	4
	2 ,LRDEEQ(6) ,LRXSEQ(6) ,LRXAUP(6) ,LRCYDU(6) ,LRXALW(6) ,LRCYDL(6)	INPUT	5
	3 ,LRSLEQ(6) ,LRMACH(6) ,LRALFA(6) ,LRYIU(6) ,LRYIL(6) ,LRSTRT(6)	INPUT	6
	4 ,LRNN1(6) ,LRNA2(6) ,LRNN3(6) ,LRNN4(6) ,LRNN5(6) ,LRNN6(6)	INPUT	7
	5 ,NLGRNG(6) ,NPARA9(6)	NOUT	2
15	COMMON/NOUT/ NAIRFL(6)	NOUT	3
	1 ,LRDEEQ(6) ,LRYSEQ(6) ,LRDDEQ(6) ,LRRUEQ(6) ,LRUBEQ(6)	NOUT	4
	2 ,LRID(6) ,LRPOEQ(6) ,LRN0GO(6) ,LRSUB(6) ,LRSUPR(6) ,LRFLOW(6)	NAXES	2
	COMMON/NAXES/ NALL(5)	NAXES	3
	1 ,NMXB(6) ,NUPB(6) ,NDU0XB(6) ,NAF3B(6) ,NDWNB(6) ,NKTAB(6)	NAXES	4
	2 ,NX1B(6) ,NX2B(6) ,NYB(6) ,NMB(6) ,NMO1B(6) ,NMO2B(6)	NAXES	5
20	3 ,NDU1B(6) ,NDU2B(6) ,NDDQB(6) ,NPOB(6) ,NP1B(6) ,NPKTAB(6)	NPRCD	2
	COMMON/NPRCD/ NCUPS1(6) ,NCUPS2(6) ,NCAFU2(6) ,NCAFL2(6) ,NCAFU3(6)	NPRCD	3
	1 ,NCDWN1(6) ,NCDWN2(6) ,NPUPS1(6) ,NPUPS2(6) ,NPAFU1(6) ,NPAFU2(6)	NPRCD	4
	2 ,NPAFU3(6) ,NPAFL1(6) ,NPAFL2(6) ,NPDWN1(6) ,NPDWN2(6) ,NUPS(6)	NPRCD	5
	3 ,NAF1(6) ,NAF2(6)	PRP4	13
25	DIMENSION ID(6)	PRP4	14
	DIMENSION L3ID(2)	PRP4	15
	DATA L3ID/5,20/	PRP4	16
	CALL BPNFO(ITRN,ID)	PRP4	17
	J=2	PRP4	18
30	ICRIT(J) = ID(3)	PRP4	19
	C	PRP4	20
	C A VALUE OF ICRIT(J)=2 IS ALLOWED FOR THIS VARIABLE, OTHERWISE THE	PRP4	21
	C PROGRAM AWAITS ANOTHER ATTENTION SOURCE	PRP4	22
	IF(ICRIT(J).EQ.1) CALL WAITE(DUM,0,DUM,DUM)	PRP4	23
35	CALL ASCAL(1)	PRP4	24
	CALL ERASE(NALL)	PRP4	25
	CALL ENLB(2,L3ID)	PRP4	26
	CALL GENDF(NAIRFL,0)	PRP4	27
	CALL GENDF(NCAFL2,0)	PRP4	28
40	CALL GENDF(NUPS,0)	PRP4	29
	CALL GENDF(LRAFL2,0)	PRP4	30
	CALL GENDF(NMXP,0)	PRP4	31
	CALL WAITE(DUM,0,DUM,DUM)	PRP4	32
	END		

```

OVERLAY(15,0)
PROGRAM AFL2

C
C THIS PROGRAM DISPLAYS OUTPUT FROM SUBROUTINE IOLWRIN
C
COMMON/OUTCOM/
1  X1(160) ,Y1(160) ,Y2(160) ,NN1 ,NN2
COMMON/ICNTRL/J ,ICRIT(2) ,LL(2) ,IGO(2)
COMMON/NOUT/ NAIRFL(6)
10 1 ,LRDEEQ(6) ,LRYSEQ(6) ,LRDOEQ(6) ,LRRUEQ(6) ,LRUBEQ(6)
2 ,LRID(6) ,LRPOEQ(6) ,LRNOGO(6) ,LRSUB(6) ,LRSUPR(6) ,LRFLOW(6)
COMMON/NPRCD/ NCUPS1(6) ,NCUPS2(6) ,NCAFU2(6) ,NCAFL2(6) ,NCAFU3(6)
1 ,NCDWN1(6) ,NCDWN2(6) ,NPUPS1(6) ,NPUPS2(6) ,NPAFU1(6) ,NPAFU2(6)
2 ,NPAFU3(6) ,NPAFL1(6) ,NPAFL2(6) ,NPDOWN1(6) ,NPDOWN2(6) ,NUPS(6)
15 3 ,NAF1(6) ,NAF2(6)
COMMON/NCHARS/NNEQ ,NAEQ ,NXOSEQ(2) ,NDVIEQ(2) ,NXSEQ(2)
1 ,NYSOEQ(2) ,NXAEQ(2) ,NCYDEQ(2) ,NSLEQ(2) ,NDEEQ(2) ,NYSEQ(2)
2 ,NDVOEQ(2) ,NRUEQ(2) ,NUBEQ(2) ,NID(2) ,NMACHQ(2) ,NALPHA(2)
3 ,NYIEQ(2) ,NYIEQ(2) ,NPOEQ(2) ,FMTI ,FMTF
20 COMMON C ,CK ,RS ,FM ,ALPHA
COMMON/AINPUT/AIN(24) ,NNI(7) ,HI(5)
COMMON/YUVSAV/NNN(3) ,YUV(156)
COMMON/PTARFL/XX(40,2) ,YY(40,2) ,AM(40,2) ,CA ,SA
COMMON/RBUBCM/RBUB ,UBINIT ,IRBUB
25 COMMON/COMPRS/XP(160,2) ,PP(160,2) ,NP(2)
COMMON/ISSCAL/IDSCAL
CALL ASCAL(1)
CALL ERASG(IDSCAL)
CALL ERASG(IDSCAL-1)
30 CALL ERASE(LRNOGO)
C
C ERASE TEXT ENTITIES PREVIOUSLY DISPLAYED BY THIS PROGRAM
CALL ERASE(LRRUEQ)
CALL ERASE(LRID)
35 CALL ERASE(LRUBEQ)
CALL ERASE(LRPOEQ)
ICRIT = ICRIT(J)
L = LL(J)
CALL IOLWRIN(ICRIT,L)
40 IF(NN2.NE.1) CALL GENDF(LRNOGO,0)
C
C DISPLAY THE OUTPUT VALUES OF RBUB AND UB
CALL ENSHFT(NRUEQ,5,RBUB,FMTF)
CALL MODFY(LRRUEQ,1,2,NRUEQ)
45 CALL GENDF(LRRUEQ,0)
IF(IRBUB.EQ.0) GO TO 4
IF(IRBUB.EQ.2) CALL GENDF(LRID,0)
GO TO 5
4 CALL ENSHFT(NUBEQ,3,UBINIT,FMTF)
CALL MODFY(LRUBEQ,1,2,NUBEQ)
CALL GENDF(LRUBEQ,0)
50 6 CONTINUE
IF(NN2.EQ.3) GO TO 3
NN = NP(J)
55 C
C
C DEPENDING ON THE VALUE OF NN2, DISPLAY THE OUTPUT VALUE OF PO
CALL ENSHFT(NPOEQ,3,PP(NN,J),FMTF)
CALL MODFY(LRPOEQ,1,2,NPOEQ)
CALL GENDF(LRPOEQ,0)
60 C
C
C DEPENDING ON THE VALUE OF NN2 AND IGO(J), DISPLAY ASTERISKS
C INDICATING THE NEXT PROGRAM STEP
IF(NN2.EQ.1) IGO(J)=1
IF(NN2.EQ.1) CALL GENDF(NPAFU1,0)
65 IF(IGO(1).EQ.1.AND.IGO(2).EQ.1) CALL GENDF(NPDOWN1,0)
9 CALL PLOTT(0.0,1.0,0.0,1.0)
C
C WAIT FOR AN ATTENTION SOURCE
CALL WAITE(DUM,0,DUM,DUM)
70 END

```

```

AFL2      2
AFL2      3
AFL2      4
AFL2      5
AFL2      6
OUTCOM    2
OUTCOM    3
ICNTRL    2
NOUT      2
NOUT      3
NOUT      4
NPRCD     2
NPRCD     3
NPRCD     4
NPRCD     5
NCHARS    2
NCHARS    3
NCHARS    4
NCHARS    5
COMMON    2
AINPUT    2
YUVSAV    2
PTARFL    2
RBUBCM    2
COMPRS    2
ISSCAL    2
AFL2      19
AFL2      20
AFL2      21
AFL2      22
AFL2      23
AFL2      24
AFL2      25
AFL2      26
AFL2      27
AFL2      28
AFL2      29
AFL2      30
AFL2      31
AFL2      32
AFL2      33
AFL2      34
AFL2      35
AFL2      36
AFL2      37
AFL2      38
AFL2      39
AFL2      40
AFL2      41
AFL2      42
AFL2      43
AFL2      44
AFL2      45
AFL2      46
AFL2      47
AFL2      48
AFL2      49
AFL2      50
AFL2      51
AFL2      52
AFL2      53
AFL2      54
AFL2      55
AFL2      56
AFL2      57
AFL2      58
AFL2      59
AFL2      60
AFL2      61
AFL2      62

```

	OVERLAY(16,0)	PRP5	2
	PROGRAM PRP5	PRP5	3
		PRP5	4
		PRP5	5
		PRP5	6
		COMNXY	2
		ICNTRL	2
		INPUT	2
5	C THIS PROGRAM DISPLAYS ITEMS NEEDED FOR PROGRAM AFU3	INPUT	3
	C	INPUT	4
	C	INPUT	5
		INPUT	6
		INPUT	7
		NOUT	2
		NOUT	3
		NOUT	4
		NAXES	2
		NAXES	3
		NAXES	4
		NAXES	5
		NPRCD	2
		NPRCD	3
		NPRCD	4
		NPRCD	5
		PRP5	13
		PRP5	14
		PRP5	15
		PRP5	16
		PRP5	17
		PRP5	18
		PRP5	19
		PRP5	20
		PRP5	21
		PRP5	22
		PRP5	23
		PRP5	24
		PRP5	25
		PRP5	26
		PRP5	27

10	1	COMMON/COMNXY/NXY1(6) ,NXY2(6)
	2	COMMON/ICNTRL/J ,ICRIT(2) ,LL(2) ,IGO(2)
	3	COMMON/INPUT/
	4	1 ,LRUPS(6) ,LRSTG(6) ,LRAFU2(6) ,LRAFL2(6) ,LRAFU3(6) ,LRX00Q(6)
	5	2 ,LRDIEQ(6) ,LRXSEQ(6) ,LRXAUP(6) ,LRXYDU(6) ,LRXALW(6) ,LRXYDL(6)
	6	3 ,LRSLEQ(6) ,LRMACH(6) ,LRALFA(6) ,LRYIU(6) ,LXYIL(6) ,LRSTRT(6)
	7	4 ,LRNN1(6) ,LRNA2(6) ,LRNN3(6) ,LRNN4(6) ,LRNN5(6) ,LRNN6(6)
	8	5 ,NLGRNG(6) ,NPARAB(6)
	9	COMMON/NOUT/ NAIRFL(6)
15	1	1 ,LRDEEQ(6) ,LRYSEQ(6) ,LRDOEQ(6) ,LRRUEQ(6) ,LRUBEQ(6)
	2	2 ,LRID(6) ,LRPOEQ(6) ,LRNOGO(6) ,LRSUB(6) ,LRSUPR(6) ,LRFLOW(6)
	3	COMMON/NAXES/ NALL(6)
	4	1 ,NMXB(6) ,NUPB(6) ,NDUDXB(6) ,NAF3B(6) ,NDWNB(6) ,NKTAB(6)
	5	2 ,NX1B(6) ,NX2B(6) ,NYB(6) ,NMB(6) ,NMO1B(6) ,NMO2B(6)
20	3	3 ,NDU1B(6) ,NDU2B(6) ,NDUQ3(6) ,NPOB(6) ,NP1B(6) ,NPKTAB(6)
	4	COMMON/NPRCD/ NCUPS1(6) ,NCUPS2(6) ,NCAFU2(6) ,NCAFL2(6) ,NCAFU3(6)
	5	1 ,NCDWN1(6) ,NCDWN2(6) ,NPUPS1(6) ,NPUPS2(6) ,NPAFU1(6) ,NPAFU2(6)
	6	2 ,NPAFU3(6) ,NPAFL1(6) ,NPAFL2(6) ,NPDWN1(6) ,NPDWN2(6) ,NUPS(6)
	7	3 ,NAF1(6) ,NAF2(6)
25	8	DIMENSION LBID(2)
	9	DATA LBID/6,20/
	10	J = 1
	11	IGO(J) = 0
30	12	CALL ASCAL(1)
	13	CALL ERASE(NALL)
	14	CALL ENLB(2,LBID)
	15	CALL GENOF(NAIRFL,0)
	16	CALL GENOF(NCAFU3,0)
	17	CALL GENOF(NPAFU2,0)
35	18	CALL GENOF(NUPS,0)
	19	CALL GENOF(LRAFU3,0)
	20	CALL GENOF(NMXB,0)
	21	CALL WAITE(DUM,0,DUM,DUM)
	22	END

	OVERLAY(20,0)		PRP6	2
	PROGRAM PRP6		PRP6	3
C			PRP6	4
C	THIS PROGRAM DISPLAYS ITEMS NEEDED FOR PROGRAM DWN1		PRP6	5
C			PRP6	6
5	COMMON/ICNTRL/J ,ICRIT(2) ,LL(2) ,ISO(2)	ICNTRL	2	
	COMMON/OUTCOM/	OUTCOM	2	
	1 X1(160) ,Y1(160) ,Y2(160) ,NN1 ,NN2	OUTCOM	3	
	COMMON/INPUT/	INPUT	2	
10	1 LRUPS(6) ,LRSTG(6) ,LRAFU2(6) ,LRAFL2(6) ,LRAFU3(6) ,LRX00Q(6)	INPUT	3	
	2 ,LRDIEQ(6) ,LRXSEQ(6) ,LRXAUP(6) ,LRCYDU(6) ,LRXALW(6) ,LRCYDL(6)	INPUT	4	
	3 ,LRSLEQ(6) ,LRMACH(6) ,LRALFA(6) ,LRYIU(6) ,LRYIL(6) ,LRSTRT(6)	INPUT	5	
	4 ,LRNN1(6) ,LRNA2(6) ,LRNN3(6) ,LRNN4(6) ,LRNN5(6) ,LRNN6(6)	INPUT	6	
	5 ,NLGRNG(6) ,NPARAB(6)	INPUT	7	
15	COMMON/NOU/ NAIRFL(6)	NOU	2	
	1 ,LRDEEQ(6) ,LRYSO2(6) ,LRYSEQ(6) ,LRDOEQ(6) ,LRRUEQ(6) ,LRUBEQ(6)	NOU	3	
	2 ,LRID(6) ,LRPOEQ(6) ,LRNOGO(6) ,LRSUB(6) ,LRSUPR(6) ,LRFLOW(6)	NOU	4	
	COMMON/NAXES/ NALL(6)	NAXES	2	
	1 ,NMXB(6) ,NUPB(6) ,NDOUXB(6) ,NAF3B(6) ,NDWNB(6) ,NKTAB(6)	NAXES	3	
20	2 ,NX1B(6) ,NX2B(6) ,NYB(6) ,NMB(6) ,NM01B(6) ,NM02B(6)	NAXES	4	
	3 ,NDU1B(6) ,NDU2B(6) ,NDDQ3(6) ,NPOB(6) ,NP1B(6) ,NPKTAB(6)	NAXES	5	
	COMMON/NPRCO/ NCUPS1(6) ,NCUPS2(6) ,NCAFU2(6) ,NCAFL2(6) ,NCAFU3(6)	NPRCO	2	
	1 ,NCDWN1(6) ,NCDWN2(6) ,NPUPS1(6) ,NPUPS2(6) ,NPAFU1(6) ,NPAFU2(6)	NPRCO	3	
	2 ,NPAFU3(6) ,NPAFL1(6) ,NPAFL2(6) ,NPDWN1(6) ,NPDWN2(6) ,NUPS(6)	NPRCO	4	
25	3 ,NAF1(6) ,NAF2(6)	NPRCO	5	
	DIMENSION LBID(2)	PRP6	13	
	DATA LBID/7,20/	PRP6	14	
	CALL ASCAL(1)	PRP6	15	
	CALL ERASE(NALL)	PRP6	16	
30	CALL ENLB(2,L9ID)	PRP6	17	
	CALL GENDF(NAIRFL,0)	PRP6	18	
	CALL GENDF(NCDWN1,0)	PRP6	19	
	CALL GENDF(NPAFU3,0)	PRP6	20	
	CALL GENDF(NPAFL2,0)	PRP6	21	
35	CALL GENDF(LRNN6,0)	PRP6	22	
	CALL GENDF(NDWNB,0)	PRP6	23	
	CALL WAITE(DUM,0,DUM,DUM)	PRP6	24	
	END	PRP6	25	

	OVERLAY(21,0)	DWN1	2
	PROGRAM DWN1	DWN1	3
		DWN1	4
5	C THIS PROGRAM DISPLAYS OUTPUT FROM SUBROUTINE IODNSTM	DWN1	5
	C	DWN1	6
	COMMON/ICNTRL/J ,ICNIT(2) ,LL(2) ,IGO(2)	ICNTRL	2
	COMMON/OUTCOM/	OUTCOM	2
	1 X1(160) ,Y1(160) ,Y2(160) ,NN1 ,NN2	OUTCOM	3
	COMMON/NOUT/ NAIRFL(6)	NOUT	2
10	1 ,LRDEEQ(6) ,LRVSOQ(6) ,LRYSEQ(6) ,LRDOEQ(6) ,LRRUEQ(6) ,LRUBEQ(6)	NOUT	3
	2 ,LRID(6) ,LRPOEQ(6) ,LRNOGO(6) ,LRSUB(6) ,LRSUPR(6) ,LRFLOW(6)	NOUT	4
	COMMON/NPRCD/ NCUPS1(6) ,NCUPS2(6) ,NCAFU2(6) ,NCAFL2(6) ,NCAFU3(6)	NPRCD	2
	1 ,NCDWN1(6) ,NCDWN2(6) ,NPUPS1(6) ,NPUPS2(6) ,NPAFU1(6) ,NPAFU2(6)	NPRCD	3
	2 ,NPAFU3(6) ,NPAFL1(6) ,NPAFL2(6) ,NPDWN1(6) ,NPDWN2(6) ,NUPS(6)	NPRCD	4
15	3 ,NAF1(6) ,NAF2(6)	NPRCD	5
	COMMON C ,CK ,RS ,FM ,ALPHA	COMMON	2
	COMMON/AINPUT/AIN(24) ,NNI(7) ,HI(6)	AINPUT	2
	COMMON/YUVSAV/NNN(3) ,YUV(156)	YUVSAV	2
	COMMON/PTARFL/XX(40,2) ,YY(40,2) ,AM(40,2) ,CA ,SA	PTARFL	2
20	COMMON/ISSCAL/IDSCAL	ISSCAL	2
	CALL ASCAL(1)	DWN1	16
	CALL ERASG(IDSCAL)	DWN1	17
	CALL ERASG(IDSCAL-1)	DWN1	18
	CALL ERASE(LRNOGO)	DWN1	19
25	CALL IODNSTM(J)	DWN1	20
	IF (NN2.NE.1) CALL GENDF(LRNOGO,0)	DWN1	21
	IF (NN2.EQ.1) CALL GENDF(NPDWN2,0)	DWN1	22
	CALL PLOTT2(1.0,10.0,0.8,1.0,0.8,1.0,2)	DWN1	23
	C	DWN1	24
30	C WAIT FOR AN ATTENTION SOURCE	DWN1	25
	CALL WAITE(DUM,0,DUM,DUM)	DWN1	26
	END	DWN1	27

OVERLAY(22,0)
PROGRAM DWN2

C
C
C

THIS PROGRAM DISPLAYS OUTPUT FROM SUBROUTINE AKUTTA

```

COMMON/COMNXY/NXY1(6) ,NXY2(6)
COMMON/INPUT/
1  LRUPS(6) ,LRSTG(6) ,LRAFU2(6),LRAFL2(6),LRAFU3(6),LRX00Q(6)
2  ,LRDIEQ(6),LRXSEQ(6),LRXAUP(6),LRCYDU(6),LRXALW(6),LRCYDL(6)
3  ,LRSLEQ(6),LRMACH(6),LRALFA(6),LRYIU(6) ,LRYIL(6) ,LRSTRT(6)
4  ,LRNN1(6) ,LRNA2(6) ,LRNN3(6) ,LRNN4(6) ,LRNN5(6) ,LRNN6(6)
5  ,NLGRNG(6),NPARAB(6)
COMMON/NOT/ NAIRFL(6)
1  ,LRDEEQ(6),LRYSDQ(6),LRYSEQ(6),LRDDEQ(6),LRRUEQ(6),LRUBEQ(6)
2  ,LRID(6) ,LRPOEQ(6),LRN0G0(6),LRSUB(6) ,LRSUPR(6),LRFLOW(6)
COMMON/NAXES/ NALL(6)
1  ,NMXB(6) ,NUPB(6) ,N0UDXB(6),NAF3B(6) ,N0WNB(6) ,NKTAB(6)
2  ,NX1B(6) ,NX2B(6) ,NYB(6) ,NMB(6) ,NM01B(6) ,NM02B(6)
3  ,NDU1B(6) ,NDU2B(6) ,NDDQB(6) ,NPOB(6) ,NP1B(6) ,NPKTAB(6)
COMMON/NPRCD/ NCUPS1(6),NCUPS2(6),NCAFU2(6),NCAFL2(6),NCAFU3(6)
1  ,NCDWN1(6),NCDWN2(6),NPUPS1(6),NPUPS2(6),NPAFU1(6),NPAFU2(6)
2  ,NPAFU3(6),NPAFL1(6),NPAFL2(6),NP0WN1(6),NP0WN2(6),NUPS(6)
3  ,NAF1(6) ,NAF2(6)
COMMON/COMPRS/XP(160,2) ,PP(160,2) ,NP(2)
COMMON/ISSCAL/IDSCAL
CALL ASCAL(1)
CALL ERASG(IDSCAL)
CALL ERASG(IDSCAL-1)
CALL ERASE(NALL)
CALL ENLB(1,20)
CALL GENDF(NAIRFL,0)
CALL GENDF(NCDWN2,0)
CALL GENDF(NAF1,0)
CALL GENDF(NKTAB,0)
CALL AKUTTA
PMAX = PP(1,1)
PMIN = PP(1,1)
XMAX = 1.0
XMIN = XP(1,1)
IF (XP(1,2).LT.XMIN) XMIN = XP(1,2)
DO 20 J=1,2
NN = NP(J)
DO 10 I=1,NN
IF (PP(I,J) -PMAX) 6,5,4
4 PMAX = PP(I,J)
GO TO 10
5 IF (PP(I,J) -PMIN) 8,10,10
8 PMIN = PP(I,J)
10 CONTINUE
20 CONTINUE
IF (PMIN.GT.0.0) PMIN = 0.0
CALL AREA1(XMIN,XMAX,PMIN,PMAX)
NGRAF = 0
NXY1(5) = 0
CALL DELETE(NXY1)
DO 40 J=1,2
NN = NP(J)
IF (NN.GE.60) NGRAF=1
IF (NN.GE.120) NGRAF=2
IF (NGRAF.EQ.3) GO TO 36
NXY1(6) = J
DO 30 I=1,NGRAF
NXY1(5) = I
30 CALL PLYLN(NXY1,1,XP(60*NGRAF-59,J),PP(60*NGRAF-59,J),60)
36 NXY1(6) = J
NXY1(5) = 60
CALL PLYLN(NXY1,1,XP(1+60*NGRAF,J),PP(1+60*NGRAF,J),
1 NP(J)-60*NGRAF-1)
40 CONTINUE

```

DWN2	2
DWN2	3
DWN2	4
DWN2	5
DWN2	6
COMNXY	2
INPUT	2
INPUT	3
INPUT	4
INPUT	5
INPUT	6
INPUT	7
NOUT	2
NOUT	3
NOUT	4
NAXES	2
NAXES	3
NAXES	4
NAXES	5
NPRCD	2
NPRCD	3
NPRCD	4
NPRCD	5
COMPRS	2
ISSCAL	2
DWN2	14
DWN2	15
DWN2	16
DWN2	17
DWN2	18
DWN2	19
DWN2	20
DWN2	21
DWN2	22
DWN2	23
DWN2	24
DWN2	25
DWN2	26
DWN2	27
DWN2	28
DWN2	29
DWN2	30
DWN2	31
DWN2	32
DWN2	33
DWN2	34
DWN2	35
DWN2	36
DWN2	37
DWN2	38
DWN2	39
DWN2	40
DWN2	41
DWN2	42
DWN2	43
DWN2	44
DWN2	45
DWN2	46
DWN2	47
DWN2	48
DWN2	49
DWN2	50
DWN2	51
DWN2	52
DWN2	53
DWN2	54
DWN2	55
DWN2	56
DWN2	57

70		NXY1(5) = 0	DWN2	58
		NXY1(6) = 0	DWN2	59
		CALL GENDF(NXY1,0)	DWN2	60
	C		DWN2	61
	C	WAIT FOR AN ATTENTION SOURCE	DWN2	62
75		CALL WAITE(DUM,0,DUM,DUM)	DWN2	63
		END	DWN2	64

	OVERLAY(23,0)	CVLI	2
	PROGRAM CVLI	CVLI	3
	COMMON/INPUT/	INPUT	2
5	1 ,LRUPS(6) ,LRSTG(6) ,LRAF02(6) ,LRAFL2(6) ,LRAF03(6) ,LRX00Q(6)	INPUT	3
	2 ,LRDIEQ(6) ,LRXSEQ(6) ,LRXAUP(6) ,LRCYDU(6) ,LRXALW(6) ,LRCYDL(6)	INPUT	4
	3 ,LRSLEQ(6) ,LRMACH(6) ,LRALFA(6) ,LRVIU(6) ,LRVIL(6) ,LRSTRT(6)	INPUT	5
	4 ,LRNN1(6) ,LRNA2(6) ,LRNN3(6) ,LRNN4(6) ,LRNN5(6) ,LRNN6(6)	INPUT	6
	5 ,NLGRNG(6) ,NPARA3(6)	INPUT	7
10	COMMON/NCHARS/NNEQ ,NAEQ ,NX00EQ(2) ,NOVIEQ(2) ,NXSEQ(2)	NCHARS	2
	1 ,NYSOEQ(2) ,NXAEQ(2) ,NCYDEQ(2) ,NSLEQ(2) ,NDEEQ(2) ,NYSEQ(2)	NCHARS	3
	2 ,NOVOEQ(2) ,NRUEQ(2) ,NUPEQ(2) ,NID(2) ,NMACHQ(2) ,NALPHA(2)	NCHARS	4
	3 ,NYIEQ(2) ,NYILEQ(2) ,NPOEQ(2) ,FMTI ,FMTF	NCHARS	5
	COMMON/AINPUT/AIN(24) ,NNI(7) ,HI(6)	AINPUT	2
	DIMENSION DUM(6) ,ID(6)	CVLI	7
15	C RETRIEVE ATTENTION INFORMATION FROM THE TEXT ENTITY IN A SIX INTEGER	CVLI	8
	C ARRAY ID	CVLI	9
	C CALL BPNFO(ITRN,ID)	CVLI	10
20	C ERASE THE TEXT ENTITY	CVLI	11
	C CALL ERASE(ID)	CVLI	12
	C REPLACE THE TEXT ENTITY WITH A CORRESPONDING LIGHT REGISTER	CVLI	13
	C CALL ENLR(1,ID)	CVLI	14
25	C	CVLI	15
	C	CVLI	16
	C DISPLAY THE NUMBERS BEING TYPED INTO THE LIGHT REGISTER FROM THE	CVLI	17
	C KEYBOARD	CVLI	18
	C CALL K3NPT(ID,IVAL)	CVLI	19
	C CALL ASCAL(1)	CVLI	20
30	C	CVLI	21
	C ERASE THE LIGHT REGISTER	CVLI	22
	C CALL ENLR(0,ID)	CVLI	23
	C ID1 = ID(1)-20	CVLI	24
35	C	CVLI	25
	C PUT THE NEW VALUE INTO THE CORRESPONDING TEXT ENTITY	CVLI	26
	C GO TO (10,20,30,40,50,60) ,ID1	CVLI	27
	10 NNI(1) = IVAL	CVLI	28
	CALL ENSHFT(NNEQ,3,NNI(1),FMTI)	CVLI	29
	CALL MODFY(ID,1,1,NNEQ)	CVLI	30
40	GO TO 200	CVLI	31
	20 NNI(2) = IVAL	CVLI	32
	CALL ENSHFT(NAEQ,3,NNI(2),FMTI)	CVLI	33
	CALL MODFY(ID,1,1,NAEQ)	CVLI	34
	GO TO 200	CVLI	35
45	30 NNI(3) = IVAL	CVLI	36
	CALL ENSHFT(NNEQ,3,NNI(3),FMTI)	CVLI	37
	CALL MODFY(ID,1,1,NNEQ)	CVLI	38
	GO TO 200	CVLI	39
50	40 NNI(4) = IVAL	CVLI	40
	CALL ENSHFT(NNEQ,3,NNI(4),FMTI)	CVLI	41
	CALL MODFY(ID,1,1,NNEQ)	CVLI	42
	GO TO 200	CVLI	43
55	50 NNI(5) = IVAL	CVLI	44
	CALL ENSHFT(NNEQ,3,NNI(5),FMTI)	CVLI	45
	CALL MODFY(ID,1,1,NNEQ)	CVLI	46
	GO TO 200	CVLI	47
60	60 NNI(6) = IVAL	CVLI	48
	CALL ENSHFT(NNEQ,3,NNI(6),FMTI)	CVLI	49
	CALL MODFY(ID,1,1,NNEQ)	CVLI	50
	C	CVLI	51
	C DISPLAY THIS TEXT ENTITY WHICH HAS BEEN CHANGED	CVLI	52
	C 200 CALL GENDF(ID,0)	CVLI	53
65	C	CVLI	54
	C WAIT FOR AN ATTENTION SOURCE	CVLI	55
	C CALL WAITE(DUM,0,DUM,DUM)	CVLI	56
	END	CVLI	57
		CVLI	58
		CVLI	59

	OVERLAY(24,0)	CVLR	2
	PROGRAM CVLR	CVLR	3
	COMMON/INPUT/	INPUT	2
5	1 LRUPS(6) ,LRSTG(6) ,LRAFU2(6) ,LRAFL2(6) ,LRAFU3(6) ,LRX00Q(6)	INPUT	3
	2 ,LRDIEQ(6) ,LRXSEQ(6) ,LRXAUP(6) ,LRCYDU(6) ,LRXALW(6) ,LRCYDL(6)	INPUT	4
	3 ,LRSLEQ(6) ,LRMACH(6) ,LRALFA(6) ,LRYIU(6) ,LRYIL(6) ,LRSTRT(6)	INPUT	5
	4 ,LRNN1(6) ,LRNA2(6) ,LRNN3(6) ,LRNN4(6) ,LRNN5(6) ,LRNN6(6)	INPUT	6
	5 ,NLGRNG(6) ,NPARAB(6)	INPUT	7
10	COMMON/NCHARS/NNEQ ,NAEQ ,NX00EQ(2) ,NDVIEQ(2) ,NXSEQ(2)	NCHARS	2
	1 ,NYSOEQ(2) ,NXAEQ(2) ,NCYDEQ(2) ,NSLEQ(2) ,NDEEQ(2) ,NYSEQ(2)	NCHARS	3
	2 ,NDVOEQ(2) ,NRUEQ(2) ,NUBEQ(2) ,NID(2) ,NMACHQ(2) ,NALPHA(2)	NCHARS	4
	3 ,NYIEQ(2) ,NYILEQ(2) ,NP0EQ(2) ,FMTI ,FMTF	NCHARS	5
	COMMON/AINPUT/AIN(24) ,NNI(7) ,HI(6)	AINPUT	2
15	COMMON C ,CK ,RS ,FM ,ALPHA	COMMON	2
	DIMENSION DUM(6) ,ID(6)	CVLR	8
	C	CVLR	9
	C RETRIEVE ATTENTION INFORMATION FROM THE TEXT ENTITY IN A SIX INTEGER	CVLR	10
	C ARRAY ID	CVLR	11
	CALL 9PNFO(ITRN,ID)	CVLR	12
20	C	CVLR	13
	C ERASE THE TEXT ENTITY	CVLR	14
	CALL ERASE(ID)	CVLR	15
	C	CVLR	16
	C REPLACE THE TEXT ENTITY WITH A CORRESPONDING LIGHT REGISTER	CVLR	17
25	CALL ENLR(1,ID)	CVLR	18
	C	CVLR	19
	C DISPLAY THE NUMBERS BEING TYPED INTO THE LIGHT REGISTER FROM THE	CVLR	20
	C KEYBOARD	CVLR	21
	CALL K9NPT(ID,VAL)	CVLR	22
30	C	CVLR	23
	C ERASE THE LIGHT REGISTER	CVLR	24
	CALL ENLR(0,ID)	CVLR	25
	CALL ASCAL(1)	CVLR	26
	ID1 = ID(1)	CVLR	27
35	C	CVLR	28
	C PUT THE NEW VALUE INTO THE CORRESPONDING TEXT ENTITY	CVLR	29
	GO TO (10,20,30,40,50,60,70,80,90,100,110,120,130,140) ,ID1	CVLR	30
	10 AIN(8) = VAL	CVLR	31
40	CALL ENSHFT(NX00EQ,4,AIN(8) ,FMTF)	CVLR	32
	CALL MODFY(ID,1,2,NX00EQ)	CVLR	33
	GO TO 200	CVLR	34
	20 AIN(1) = VAL	CVLR	35
	CALL ENSHFT(NDVIEQ,8,AIN(1) ,FMTF)	CVLR	36
	CALL MODFY(ID,1,2,NDVIEQ)	CVLR	37
45	GO TO 200	CVLR	38
	30 AIN(2) = VAL	CVLR	39
	CALL ENSHFT(NXSEQ,3,AIN(2) ,FMTF)	CVLR	40
	CALL MODFY(ID,1,2,NXSEQ)	CVLR	41
	GO TO 200	CVLR	42
50	40 AIN(3) = VAL	CVLR	43
	CALL ENSHFT(NXAEQ,3,AIN(3) ,FMTF)	CVLR	44
	CALL MODFY(ID,1,2,NXAEQ)	CVLR	45
	GO TO 200	CVLR	46
	50 AIN(4) = VAL	CVLR	47
55	CALL ENSHFT(NCYDEQ,4,AIN(4) ,FMTF)	CVLR	48
	CALL MODFY(ID,1,2,NCYDEQ)	CVLR	49
	GO TO 200	CVLR	50
	60 AIN(5) = VAL	CVLR	51
	CALL ENSHFT(NXAEQ,3,AIN(5) ,FMTF)	CVLR	52
60	CALL MODFY(ID,1,2,NXAEQ)	CVLR	53
	GO TO 200	CVLR	54
	70 AIN(6) = VAL	CVLR	55
	CALL ENSHFT(NCYDEQ,4,AIN(6) ,FMTF)	CVLR	56
	CALL MODFY(ID,1,2,NCYDEQ)	CVLR	57
65	GO TO 200	CVLR	58
	80 AIN(7) = VAL	CVLR	59
	CALL ENSHFT(NSLEQ,10,AIN(7) ,FMTF)	CVLR	60
	CALL MODFY(ID,1,2,NSLEQ)	CVLR	61
	90 GO TO 200	CVLR	62

70	100 GO TO 200	CVLR	63
	110 FM = VAL	CVLR	64
	CALL ENSHFT(NMACHQ,9,FM,FMTF)	CVLR	65
	CALL MODIFY(ID,1,2,NMACHQ)	CVLR	66
	GO TO 200	CVLR	67
75	120 ALPHA = VAL	CVLR	68
	CALL ENSHFT(NALPHA,6,ALPHA,FMTF)	CVLR	69
	CALL MODIFY(ID,1,2,NALPHA)	CVLR	70
	GO TO 200	CVLR	71
	130 AIN(11) = VAL	CVLR	72
80	CALL ENSHFT(NYIUEQ,10,AIN(11),FMTF)	CVLR	73
	CALL MODIFY(ID,1,2,NYIUEQ)	CVLR	74
	GO TO 200	CVLR	75
	140 AIN(12) = VAL	CVLR	76
	CALL ENSHFT(NYILEQ,10,AIN(12),FMTF)	CVLR	77
85	CALL MODIFY(ID,1,2,NYILEQ)	CVLR	78
	C	CVLR	79
	C DISPLAY THIS TEXT ENTITY WHICH HAS BEEN CHANGED	CVLR	80
	200 CALL GENOF(ID,0)	CVLR	81
	C	CVLR	82
90	C WAIT FOR AN ATTENTION SOURCE	CVLR	83
	CALL WAITE(DUM,0,DUM,DUM)	CVLR	84
	END	CVLR	85

15

	OVERLAY(26,0)	STOP	2
	PROGRAM STOP	STOP	3
	COMMON/NCON/ ICON	NCON	2
	COMMON/INPUT/	INPUT	2
5	1 ,LRUPS(6) ,LRSTG(6) ,LRAFU2(6) ,LRAFL2(6) ,LRAFU3(6) ,LRX00Q(6)	INPUT	3
	2 ,LRDIEQ(6) ,LRXSEQ(6) ,LRXAUP(6) ,LRCYDU(6) ,LRXALW(6) ,LRCYDL(6)	INPUT	4
	3 ,LRSLEQ(6) ,LRMACH(6) ,LRALFA(6) ,LRYIU(6) ,LRYIL(6) ,LRSTRT(6)	INPUT	5
	4 ,LRNN1(6) ,LRNA2(6) ,LRNN3(6) ,LRNN4(6) ,LRNN5(6) ,LRNN6(6)	INPUT	6
	5 ,NLGRNG(6) ,NPARA9(6)	INPUT	7
10	COMMON/NOUT/ NAIRFL(6)	NOUT	2
	1 ,LRDEEQ(6) ,LRYSEQ(6) ,LRDOEQ(6) ,LRRUEQ(6) ,LRUBEQ(6)	NOUT	3
	2 ,LRID(6) ,LRPOEQ(6) ,LRNOGO(6) ,LRSUB(6) ,LRSUPR(6) ,LRFLOW(6)	NOUT	4
	COMMON/NPRCD/ NCUPS1(6) ,NCUPS2(6) ,NCAFU2(6) ,NCAFL2(6) ,NCAFU3(6)	NPRCD	2
	1 ,NCDWN1(6) ,NCDWN2(6) ,NPUPS1(6) ,NPUPS2(6) ,NPAFU1(6) ,NPAFU2(6)	NPRCD	3
15	2 ,NPAFU3(6) ,NPAFL1(6) ,NPAFL2(6) ,NPDOWN1(6) ,NPDOWN2(6) ,NUPS(6)	NPRCD	4
	3 ,NAF1(6) ,NAF2(6)	NPRCD	5
	COMMON/NAXES/ NALL(6)	NAXES	2
	1 ,NMXB(6) ,NUPB(6) ,NDUDB(6) ,NAF3B(6) ,NDWNB(6) ,NKTAB(6)	NAXES	3
	2 ,NX1B(6) ,NX2B(6) ,NYB(6) ,NMB(6) ,NM01B(6) ,NM02B(6)	NAXES	4
20	3 ,NDU1B(6) ,NDU2B(6) ,NDQD3(6) ,NPOB(6) ,NP13(6) ,NPKTAB(6)	NAXES	5
	C	STOP	9
	C ERASE THE SCREEN DISPLAYS	STOP	10
	CALL ASCAL(1)	STOP	11
	CALL ENLB(0,1)	STOP	12
25	CALL ERASG(1)	STOP	13
	CALL ERASG(2)	STOP	14
	CALL ERASE(NALL)	STOP	15
	C	STOP	16
	C CLOSE THE DATA FILE	STOP	17
30	CALL CLOS	STOP	18
	C	STOP	19
	C RELEASE THE CONSOLE	STOP	20
	CALL RLCON(ICON)	STOP	21
	END	STOP	22

		SUBROUTINE PLOTT(X1MIN,X1MAX,Y1MIN,Y1MAX)	PLOTT	2
	C		PLOTT	3
	C	THIS SUBROUTINE DISPLAYS TWO DISJOINTED CURVES COVERING THE	PLOTT	4
	C	GRAPHICAL DISPLAY AREA	PLOTT	5
5	C	COMMON/OUTCOM/	PLOTT	6
		1 X1(160) ,Y1(160) ,Y2(160) ,NN1 ,NN2	OUTCOM	2
		COMMON/COMNXY/NXY1(6) ,NXY2(6)	OUTCOM	3
		COMMON/AINPUT/AIN(24) ,NNI(7) ,HI(6)	COMNXY	2
			AINPUT	2
10	C		PLOTT	10
	C	IF THERE IS ONLY ONE POINT TO BE PLOTTED, FORGET IT AND PLOT FOUR	PLOTT	11
	C	POINTS ON THE SCREEN TO FORM A LARGE X COVERING THE SCREEN	PLOTT	12
		IF(NN1.GT.1) GO TO 5	PLOTT	13
		NN1 = 4	PLOTT	14
15		X1(1) = X1MIN	PLOTT	15
		X1(2) = X1MAX	PLOTT	16
		X1(3) = X1MIN	PLOTT	17
		X1(4) = X1MAX	PLOTT	18
		Y1(1) = Y1MIN	PLOTT	19
20		Y1(2) = Y1MAX	PLOTT	20
		Y1(3) = Y1MAX	PLOTT	21
		Y1(4) = Y1MIN	PLOTT	22
		XMIN = X1MIN	PLOTT	23
		YMIN = Y1MIN	PLOTT	24
25		XMAX = X1MAX	PLOTT	25
		YMAX = Y1MAX	PLOTT	26
		NXY1(5) = 0	PLOTT	27
		CALL DLETE(NXY1)	PLOTT	28
		NXY1(5) = 60	PLOTT	29
30		CALL AREA1(XMIN,XMAX,YMIN,YMAX)	PLOTT	30
		CALL PLYLN(NXY1,1,X1(1),Y1(1),3)	PLOTT	31
		CALL GENDF(NXY1,0)	PLOTT	32
		RETURN	PLOTT	33
	C		PLOTT	34
35	C	FIND THE LARGEST AND SMALLEST VALUES OF Y1	PLOTT	35
		5 CALL AMXMN1(YMAX,YMIN)	PLOTT	36
		NXY1(5) = 0	PLOTT	37
		CALL DLETE(NXY1)	PLOTT	38
		XMIN = X1(1)	PLOTT	39
40		XMAX = X1(NN1)	PLOTT	40
		IF(X1MIN.LT.XMIN) XMIN=X1MIN	PLOTT	41
		IF(X1MAX.GT.XMAX) XMAX = X1MAX	PLOTT	42
		IF(Y1MIN.LT.YMIN) YMIN = Y1MIN	PLOTT	43
		IF(Y1MAX.GT.YMAX) YMAX = Y1MAX	PLOTT	44
45	C		PLOTT	45
	C	FIND THE NUMBER OF POINTS IN THE FIRST AND SECOND CURVES	PLOTT	46
		NNN1 = NNI(7)-1	PLOTT	47
		NNN2 = NNI(7)-NNI(7)	PLOTT	48
		IF(NNI(7).EQ.0) NNN1=NN1	PLOTT	49
50		IF(NNI(7).EQ.0) NNN2=0	PLOTT	50
	C		PLOTT	51
	C	CREATE THE POLYLINE ENTITY FOR THE FIRST CURVE	PLOTT	52
		NGRAF1 = 0	PLOTT	53
		IF(NNN1.GT.60) NGRAF1 = 1	PLOTT	54
55		IF(NNN1.GT.120) NGRAF1 = 2	PLOTT	55
		IF(NGRAF1.EQ.0) GO TO 30	PLOTT	56
		DO 20 I=1,NGRAF1	PLOTT	57
		NXY1(5) = I	PLOTT	58
	20	CALL PLYLN(NXY1,1,X1(60*I-59),Y1(60*I-59),60)	PLOTT	59
60	30	IF((NNN1-60*NGRAF1-1).LE.0) GO TO 40	PLOTT	60
		NXY1(5) = NGRAF1+1	PLOTT	61
		CALL PLYLN(NXY1,1,X1(1+60*NGRAF1),Y1(1+60*NGRAF1),NNN1-60*NGRAF1-1	PLOTT	62
		1)	PLOTT	63
	C		PLOTT	64
65	C	CREATE THE POLYLINE ENTITY FOR THE SECOND CURVE	PLOTT	65
		40 NGRAF2=0	PLOTT	66
		IF(NNN2.GT.60) NGRAF2 = 1	PLOTT	67
		IF(NNN2.GT.120) NGRAF2 = 2	PLOTT	68
		N1 = NGRAF1+2	PLOTT	69

70	IF(NGRAF2.EQ.0) GO TO 60	PLOTT	70
	N2 = N1+NGRAF2-1	PLOTT	71
	DO 50 I=N1,N2	PLOTT	72
	NXY1(5) = I	PLOTT	73
	NNNN1 = NNN1+60*(I-N1+1)-58	PLOTT	74
75	50 CALL PLYLN(NXY1,1,X1(NNNN1),Y1(NNNN1),60)	PLOTT	75
	60 IF((NNN2-60*NGRAF2-1).LE.0) GO TO 70	PLOTT	76
	NXY1(5) = N1+NGRAF2	PLOTT	77
	CALL PLYLN(NXY1,1,X1(NNN1+60*NGRAF2+2),Y1(NNN1+60*NGRAF2+2),	PLOTT	78
	1 NNN2-60*NGRAF2-1)	PLOTT	79
80		PLOTT	80
	C	PLOTT	81
	C CREATE THE GRID DISPLAY	PLOTT	82
	70 CALL AREA1(XMIN,XMAX,YMIN,YMAX)	PLOTT	83
	NXY1(5) = 0	PLOTT	84
85		PLOTT	85
	C	PLOTT	86
	C DISPLAY THE TWO POLYLINE ENTITIES	PLOTT	87
	CALL GENDF(NXY1,0)	PLOTT	88
	RETURN		
	END		

	SUBROUTINE PLOTT1(X1MIN,X1MAX,Y1MIN,Y1MAX)	PLOTT1	2
C		PLOTT1	3
C	THIS SUBROUTINE DISPLAYS ONE CURVE IN THE GRAPHIC DISPLAY AREA	PLOTT1	4
	COMMON/OUTCOM/	OUTCOM	2
5	1 X1(160) ,Y1(160) ,Y2(160) ,NN1 ,NN2	OUTCOM	3
	COMMON/COMNXY/NXY1(6) ,NXY2(6)	COMNXY	2
C		PLOTT1	7
C	IF THERE IS ONLY ONE POINT TO BE PLOTTED, FORGET IT AND PLOT FOUR	PLOTT1	8
C	POINTS ON THE SCREEN TO FORM A LARGE X COVERING THE SCREEN	PLOTT1	9
10	IF (NN1.GT.1) GO TO 5	PLOTT1	10
	NN1=4	PLOTT1	11
	X1(1) = X1MIN	PLOTT1	12
	X1(2) = X1MAX	PLOTT1	13
	X1(3) = X1MIN	PLOTT1	14
15	X1(4) = X1MAX	PLOTT1	15
	Y1(1) = Y1MIN	PLOTT1	16
	Y1(2) = Y1MAX	PLOTT1	17
	Y1(3) = Y1MAX	PLOTT1	18
	Y1(4) = Y1MIN	PLOTT1	19
20	C	PLOTT1	20
C	FIND THE LARGEST AND SMALLEST VALUES OF Y1	PLOTT1	21
	5 CALL AMXMMN1(YMAX,YMIN)	PLOTT1	22
C		PLOTT1	23
C	CREATE THE POLYLINE ENTITY FOR NXY1	PLOTT1	24
25	NGRAF = 0	PLOTT1	25
	NXY1(5) = 0	PLOTT1	26
	CALL DELETE(NXY1)	PLOTT1	27
	XMIN = X1(1)	PLOTT1	28
	XMAX = X1(NN1)	PLOTT1	29
30	IF (X1MIN.LT.XMIN) XMIN = X1MIN	PLOTT1	30
	IF (X1MAX.GT.XMAX) XMAX = X1MAX	PLOTT1	31
	IF (Y1MIN.LT.YMIN) YMIN = Y1MIN	PLOTT1	32
	IF (Y1MAX.GT.YMAX) YMAX = Y1MAX	PLOTT1	33
	IF (NN1.GT.60) NGRAF = 1	PLOTT1	34
35	IF (NN1.GT.120) NGRAF = 2	PLOTT1	35
	IF (NGRAF.EQ.0) GO TO 30	PLOTT1	36
	DO 20 I=1,NGRAF	PLOTT1	37
	NXY1(5) = I	PLOTT1	38
	CALL PLYLN(NXY1,1,X1(60*I-59),Y1(60*I-59),60)	PLOTT1	39
40	20 CONTINUE	PLOTT1	40
30	NXY1(5) = 60	PLOTT1	41
	IF ((NN1-60*NGRAF-1).LE.0) GO TO 40	PLOTT1	42
	CALL PLYLN(NXY1,1,X1(1+60*NGRAF),Y1(1+60*NGRAF),NN1-60*NGRAF-1)	PLOTT1	43
40	CALL AREA1(XMIN,XMAX,YMIN,YMAX)	PLOTT1	44
45	NXY1(5) = 0	PLOTT1	45
C		PLOTT1	46
C	DISPLAY THE POLYLINE ENTITY FOR NXY1	PLOTT1	47
	CALL GENDF(NXY1,0)	PLOTT1	48
	RETURN	PLOTT1	49
50	END	PLOTT1	50

	SUBROUTINE PLOTT2(X1MIN,X1MAX,Y1MIN,Y1MAX,Y2MIN,Y2MAX,J)	PLOTT2	2
C		PLOTT2	3
C	THIS SUBROUTINE DISPLAYS TWO CURVES IN THE TWO SUBAREAS OF THE	PLOTT2	4
C	GRAPHIC DISPLAY AREA	PLOTT2	5
5		PLOTT2	6
C	COMMON/OUTCOM/	OUTCOM	2
	1 X1(160) ,Y1(160) ,Y2(160) ,NN1 ,NN2	OUTCOM	3
	COMMON/COMNXY/NXY1(5) ,NXY2(6)	COMNXY	2
C		PLOTT2	9
10	IF THERE IS ONLY ONE POINT TO BE PLOTTED, FORGET IT AND PLOT FOUR	PLOTT2	10
C	POINTS ON THE SCREEN TO FORM A LARGE X COVERING THE SCREEN	PLOTT2	11
	IF(NN1.GT.1) GO TO 5	PLOTT2	12
	NN1=4	PLOTT2	13
	X1(1) = X1MIN	PLOTT2	14
15	X1(2) = X1MAX	PLOTT2	15
	X1(3) = X1MIN	PLOTT2	16
	X1(4) = X1MAX	PLOTT2	17
	Y1(1) = Y1MIN	PLOTT2	18
	Y1(2) = Y1MAX	PLOTT2	19
20	Y1(3) = Y1MAX	PLOTT2	20
	Y1(4) = Y1MIN	PLOTT2	21
	Y2(1) = Y2MIN	PLOTT2	22
	Y2(2) = Y2MAX	PLOTT2	23
25	Y2(3) = Y2MAX	PLOTT2	24
	Y2(4) = Y2MIN	PLOTT2	25
C		PLOTT2	26
C	FIND THE LARGEST AND SMALLEST VALUES OF Y1	PLOTT2	27
	5 CALL AMXMN1(YMAX,YMIN)	PLOTT2	28
C		PLOTT2	29
30	CREATE THE POLYLINE ENTITY FOR NXY1	PLOTT2	30
	NGRAF = 0	PLOTT2	31
	NXY1(5) = 0	PLOTT2	32
	CALL DLETE(NXY1)	PLOTT2	33
	XMIN = X1(1)	PLOTT2	34
35	XMAX = X1(NN1)	PLOTT2	35
	IF(X1MIN.LT.XMIN) XMIN = X1MIN	PLOTT2	36
	IF(X1MAX.GT.XMAX) XMAX = X1MAX	PLOTT2	37
	IF(Y1MIN.LT.YMIN) YMIN = Y1MIN	PLOTT2	38
	IF(Y1MAX.GT.YMAX) YMAX = Y1MAX	PLOTT2	39
40	IF(NN1.GT.60) NGRAF = 1	PLOTT2	40
	IF(NN1.GT.120) NGRAF = 2	PLOTT2	41
	IF(NGRAF.EQ.0) GO TO 30	PLOTT2	42
	DO 20 I=1,NGRAF	PLOTT2	43
	NXY1(5) = I	PLOTT2	44
45	CALL PLYLN(NXY1,1,X1(60*I-59),Y1(60*I-59),60)	PLOTT2	45
	20 CONTINUE	PLOTT2	46
	30 NXY1(5) = 60	PLOTT2	47
	IF((NN1-60*NGRAF-1).LE.0) GO TO 32	PLOTT2	48
	CALL PLYLN(NXY1,1,X1(1+60*NGRAF),Y1(1+60*NGRAF),NN1-60*NGRAF-1)	PLOTT2	49
50	32 CALL AREA2(XMIN,XMAX,YMIN,YMAX,1)	PLOTT2	50
	NXY1(5) = 0	PLOTT2	51
C		PLOTT2	52
C	DISPLAY THE POLYLINE ENTITY FOR NXY1	PLOTT2	53
	CALL GENDF(NXY1,0)	PLOTT2	54
55	IF(J.EQ.1) RETURN	PLOTT2	55
	CALL AMXMN2(YMAX,YMIN)	PLOTT2	56
	NXY2(5) = 0	PLOTT2	57
	CALL DLETE(NXY2)	PLOTT2	58
	IF(NN1.LE.1) GO TO 50	PLOTT2	59
60	IF(Y2MIN.LT.YMIN) YMIN = Y2MIN	PLOTT2	60
	IF(Y2MAX.GT.YMAX) YMAX = Y2MAX	PLOTT2	61
C		PLOTT2	62
C	CREATE THE POLYLINE ENTITY FOR NXY2	PLOTT2	63
	IF(NGRAF.EQ.0) GO TO 50	PLOTT2	64
65	DO 40 I=1,NGRAF	PLOTT2	65
	NXY2(5) = I	PLOTT2	66
	40 CALL PLYLN(NXY2,1,X1(60*I-59),Y2(60*I-59),60)	PLOTT2	67
	50 NXY2(5) = 61	PLOTT2	68
	IF((NN1-60*NGRAF-1).LE.0) GO TO 50	PLOTT2	69

70	CALL PLYLN(NXY2,1,X1(1+60*NGRAF),Y2(1+60*NGRAF),NN1-60*NGRAF-1)	PLOTT2	70
	60 CALL AREA2(XMIN,XMAX,YMIN,YMAX,?)	PLOTT2	71
	NXY2(5) = 0	PLOTT2	72
	C	PLOTT2	73
	C DISPLAY THE POLYLINE ENTITY FOR NXY?	PLOTT2	74
75	CALL GENOF(NXY2,0)	PLOTT2	75
	RETURN	PLOTT2	76
	END	PLOTT2	77

	SUBROUTINE AREA1(XMIN,XMAX,YMIN,YMAX)	AREA1	2
		AREA1	3
	THIS SUBROUTINE DETERMINES THE GRID DISPLAY FOR A GRAPH COVERING	AREA1	4
	THE ENTIRE GRAPHIC DISPLAY AREA	AREA1	5
5		AREA1	6
	COMMON/ISSCAL/IDSCAL	ISSCAL	2
	DIMENSION ALIM(4),USER(4)	AREA1	8
	DATA ALIM/-40.,-40.,57.,57./	AREA1	9
	DX = XMAX-XMIN	AREA1	10
10	DY = YMAX-YMIN	AREA1	11
	USER(1) = XMIN	AREA1	12
	USER(2) = YMIN	AREA1	13
	USER(3) = XMAX	AREA1	14
	USER(4) = YMAX	AREA1	15
15	IDSCAL = 2	AREA1	16
	CALL SSCAL(IDSCAL,ALIM,USER)	AREA1	17
	CALL ASCAL(IDSCAL)	AREA1	18
	CALL GRDNH(IDSCAL)	AREA1	19
	CALL CGRIDIV(2,XMIN,XMAX, YMIN,YMAX,DX,DY,0,0,1,6, 6)	AREA1	20
20	CALL RTNID(IDA)	AREA1	21
	RETURN	AREA1	22
	END	AREA1	23

		SUBROUTINE AREA2(XMIN,XMAX,YMIN,YMAX, ID)	AREA2	2
	C		AREA2	3
	C	THIS SUBROUTINE CREATES THE GRID DISPLAY FOR A GRAPH COVERING A	AREA2	4
	C	SUBAREA OF THE ENTIRE GRAPHIC DISPLAY AREA DEPENDING ON ID	AREA2	5
5	C		AREA2	6
		COMMON/ISSCAL/IDSCAL	ISSCAL	2
		DIMENSION ALIM(4,2),USER(4,2)	AREA2	9
		DATA ALIM/-40.,-40.,57.,10.,-40.,17.,57.,57./	AREA2	9
		USER(1,ID) = XMIN	AREA2	10
10		USER(2,ID) = YMIN	AREA2	11
		USER(3,ID) = XMAX	AREA2	12
		USER(4,ID) = YMAX	AREA2	13
		DX = XMAX-XMIN	AREA2	14
		DY = YMAX-YMIN	AREA2	15
15		IDSCAL = ID*2	AREA2	16
		CALL SSCAL(IDSCAL,ALIM(1,ID),USER(1,ID))	AREA2	17
		CALL ASCAL(IDSCAL)	AREA2	18
		CALL GRDN4(IDSCAL)	AREA2	19
		CALL CGRIDIV(2,XMIN,XMAX,YMIN,YMAX,DX,DY,0,0,1,1,6,6)	AREA2	20
20		CALL RTNID(IDA)	AREA2	21
		RETURN	AREA2	22
		END	AREA2	23

		SUBROUTINE AMXMN1(V1MAX,Y1MIN)	AMXMN1	2
C			AMXMN1	3
C		THIS SUBROUTINE DETERMINES THE LARGEST AND SMALLEST VALUES FOR V1	AMXMN1	4
C			AMXMN1	5
5		COMMON/OUTCOM/	OUTCOM	2
	1	X1(160) ,V1(160) ,Y2(160) ,NN1 ,NN2	OUTCOM	3
		Y1MAX = V1(1)	AMXMN1	7
		Y1MIN = V1(1)	AMXMN1	8
		DO 20 I=2,NN1	AMXMN1	9
10		IF(V1(I)-Y1MAX) 15,15,12	AMXMN1	10
	12	Y1MAX = V1(I)	AMXMN1	11
		GO TO 20	AMXMN1	12
	15	IF(V1(I)-Y1MIN) 18,20,20	AMXMN1	13
	18	Y1MIN = V1(I)	AMXMN1	14
15	20	CONTINUE	AMXMN1	15
		RETURN	AMXMN1	16
		END	AMXMN1	17

	SUBROUTINE AMXMN2(Y2MAX,Y2MIN)	AMXMN2	2
		AMXMN2	3
C	THIS SUBROUTINE DETERMINES THE LARGEST AND SMALLEST VALUES FOR Y2	AMXMN2	4
C		AMXMN2	5
5	COMMON/OUTCOM/	OUTCOM	2
	1 X1(160) ,Y1(160) ,Y2(160) ,NN1 ,NN2	OUTCOM	3
	Y2MAX = Y2(1)	AMXMN2	7
	Y2MIN = Y2(1)	AMXMN2	8
	DO 30 I=2,NN1	AMXMN2	9
10	IF(Y2(I) -Y2MAX) 25,25,22	AMXMN2	10
	22 Y2MAX = Y2(I)	AMXMN2	11
	GO TO 30	AMXMN2	12
	25 IF(Y2(I) -Y2MIN) 28,30,30	AMXMN2	13
	28 Y2MIN = Y2(I)	AMXMN2	14
15	30 CONTINUE	AMXMN2	15
	RETURN	AMXMN2	16
	END	AMXMN2	17

REFERENCES

1. Tai, T. C., "Application of the Method of Integral Relations to Transonic Airfoil Problems: Part I - Inviscid Supercritical Flow over Symmetrical Airfoil at Zero Angle of Attack," NSRDC Report 3424 (Sep 1970); also presented as Paper 71-98, AIAA 9th Aerospace Sciences Meeting, New York, N. Y. (Jan 1971).
2. Tai, T. C., "Application of the Method of Integral Relations to Transonic Airfoil Problems: Part II - Inviscid Supercritical Flow About Lifting Airfoils with Embedded Shock Wave," NSRDC Report 3424 (Jul 1972); also presented as Paper 73-658, AIAA 6th Fluid and Plasma Dynamics Conference, Palm Springs, California (Jul 1973).
3. Graham, D. J. et al., "A Systematic Investigation of Pressure Distribution at High Speeds over Five Representative NACA Low-Drag and Conventional Airfoil Sections," NACA Report 832 (1945).
4. Ahlberg, J. H. et al., "The Theory of Splines and Their Applications," Academic Press, New York (1967).

INITIAL DISTRIBUTION

Copies

1	ARMY CHIEF OF RES & DEV
1	ABRL/TB MESZAROS
1	AMC REDSTONE SIC/DUERR
1	AMERDC
3	ONR
	1 ONR 430
	1 ONR 432/L. BRAM
	1 ONR 461
1	USNA LIB
1	NAVPGSCOL LIB
10	AIR
	1 AIR 03A
	1 AIR 03C
	1 AIR 310
	3 AIR 320
	1 AIR 50174B
	1 AIR 5108
	2 AIR 5301
1	ORD LIB
1	NAVAIRDEVCEN ADT LIB
1	NAVWPNSCEN 753 LIB
1	NOL 730 LIB
1	NWL LIB
1	NAVMISCEN
1	AFFDL/APPL MECH LIB
1	AFOSR
1	AIR FORCE AERO RES LABS
1	AFIT
1	AEDC
4	NASA
	1 HQS NASA
	1 NASA AMES RES CEN
	1 NASA LANGLEY RES CEN
	1 NASA RES CEN
1	NSF

CENTER DISTRIBUTION

1	C 0000	NELSON PERRY W
20	C 1606	TAI TSZE C
10	C 1830	ERNST HERBERT M
30	C 5614	REPORTS DISTRIBUTION
	1 C 5641	LIBRARY
	1 A 5642	LIBRARY
2	C 5643	AVIATION COLLECTION

UNCLASSIFIED

Security Classification

DOCUMENT CONTROL DATA - R & D

(Security classification of title, body of abstract and indexing annotation must be entered when the overall report is classified)

1. ORIGINATING ACTIVITY (Corporate author) Aviation and Surface Effects Department Naval Ship Research and Development Center Bethesda, Maryland 20034		2a. REPORT SECURITY CLASSIFICATION Unclassified	
		2b. GROUP	
3. REPORT TITLE A COMPUTER PROGRAM THAT USES INTERACTIVE GRAPHICS TO SOLVE INVISCID TRANSONIC FLOWS OVER LIFTING AIRFOILS			
4. DESCRIPTIVE NOTES (Type of report and inclusive dates) Research and Development Report			
5. AUTHOR(S) (First name, middle initial, last name) Douglas A. Lien and Tsze C. Tai			
6. REPORT DATE September 1973	7a. TOTAL NO. OF PAGES 201	7b. NO. OF REFS 4	
8a. CONTRACT OR GRANT NO. NSRDC AIRTASK R230.201	9a. ORIGINATOR'S REPORT NUMBER(S) NSRDC Report 4252		
b. PROJECT NO. c. NSRDC 1-1670-277	9b. OTHER REPORT NO(S) (Any other numbers that may be assigned this report) Aero Report 1194		
d.			
10. DISTRIBUTION STATEMENT FOR OFFICIAL USE ONLY			
11. SUPPLEMENTARY NOTES		12. SPONSORING MILITARY ACTIVITY Commander Naval Air Systems Command (AIR-320) Washington, D. C. 20360	
13. ABSTRACT <p>A computer program that utilizes the method of integral relations has been developed at the Naval Ship Research and Development Center for use in determining the inviscid transonic flows past lifting airfoils. It allows for a change of entropy across the shock wave and accounts for the presence of an oblique or normal shock at the shock foot. Since many iterations of the trial and error type are required to obtain the converged flow solution, the program has been adapted for use on the interactive graphic systems of the CDC 6700 computer. This minimizes the man-machine interaction time involved with such iterations. It has been applied to several airfoil cases with supercritical flow on the upper surface and subcritical flow on the lower surface. The theoretical basis for this program has previously been reported. This report documents the computer program which is written in the language of FORTRAN Extended Version 3.0.</p>			

